## nexdrans <br> Consulting

A Division of NextEng Consulting Group Inc.

Transportation Planning
Traffic Impact Assessment
Parking Assessment
Site Access Design \& Review
Site Servicing and Grading
Stormwater Management Municipal Road Design

## PROPOSED <br> RESIDENTIAL <br> DEVELOPMENT

1020, 1024, 1028, 1032 and 1042
Sixth Line Road
Town of Oakville, Ontario
October 2016
Project No:NT-16-114

October 3, 2016

Ms. Alyssa Trivelli, Development Manager

Dunpar
105 Six Point Road
Etobicoke, ON M8Z 2X3

## Re: Transportation Impact Study Proposed Residential Development 1020, 1024, 1028, 1032 and 1042 Sixth Line Road Town of Oakville, Ontario Our Project No. NT-16-114

NexTrans Engineering is pleased to present the enclosed Transportation Impact Study for the above noted site in support of the Official Plan and Zoning By-law Amendment Applications.

The subject development is located at the municipal addresses 1020, 1024, 1028, 1032 and 1042 Sixth Line Road, in the Town of Oakville. The subject development generally bounded to the east by Sixth Line Road, to the south by North Service Road and to the north by Sunny Crest Lane. The proposed development consists of 81 residential condominium townhouse units and the retention of two single family homes at 1024 and 1028 Sixth Line Road. The proposed development provides a total of 179 vehicle parking spaces, including 20 visitor parking spaces. Vehicular accesses are proposed via one main entrance and one laneway onto Sixth Line Road, with one additional emergency access proposed onto Sunny Crest Lane.

The Transportation Impact Study concludes that the development proposal can adequately be accommodated by the existing transportation network in the area. We trust the enclosed sufficiently addresses your needs. Should you have any questions, please do not hesitate to contact the undersigned.

Yours truly,

## NEXTRANS ENGINEERING



Richard Pernicky, CET, MITE
Principal

## EXECUTIVE SUMMARY

NexTrans Engineering was retained by Dunpar (the 'Client') to undertake a Transportation Impact Study in support of Official Plan Amendment and Zoning By-law Amendment Applications for a proposed residential development. The subject development is located at the municipal addresses 1020, 1024, 1028, 1032 and 1042 Sixth Line Road, in the Town of Oakville. The subject development generally bounded to the east by Sixth Line Road, to the south by North Service Road and to the north by Sunny Crest Lane.

## Development Proposal

The proposed development consists of 81 residential condominium townhouse units and the retention of two single family homes at 1024 and 1028 Sixth Line Road.

## Development Access

Vehicular accesses are proposed via one main entrance and one laneway onto Sixth Line Road, with one additional emergency access proposed onto Sunny Crest Lane.

## Capacity Analysis

The development proposal is expected to generate 34 two-way auto trips ( 6 inbound and 28 outbound) during the weekday morning peak hour and 40 two-way trips ( 27 inbound and 13 outbound) during the afternoon peak hour.

Under the existing, future background and future total traffic conditions, all intersections considered in the analysis are expected to operate at acceptable levels of service with no critical movements are identified. As such, no improvements are required to accommodate the proposed improvements.

## Vehicle Parking Review

Based on the Town of Oakville's By-law 2014-014 Consolidated to April 4, 2016, a total of 162 parking spaces (including 20 visitor parking spaces) are required for the proposed development. The proposed parking supply of 179 spaces (including 20 visitor parking spaces) meets the Town of Oakville's Zoning By-law requirement.

## Transportation Demand Management Measures and Incentives

It is recommended that the applicant to implement the TDM measures and incentives identified in this report to support active transportation, public transit and meet the assumed non-auto modal split used in this report.

## Site Plan Review

AutoTURN software was used (HSU TAC-1999) to generate vehicular turning templates to confirm and demonstrate the accessibility of the proposed accesses.

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### 1.0 INTRODUCTION

NexTrans Engineering was retained by Dunpar (the 'Client') to undertake a Transportation Impact Study in support of Official Plan Amendment and Zoning By-law Amendment Applications for a proposed residential development.

The subject development is located at the municipal addresses 1020, 1024, 1028, 1032 and 1042 Sixth Line Road, in the Town of Oakville. The subject development is generally bounded to the east by Sixth Line Road, to the south by North Service Road and to the north by Sunny Crest Lane.

The location of the proposed development is illustrated in Figure 1-1.
The proposed development consists of 81 residential condominium townhouse units and the retention of two single family homes at 1024 and 1042 Sixth Line. The proposed site plan is illustrated in Figure 1-2.

Vehicular accesses are proposed via one main entrance and one laneway onto Sixth Line Road, with one additional emergency access proposed onto Sunny Crest Lane. The proposed development provides a total of 179 vehicle parking spaces, including 20 visitor parking spaces.

### 2.0 EXISTING TRAFFIC CONDITIONS

### 2.1. Existing Road Network

The existing road network, lane configuration and existing traffic control for the study area are shown in Figure 2-1. The details area described below:

- Sixth Line Road/North Service Road: is a north-south to east-west collector road under the jurisdiction of the Town of Oakville. It has two general purpose lanes and it maintains a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$ in the vicinity of the subject site.
- Rancliffe Road/Leighland Avenue: is an east-west collector road under the jurisdiction of the Town of Oakville. It has two general purpose lanes and it maintains a posted speed limit of $50 \mathrm{~km} / \mathrm{h}$.
- Sunny Crest Lane: is an existing gravel lane that services sixth existing homes.
- Germorda Drive: is an existing local road under the jurisdiction of the Town of Oakville. It has two general purpose lanes.


### 2.2. Existing Transit Network

The proposed development is located approximately 250 m (about 5-minute walk) from Route 13 Westoak Trails bus stops at the Sixth Line Road/Rancliffe Road/Leighland Avenue intersection. Route 13 Westoak Trails is currently operating between Oakville GO Train and Bronte GO Train stations. The frequency is 15 minutes during the morning and afternoon peak periods and 30 minutes frequency during the off peak periods.

Figure 2-2 illustrates the existing Bus Route 13 Westoak Trails and existing GO Train stations.

Figure 2-2 - Bus Route 13 Westoak Trails and Existing GO Train Stations


Source: Oakville Transit Website

### 2.3. Existing Active Transportation Network

## Sidewalks

Currently, there are sidewalks located on both sides of Sixth Line Road vicinity of the proposed development. However, along North Service Road, only the north side currently has sidewalk.

Leighland Avenue currently has sidewalks on both sides east of Sixth Line Road, however Rancliffe Road does not have sidewalks under the existing conditions.

Sidewalks are not currently available on Sunny Crest Lane.

## Bicycle Lanes

Currently, Sixth Line Road has dedicated bicycle lanes on both sides in the vicinity of the proposed development. The bicycle lanes end at North Service Road.

There are no dedicated bicycles on Rancliffe Road/Leighland Avenue and Sunny Crest Lane.

### 2.4. Existing Traffic Volumes

Existing traffic volumes at the study area intersections were undertaken by Spectrum on Wednesday September 21, 2016 during the morning (7:00 a.m. to 10:00 a.m.) and afternoon (4:00 p.m. to 7:00 p.m.) peak periods. Turning movement count summaries are provided in Appendix A.

### 2.5. Existing Traffic Assessment

The existing volumes are illustrated in Figure 2-3, and were analyzed using Synchro 9 software. The methodology of the software follows the procedures described and outlined in the Highway Capacity Manual, HCM 2000, published by the Transportation Research Board. The detailed results are provided in Appendix B and summarized in Table 2.1.

Table 2.1 - Level of Service - Existing Traffic Assessments

| Intersection | Key Movement | Weekday AM Peak Hour |  | Weekday PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | EB LTR | $\mathrm{A}(0.02)$ | 9 | $\mathrm{~A}(0.03)$ |
| Sixth Line Road/Rancliffe | WB LTR | $\mathrm{A}(0.19)$ | 9 | Delay (s) | LOS (v/c) |
| Relay (s) |  |  |  |  |  |
| Road/Leighland Avenue | NB LTR | $\mathrm{A}(0.06)$ | 9 | 9 |  |
| (unsignalized intersection) | SB LTR | $\mathrm{C}(0.78)$ | 22 | $\mathrm{~A}(0.21)$ | 12 |
|  | EB LR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.45)$ | 13 |
| Sixth Line Road/Sunny Crest Lane | NB LT | $\mathrm{A}(0.00)$ | 0 | 0 |  |
|  | SB TR | $\mathrm{A}(0.09)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |
| Sixth Line/Germorda Drive | EB LTR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.00)$ | 0 |
|  | WB LTR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.00)$ | 9 |
|  | NB LTR | $\mathrm{A}(0.00)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |
|  | SB LTR | $\mathrm{A}(0.00)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |

Under the existing traffic conditions, all intersections considered in the analysis are operating at acceptable levels of service with no critical movements are identified.

### 3.0 FUTURE BACKGROUND CONDITIONS

A five year horizon (2021) is selected to assess the impact of the proposed development on the existing and anticipated future road network in the area. This timeline also coincides with the completion of the proposed development.

### 3.1. Background Growth and Development Application

It is NexTrans understanding that there are no current active development applications in the immediate vicinity of the subject site. In addition, the area is a relatively stable residential neighbourhood. For the purpose of this assessment, 1.0 percent through traffic growth rate is assumed for Sixth Line Road and Rancliffe Road/Leighland Avenue.

### 3.2. Future Background Traffic Assessment

The estimated 2021 future background traffic volumes are illustrated in Figure 3-1, and were analyzed using Synchro 9 software. The detailed calculations are provided in Appendix C and summarized in Table 3-1.

Table 3.2 - Level of Service - 2021 Future Background Traffic Assessments

| Intersection | Key | Weekday AM Peak Hour |  | Weekday PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS (v/c) | Delay (s) | LOS (v/c) | Delay (s) |
| Sixth Line Road/Ranclife | EB LTR | $\mathrm{A}(0.02)$ | 9 | $\mathrm{~A}(0.03)$ | 9 |
| Road/Leighland Avenue | WB LTR | $\mathrm{A}(0.21)$ | 10 | $\mathrm{~B}(0.49)$ | 12 |
| (unsignalized intersection) | NB LTR | $\mathrm{A}(0.06)$ | 9 | $\mathrm{~B}(0.23)$ | 10 |
|  | SB LTR | $\mathrm{D}(0.83)$ | 26 | $\mathrm{~B}(0.48)$ | 13 |
| Sixth Line Road/Sunny Crest Lane | EB LR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.00)$ | 0 |
| (unsignalized intersection) | NB LT | $\mathrm{A}(0.00)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |
|  | SB TR | $\mathrm{A}(0.09)$ | 0 | $\mathrm{~A}(0.05)$ | 0 |
| Sixth Line/Germorda Drive | EB LTR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.00)$ | 0 |
|  | WB LTR | $\mathrm{A}(0.00)$ | 9 | $\mathrm{~A}(0.00)$ | 9 |
|  | NB LTR | $\mathrm{A}(0.00)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |
|  | SB LTR | $\mathrm{A}(0.00)$ | 0 | $\mathrm{~A}(0.00)$ | 0 |

Under the future background conditions, all intersections considered in the analysis are expected to operate at acceptable levels of service with no critical movements are identified.

### 4.0 SITE TRAFFIC

### 4.1. Proposed Development

The proposed development consists of 81 residential condominium townhouse units and the retention of two single family homes at 1024 and 1028 Sixth Line Road.

The 2011 Transportation Tomorrow Survey (TTS) and the Trip Generation Manual, $9^{n}$ Edition published by the Institute of Transportation Engineers (ITE) information was reviewed to estimate the modal split, trip distribution and trip generation for the proposed development.

### 4.2. Non-auto Modal Split

Table 4.1 summarizes the non-auto modal split information based on the review of the 2011 Transportation Tomorrow Survey data for Ward 5 in the Town of Oakville.

Table 4.1 - Non-Auto Modal Split based on 2011 TTS Data

| Ward |  | Trips Made by Residents of the Town of Oakville | Trips to the Town of Oakville |
| :---: | :---: | :---: | :---: |
| Ward 5 | $6-9$ AM | $18 \%$ | $17 \%$ |
|  | 24 Hours | $12 \%$ | $12 \%$ |
| Average |  | $15 \%$ | $14.5 \%$ |

Based on the information outlined in Table 4.1, the average non-auto modal split is approximately $15 \%$ for both the inbound and outbound. For the purpose of this assessment, only $5 \%$ modal split has been assumed. This assumption is reasonable given that the proposed development is only 250 m (about 5 -minute walk) from the existing transit stops at the Sixth Line Road/Rancliffe Road/Leighland Avenue intersection, and only 1.3 km from the Trafalgar Road and Oakville Place.

### 4.3. Trip Generation

The trip generation forecast was undertaken using the information contained in the Trip Generation Manual, $9^{n h}$ Edition published by the Institute of Transportation Engineers (ITE). Based on our review, the selected corresponding land use code (LUC) is: "Residential Condominium/Townhouse" (LUC 230) for the proposed development.

The summary of the vehicular trip generation is summarized in Table 4.2.
Table 4.2 - Site Traffic Trip Generation

| ITE Land Use | Magnitude | Parameter | Morning Peak |  |  | Afternoon Peak |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | In | Out | Total | In | Out | Total |
| Residential Condominium (LUC 230) | 81 units | Total Trips | 6 | 30 | 36 | 28 | 14 | 42 |
|  |  | Rate (trips/unit) | 0.07 | 0.37 | 0.44 | 0.35 | 0.17 | 0.52 |
|  |  | Non-auto mode share (5\%) | 0 | 2 | 2 | 1 | 1 | 2 |
| Total New Trips |  |  | 6 | 28 | 34 | 27 | 13 | 40 |

The development proposal is expected to generate 34 two-way auto trips ( 6 inbound and 28 outbound) during the weekday morning peak hour and 40 two-way trips ( 27 inbound and 13 outbound) during the afternoon peak hour.

It should be noted that the trips generated by the two single family homes at 1024 and 1028 Sixth Line Road are captured as part of the existing traffic turning movement counts at the intersections.

### 4.4. Trip Distribution and Assignment

The 2011 Transportation Tomorrow Survey (TTS) data was reviewed for the Town of Oakville in order to estimate the general trip distribution for the proposed residential development. Table 4.3 summarizes the general trip distribution to and from the proposed development.

Table 4.3 - Trip Assignment

| Direction | To the Town of Oakville | From the Town of Oakville |
| :---: | :---: | :---: |
| Oakville | $56 \%$ | $58 \%$ |
| Burlington | $12 \%$ | $6 \%$ |
| Peel Region | $15 \%$ | $21 \%$ |
| Toronto | $4 \%$ | $9 \%$ |
| Hamiton Area | $8 \%$ | $2 \%$ |
| Others | $5 \%$ | $4 \%$ |
| Total | $100 \%$ | $100 \%$ |

Table 4.4 summarizes the trip assignment for the proposed development based on the 2011 TTS information outlined in Table 4.3 and the assessment of the existing road network.

Table 4.4 - Trip Assignment

| Direction | Street Name | To/From Proposed Development |
| :---: | :---: | :---: |
| East/West | Leighland Avenue | $20 \%$ |
|  | North Service Road | $55 \%$ |
| North/South | Sixth Line Road | $25 \%$ |
| Total |  |  |

Figure 4-1 illustrates the site trip assignment, with Figure 4-2 illustrating the site generated traffic volumes.

### 5.0 FUTURE TOTAL TRAFFIC CONDITIONS

### 5.1. Future Total Traffic Assessment

The estimated 2021 future total traffic volumes (future background traffic volumes plus site generated traffic volumes) are illustrated in Figure 5-1, and were analyzed using Synchro 9 software. The detailed calculations are provided in Appendix D and summarized in Table 5.1.

Table 5.1 - Level of Service - 2021 Future Total Traffic Assessments

| Intersection | Key Movement | Weekday AM Peak Hour |  | Weekday PM Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | LOS (v/c) | Delay (s) | LOS (v/c) | Delay (s) |
| Sixth Line Road/Rancliffe Road/Leighland Avenue (unsignalized intersection) | EB LTR | A (0.02) | 9 | A (0.03) | 9 |
|  | WB LTR | A (0.21) | 10 | B (0.50) | 12 |
|  | NB LTR | A (0.10) | 9 | B (0.24) | 10 |
|  | SB LTR | D (0.84) | 27 | B (0.50) | 14 |
| Sixth Line Road/Sunny Crest Lane (unsignalized intersection) | EB LR | A (0.00) | 10 | A (0.00) | 0 |
|  | NB LT | A (0.00) | 0 | A (0.00) | 0 |
|  | SB TR | A (0.10) | 0 | A (0.05) | 0 |
| Sixth Line/Germorda Drive (unsignalized intersection) | WB LTR | A (0.00) | 9 | A (0.00) | 9 |
|  | NB LTR | A (0.03) | 0 | A (0.10) | 0 |
|  | SB LTR | A (0.00) | 0 | A (0.00) | 0 |
| Sixth Line Road/Site Access 1 (unsignalized intersection) | EB LR | A (0.03) | 0 | A (0.01) | 9 |
|  | NB LT | A (0.00) | 1 | A (0.01) | 1 |
|  | SB TR | A (0.08) | 0 | A (0.05) | 0 |
| Sixth Line Road/Site Access 2 (unsignalized intersection) | EB LR | A (0.01) | 9 | A (0.00) | 10 |
|  | NB LT | A (0.00) | 0 | A (0.00) | 0 |
|  | SB TR | A (0.08) | 0 | A (0.05) | 0 |

Under the future total conditions, all intersections considered in the analysis are expected to operate at acceptable levels of service with no critical movements are identified. No additional improvements are required to accommodate the proposed development.

### 5.2. Proposed Development Access

Based on the intersection capacity analysis results outlined in Table 5-1, the proposed development accesses onto Sixth Line Road are expected to operate at acceptable levels of service.

### 5.3. Active Transportation Assessment

## Sidewalks

Under the existing conditions, there are sidewalks located on both sides of Sixth Line Road vicinity of the proposed development. However, along North Service Road, only the north side currently has sidewalk. It is NexTrans understanding that the proposed development provides direct sidewalk connections from the proposed development to connect with the existing sidewalks via the proposed main entrance onto Sixth Line Road.

The existing sidewalks along the west side of Sixth Line Road will be relocated away from the curb along the frontage of the proposed development to provide more buffer between pedestrians, bicycles and automobiles. This is an improvement given that the existing sidewalk on the west side of Sixth Line Road is located adjacent to the pavement.

It is our understanding that sidewalks will be provided as part of the road network within the proposed development to facilitate active transportation modes.

## Bicycle Lanes

Under the existing conditions, Sixth Line Road has dedicated bicycle lanes on both sides in the vicinity of the proposed development. The bicycle lanes end at North Service Road. Ideally, the bicycle lanes should continue on North Service Road and connect to Trafalgar Road. This provision will provide the residents with option to ride their bicycles to go shopping or run errands. However, this provision is beyond the scope of this development. It is recommended that the Town of Oakville should consider this provision in the future to promote sustainable modes of transportation in the Town.

The proposed development is located approximately 1.3 km from Oakville Place and Trafalgar Road. Based on an assumed walking speed of $1.2 \mathrm{~m} / \mathrm{s}$, it would take approximately 18 minutes from the proposed development to these locations on foot, and about 6 minutes by bicycle (assumed bicycle speed of $3 \mathrm{~m} / \mathrm{s}$ ).

### 5.4. Public Transit Assessment

The proposed development is located approximately 250 m (about 5-minute walk) from Route 13 Westoak Trails bus stops at the Sixth Line Road/Rancliffe Road/Leighland Avenue intersection. Route 13 Westoak Trails is currently operating between Oakville GO Train and Bronte GO Train stations. The frequency is 15 minutes during the morning and afternoon peak periods and 30 minutes frequency during the off peak periods.

As part of electrification project, Metrolinx is expanding GO Transit to enable 15-minute service along the Lakeshore West Corridor from Strachan Avenue to Burlington with electrified trains that provide faster and more frequent service. This service will allow the existing and future residents to take up more transit trips to go to work or for discretionary trips to other parts of GTHA. It is anticipated that the non-auto modal split will grow from the existing $15 \%$ to $20 \%$ or more in the future.

### 6.0 SITE PLAN REVIEW

AutoTURN software was used (HSU TAC-1999) to generate vehicular turning templates to confirm and demonstrate the accessibility of the proposed accesses. These templates are illustrated in Figure 6-1.

### 7.0 PARKING ASSESSMENT

The Town of Oakville's By-law 2014-014 Consolidated to April 4, 2016 parking requirement and supply for the proposed development is summarized in Table 7.1.

Table 7.1 - Town of Oakville By-law Vehicle Parking Requirements

| Land Use | Type | No. of Unit/GFA | Parking Rates | Parking <br> Requirement | Parking <br> Supply |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Townhouse <br> dwelling | Visitor | 81 units | 0.25 spaces/unit | 20 | 179 |
|  | Resident | 81 units | 2.0 spaces/unit | 162 |  |

Based on the Town of Oakville's By-law 2014-014 Consolidated to April 4, 2016, a total of 162 parking spaces (including 20 visitor parking spaces) are required for the proposed development. The proposed parking supply of 179 spaces (including 20 visitor parking spaces) meets the Town of Oakville's Zoning By-law requirement.

### 8.0 TRANSPORTATION DEMAND MANAGEMENT

Transportation Demand Management (TDM) is a co-ordinated series of actions aimed at maximizing the people moving capability of the transportation system. Intended to reduce single-occupant auto use, potential TDM measures include: TDM supportive land use, bicycle and pedestrian programs and facilities, public transit improvements, preferential treatments for buses and ridesharing, where appropriate.

The following TDM measures and incentives are recommended for the proposed residential development:

- Provide direct shared pedestrian and cycling connections from the proposed development to Sixth Line Road;
- Provide information package for new residents. The information package includes GO Train schedules, Oakville Transit bus route schedules, community and cycling maps, where appropriate. The Information Package can be distributed at the sale office.
- Provide pre-load PRESTO Cards with the starting value of $\$ 25$ (inclusive of the registration fee) to the residents on demand basis. This will help the future residents to consider taking GO Train and Oakville Transit as an alternative mode of transportation. The pre-loaded PRESTO Cards can be distributed in conjunction with the Information Package at the time of purchase or at occupancy.


### 9.0 CONCLUSIONS / FINDINGS

The findings and conclusions of our analysis are as follows:

- The proposed development consists of 81 residential condominium townhouse units and the retention of two single family homes at 1024 and 1042 Sixth Line Road.
- Vehicular accesses are proposed via one main entrance and one laneway onto Sixth Line Road, with one additional emergency access proposed onto Sunny Crest Lane. Based on the intersection capacity analysis, the proposed development accesses are expected to operate at acceptable levels of service.
- The development proposal is expected to generate 34 two-way auto trips (6 inbound and 28 outbound) during the weekday morning peak hour and 40 two-way trips ( 27 inbound and 13 outbound) during the afternoon peak hour.
- Based on the Town of Oakville's By-law 2014-014 Consolidated to April 4, 2016, a total of 162 parking spaces (including 20 visitor parking spaces) are required for the proposed development. The proposed parking supply of 179 spaces (including 20 visitor parking spaces) meets the Town of Oakville's Zoning Bylaw requirement.
- Under the existing, future background and future total traffic conditions, all intersections considered in the analysis are expected to operate at acceptable levels of service with no critical movements are identified. As such, no improvements are required to accommodate the proposed development.
- It is recommended that the proposed development provide and implement the proposed Transportation Demand Management measures and incentives suggested in this report.



Figure 1-2
nexllirans
Proposed Site Plan
ENGINEERING

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# Appendix A Existing Traffic Data 

## Turning Movement Count (1. RANCLIFFE RD \& 6TH LINE)

| Start Time | N Approach 6TH LINE |  |  |  |  | E Approach RANCLIFFE RD |  |  |  |  | S Approach 6TH LINE |  |  |  |  | W Approach RANCLIFFE RD |  |  |  |  | Int. Total ( 15 min ) | Int. Total ( 1 hr ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right <br> $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | $\begin{aligned} & \text { Left } \\ & \mathrm{N}: \end{aligned}$ | $\begin{aligned} & \text { Peds } \\ & \text { N: } \end{aligned}$ | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { E:N } \end{aligned}$ | Thru <br> E:W | $\begin{aligned} & \text { Left } \\ & \mathrm{E}: \mathrm{S} \end{aligned}$ | Peds E: | Approach Total | Right S:E | $\begin{aligned} & \text { Thru } \\ & \text { S:N } \end{aligned}$ | $\begin{aligned} & \text { Left } \\ & \mathrm{S}: \mathrm{W} \end{aligned}$ | $\begin{aligned} & \text { Peds } \\ & \text { S: } \end{aligned}$ | Approach Total | Right w: s | Thru <br> W:E | $\begin{aligned} & \text { Left } \\ & \mathrm{W}: \mathrm{N} \end{aligned}$ | Peds W: | Approach Total |  |  |
| 07:00:00 | 1 | 7 | 81 | 1 | 89 | 14 | 0 | 0 | 0 | 14 | 3 | 5 | 1 | 0 | 9 | 0 | 1 | 0 | 2 | 1 | 113 |  |
| 07:15:00 | 0 | 18 | 106 | 0 | 124 | 19 | 0 | 0 | 0 | 19 | 0 | 1 | 1 | 2 | 2 | 1 | 0 | 0 | 2 | 1 | 146 |  |
| 07:30:00 | 0 | 32 | 90 | 0 | 122 | 23 | 0 | 1 | 0 | 24 | 0 | 3 | 0 | 1 | 3 | 0 | 3 | 0 | 0 | 3 | 152 |  |
| 07:45:00 | 0 | 25 | 129 | 0 | 154 | 18 | 0 | 1 | 0 | 19 | 0 | 3 | 0 | 0 | 3 | 0 | 3 | 1 | 2 | 4 | 180 | 591 |
| 08:00:00 | 1 | 20 | 98 | 0 | 119 | 32 | 2 | 1 | 0 | 35 | 0 | 10 | 0 | 0 | 10 | 1 | 1 | 2 | 0 | 4 | 168 | 646 |
| 08:15:00 | 0 | 37 | 108 | 3 | 145 | 26 | 1 | 1 | 3 | 28 | 0 | 3 | 0 | 1 | 3 | 1 | 0 | 2 | 1 | 3 | 179 | 679 |
| 08:30:00 | 0 | 23 | 104 | 1 | 127 | 19 | 1 | 0 | 2 | 20 | 1 | 2 | 0 | 0 | 3 | 0 | 3 | 1 | 1 | 4 | 154 | 681 |
| 08:45:00 | 0 | 18 | 91 | 0 | 109 | 25 | 1 | 2 | 1 | 28 | 1 | 7 | 0 | 0 | 8 | 0 | 2 | 0 | 0 | 2 | 147 | 648 |
| 09:00:00 | 0 | 14 | 51 | 0 | 65 | 25 | 0 | 0 | 0 | 25 | 3 | 5 | 0 | 0 | 8 | 1 | 1 | 0 | 0 | 2 | 100 | 580 |
| 09:15:00 | 0 | 14 | 54 | 0 | 68 | 19 | 0 | 1 | 1 | 20 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 90 | 491 |
| 09:30:00 | 0 | 13 | 65 | 2 | 78 | 11 | 2 | 1 | 1 | 14 | 1 | 5 | 0 | 0 | 6 | 0 | 0 | 1 | 2 | 1 | 99 | 436 |
| 09:45:00 | 1 | 12 | 63 | 0 | 76 | 21 | 0 | 3 | 0 | 24 | 4 | 7 | 2 | 0 | 13 | 1 | 0 | 0 | 2 | 1 | 114 | 403 |


| 16:00:00 | 1 | 11 | 31 | 1 | 43 | 58 | 2 | 0 | 1 | 60 | 1 | 21 | 0 | 0 | 22 | 0 | 1 | 3 | 0 | 4 | 129 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15:00 | 1 | 14 | 42 | 2 | 57 | 43 | 1 | 2 | 1 | 46 | 0 | 19 | 0 | 0 | 19 | 1 | 0 | 1 | 1 | 2 | 124 |  |
| 16:30:00 | 0 | 10 | 50 | 0 | 60 | 71 | 2 | 4 | 0 | 77 | 1 | 27 | 1 | 1 | 29 | 1 | 3 | 3 | 1 | 7 | 173 |  |
| 16:45:00 | 0 | 13 | 26 | 0 | 39 | 71 | 0 | 2 | 1 | 73 | 1 | 24 | 1 | 1 | 26 | 0 | 0 | 0 | 1 | 0 | 138 | 564 |
| 17:00:00 | 0 | 13 | 34 | 0 | 47 | 60 | 1 | 3 | 0 | 64 | 1 | 31 | 1 | 0 | 33 | 2 | 0 | 0 | 0 | 2 | 146 | 581 |
| 17:15:00 | 0 | 12 | 64 | 0 | 76 | 87 | 0 | 1 | 0 | 88 | 1 | 35 | 0 | 0 | 36 | 0 | 1 | 1 | 2 | 2 | 202 | 659 |
| 17:30:00 | 1 | 16 | 41 | 2 | 58 | 74 | 0 | 1 | 1 | 75 | 1 | 34 | 0 | 0 | 35 | 0 | 0 | 1 | 3 | 1 | 169 | 655 |
| 17:45:00 | 2 | 17 | 37 | 1 | 56 | 89 | 0 | 1 | 0 | 90 | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 1 | 1 | 1 | 173 | 690 |
| 18:00:00 | 3 | 14 | 60 | 0 | 78 | 65 | 6 | 4 | 1 | 75 | 2 | 30 | 1 | 1 | 33 | 3 | 2 | 0 | 1 | 5 | 191 | 735 |
| 18:15:00 | 4 | 17 | 42 | 0 | 63 | 70 | 0 | 1 | 0 | 71 | 2 | 27 | 2 | 0 | 31 | 0 | 0 | 3 | 0 | 3 | 168 | 701 |
| 18:30:00 | 1 | 18 | 48 | 2 | 67 | 67 | 1 | 1 | 3 | 69 | 0 | 13 | 0 | 0 | 13 | 1 | 2 | 1 | 2 | 4 | 153 | 685 |
| 18:45:00 | 1 | 9 | 51 | 0 | 61 | 37 | 1 | 0 | 1 | 38 | 3 | 21 | 0 | 2 | 24 | 1 | 1 | 0 | 0 | 2 | 125 | 637 |
| Grand Total | 17 | 397 | 1566 | 15 | 1981 | 1044 | 21 | 31 | 17 | 1096 | 27 | 360 | 10 | 9 | 397 | 14 | 24 | 21 | 25 | 59 | 3533 | - |
| Approach\% | 0.9\% | 20\% | 79.1\% |  | - | 95.3\% | 1.9\% | 2.8\% |  | - | 6.8\% | 90.7\% | 2.5\% |  | - | 23.7\% | 40.7\% | 35.6\% |  | - | - | - |
| Totals \% | 0.5\% | 11.2\% | 44.3\% |  | 56.1\% | 29.5\% | 0.6\% | 0.9\% |  | $31 \%$ | 0.8\% | 10.2\% | 0.3\% |  | 11.2\% | 0.4\% | 0.7\% | 0.6\% |  | 1.7\% | - | - |
| Heavy | 0 | 4 | 30 |  | - | 28 | 1 | 0 |  | - | 0 | 7 | 0 |  | - | 0 | 1 | 0 |  | - | - | - |
| Heavy \% | 0\% | 1\% | 1.9\% |  | - | 2.7\% | 4.8\% | 0\% |  | - | 0\% | 1.9\% | 0\% |  | - | 0\% | 4.2\% | 0\% |  | - | - | - |
| Bicycles | 0 | 49 | 1 |  | - | 1 | 1 | 0 |  | - | 1 | 39 | 0 |  | - | 1 | 0 | 0 |  | - | - | - |
| Bicycle \% ing Moveme | 0\% Count | 12.3\% | 0.1\% |  | - | 0.1\% | 4.8\% | 0\% |  | - | 3.7\% | $6^{10.8 \%}$ | 0\% |  | - | 7.1\% | 0\% | 0\% |  | - | - | NXT16E7Z |


| Start Time | Peak Hour: 07:45 AM - 08:45 AM |  |  |  |  |  |  |  |  |  | Weather: Clear (12.7 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | N Approach 6TH LINE |  | Approach Total | Right | Thru | E Approach RANCLIFFE RD |  | Approach Total | Right | Thru | S Approach 6TH LINE |  | Approach Total | Right | Thru | W Approach RANCLIFFE RD |  | Approach Total | Int. Total ( 15 min ) |
|  |  |  | Left | Peds |  |  |  | Left | Peds |  |  |  | Left | Peds |  |  |  | Left | Peds |  |  |
| 07:45:00 | 0 | 25 | 129 | 0 | 154 | 18 | 0 | 1 | 0 | 19 | 0 | 3 | 0 | 0 | 3 | 0 | 3 | 1 | 2 | 4 | 180 |
| 08:00:00 | 1 | 20 | 98 | 0 | 119 | 32 | 2 | 1 | 0 | 35 | 0 | 10 | 0 | 0 | 10 | 1 | 1 | 2 | 0 | 4 | 168 |
| 08:15:00 | 0 | 37 | 108 | 3 | 145 | 26 | 1 | 1 | 3 | 28 | 0 | 3 | 0 | 1 | 3 | 1 | 0 | 2 | 1 | 3 | 179 |
| 08:30:00 | 0 | 23 | 104 | 1 | 127 | 19 | 1 | 0 | 2 | 20 | 1 | 2 | 0 | 0 | 3 | 0 | 3 | 1 | 1 | 4 | 154 |
| Grand Total | 1 | 105 | 439 | 4 | 545 | 95 | 4 | 3 | 5 | 102 | 1 | 18 | 0 | 1 | 19 | 2 | 7 | 6 | 4 | 15 | 681 |
| Approach\% | 0.2\% | 19.3\% | 80.6\% |  | - | 93.1\% | 3.9\% | 2.9\% |  | - | 5.3\% | 94.7\% | 0\% |  | - | 13.3\% | 46.7\% | 40\% |  | - | - |
| Totals \% | 0.1\% | 15.4\% | 64.5\% |  | 80\% | 14\% | 0.6\% | 0.4\% |  | 15\% | 0.1\% | 2.6\% | 0\% |  | 2.8\% | 0.3\% | 1\% | 0.9\% |  | 2.2\% | - |
| PHF | 0.25 | 0.71 | 0.85 |  | 0.88 | 0.74 | 0.5 | 0.75 |  | 0.73 | 0.25 | 0.45 | 0 |  | 0.48 | 0.5 | 0.58 | 0.75 |  | 0.94 | - |
| Heavy | 0 | 0 | 10 |  | 10 | 5 | 0 | 0 |  | 5 | 0 | 2 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0\% | 2.3\% |  | 1.8\% | 5.3\% | 0\% | 0\% |  | 4.9\% | 0\% | 11.1\% | 0\% |  | 10.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 1 | 105 | 429 |  | 535 | 90 | 4 | 3 |  | 97 | 1 | 16 | 0 |  | 17 | 2 | 7 | 6 |  | 15 | - |
| Lights \% | 100\% | 100\% | 97.7\% |  | 98.2\% | 94.7\% | 100\% | 100\% |  | 95.1\% | 100\% | 88.9\% | 0\% |  | 89.5\% | 100\% | 100\% | 100\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 0 | 4 |  | 4 | 1 | 0 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0.9\% |  | 0.7\% | 1.1\% | 0\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 0 | 6 |  | 6 | 4 | 0 | 0 |  | 4 | 0 | 2 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0\% | 1.4\% |  | 1.1\% | 4.2\% | 0\% | 0\% |  | 3.9\% | 0\% | 11.1\% | 0\% |  | 10.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 4 | - | - | - | - | 5 | - | - | - | - | 1 | - | - | - | - | 3 | - | - |
| Pedestrians\% | - | - | - | 28.6\% |  | - | - | - | 35.7\% |  | - | - | - | 7.1\% |  | - | - | - | 21.4\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 7.1\% |  | - |
| Bicycles on Road | 0 | 19 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 2 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 05:15 PM - 06:15 PM Weather: Mostly Cloudy ( $25.2{ }^{\circ} \mathrm{C}$ )

| Start Time | N Approach 6TH LINE |  |  |  |  | E Approach RANCLIFFE RD |  |  |  |  | S Approach 6TH LINE |  |  |  |  | w Approach RANCLIFFE RD |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total |  |
| 17:15:00 | 0 | 12 | 64 | 0 | 76 | 87 | 0 | 1 | 0 | 88 | 1 | 35 | 0 | 0 | 36 | 0 | 1 | 1 | 2 | 2 | 202 |
| 17:30:00 | 1 | 16 | 41 | 2 | 58 | 74 | 0 | 1 | 1 | 75 | 1 | 34 | 0 | 0 | 35 | 0 | 0 | 1 | 3 | 1 | 169 |
| 17:45:00 | 2 | 17 | 37 | 1 | 56 | 89 | 0 | 1 | 0 | 90 | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 1 | 1 | 1 | 173 |
| 18:00:00 | 3 | 14 | 60 | 0 | 78 | 65 | 6 | 4 | 1 | 75 | 2 | 30 | 1 | 1 | 33 | 3 | 2 | 0 | 1 | 5 | 191 |
| Grand Total | 6 | 59 | 202 | 3 | 268 | 315 | 6 | 7 | 2 | 328 | 4 | 125 | 1 | 1 | 130 | 3 | 3 | 3 | 7 | 9 | 735 |
| Approach\% | 2.2\% | 22\% | 75.4\% |  | - | 96\% | 1.8\% | 2.1\% |  | - | 3.1\% | 96.2\% | 0.8\% |  | - | 33.3\% | 33.3\% | 33.3\% |  | - | - |
| Totals \% | 0.8\% | 8\% | 27.5\% |  | 36.5\% | 42.9\% | 0.8\% | 1\% |  | 44.6\% | 0.5\% | 17\% | 0.1\% |  | 17.7\% | 0.4\% | 0.4\% | 0.4\% |  | 1.2\% | - |
| PHF | 0.5 | 0.87 | 0.79 |  | 0.86 | 0.88 | 0.25 | 0.44 |  | 0.91 | 0.5 | 0.89 | 0.25 |  | 0.9 | 0.25 | 0.38 | 0.75 |  | 0.45 | - |
| Heavy | 0 | 0 | 3 |  | 3 | 4 | 0 | 0 |  | 4 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0\% | 1.5\% |  | 1.1\% | 1.3\% | 0\% | 0\% |  | 1.2\% | 0\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 6 | 59 | 199 |  | 265 | 311 | 6 | 7 |  | 324 | 4 | 124 | 1 |  | 129 | 3 | 3 | 3 |  | 9 | - |
| Lights \% | 100\% | 100\% | 98.5\% |  | 98.9\% | 98.7\% | 100\% | 100\% |  | 98.8\% | 100\% | 99.2\% | 100\% |  | 99.2\% | 100\% | 100\% | 100\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 0 | 3 |  | 3 | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0\% | 1.5\% |  | 1.1\% | 1.3\% | 0\% | 0\% |  | 1.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 2 | - | - | - | - | 2 | - | - | - | - | 0 | - | - | - | - | 6 | - | - |
| Pedestrians\% | - | - | - | 15.4\% |  | - | - | - | 15.4\% |  | - | - | - | 0\% |  | - | - | - | 46.2\% |  | - |
| Bicycles on Crosswalk | - | - | - | 1 | - | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 7.7\% |  | - | - | - | 0\% |  | - | - | - | 7.7\% |  | - | - | - | 7.7\% |  | - |
| Bicycles on Road | 0 | 3 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 10 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 07:45 AM - 08:45 AM Weather: Clear $\left(12.7^{\circ} \mathrm{C}\right)$



Peak Hour: 05:15 PM - 06:15 PM Weather: Mostly Cloudy ( $25.2^{\circ} \mathrm{C}$ )


## Turning Movement Count (3.6TH LINE \& GERMORDA DR)

|  | N Approach 6TH LINE |  |  |  |  | E Approach GERMORDA DR |  |  |  |  | S Approach 6TH LINE |  |  |  |  | W Approach LANEWAY |  |  |  |  | Int. Total ( 15 min ) | Int. Total ( 1 hr ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right <br> $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | $\begin{aligned} & \text { Left } \\ & \mathrm{N}: \mathrm{E} \end{aligned}$ | $\begin{aligned} & \text { Peds } \\ & \mathrm{N}: \end{aligned}$ | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { F:N } \end{aligned}$ | Thru E:W | Left <br> E:S | Peds $\mathrm{E}:$ | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { S:E } \end{aligned}$ | $\begin{aligned} & \text { Thrur } \\ & \text { St } \end{aligned}$ | $\begin{aligned} & \text { Left } \\ & \text { S:W } \end{aligned}$ | Peds $\mathrm{s}:$ | Approach Total | Right W:S | Thru W: E | $\begin{aligned} & \text { Left } \\ & \mathrm{W}: \mathrm{N} \end{aligned}$ | Peds W: | Approach Total |  |  |
| 07:00:00 | 0 | 8 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 15 |  |
| 07:15:00 | 0 | 19 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 21 |  |
| 07:30:00 | 0 | 28 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 32 |  |
| 07:45:00 | 0 | 24 | 0 | 0 | 24 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 27 | 95 |
| 08:00:00 | 0 | 23 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 2 | 0 | 33 | 113 |
| 08:15:00 | 0 | 39 | 0 | 0 | 39 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 0 | 7 | 1 | 43 | 135 |
| 08:30:00 | 0 | 22 | 1 | 0 | 23 | 1 | 0 | 0 | 2 | 1 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 2 | 0 | 28 | 131 |
| 08:45:00 | 0 | 19 | 0 | 0 | 19 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 1 | 0 | 24 | 128 |
| 09:00:00 | 0 | 15 | 0 | 0 | 15 | 1 | 0 | 1 | 1 | 2 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 22 | 117 |
| 09:15:00 | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 1 | 0 | 16 | 90 |
| 09:30:00 | 0 | 14 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 3 | 0 | 19 | 81 |
| 09:45:00 | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 0 | 1 | 0 | 2 | 9 | 0 | 0 | 11 | 0 | 0 | 0 | 1 | 0 | 24 | 81 |


| **BREAK***********) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:00:00 | 0 | 6 | 1 | 0 | 7 | 0 | 0 | 0 | 1 | 0 | 1 | 21 | 0 | 0 | 22 | 0 | 0 | 0 | 1 | 0 | 29 |  |
| 16:15:00 | 0 | 17 | 0 | 1 | 17 | 0 | 0 | 1 | 2 | 1 | 0 | 20 | 0 | 1 | 20 | 0 | 0 | 0 | 1 | 0 | 38 |  |
| 16:30:00 | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 0 | 1 | 0 | 39 |  |
| 16:45:00 | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 1 | 0 | 1 | 1 | 27 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 42 | 148 |
| 17:00:00 | 0 | 15 | 1 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 1 | 35 | 0 | 0 | 37 | 0 | 0 | 0 | 4 | 0 | 53 | 172 |
| 17:15:00 | 0 | 14 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 1 | 34 | 0 | 0 | 35 | 0 | 0 | 0 | 2 | 0 | 49 | 183 |
| 17:30:00 | 0 | 15 | 0 | 0 | 15 | 0 | 0 | 0 | 2 | 0 | 0 | 35 | 0 | 0 | 35 | 0 | 0 | 0 | 3 | 0 | 50 | 194 |
| 17:45:00 | 0 | 19 | 1 | 0 | 20 | 1 | 0 | 0 | 0 | 1 | 2 | 25 | 0 | 0 | 27 | 0 | 0 | 0 | 4 | 0 | 48 | 200 |
| 18:00:00 | 0 | 14 | 2 | 0 | 16 | 0 | 0 | 0 | 5 | 0 | 0 | 31 | 0 | 1 | 31 | 0 | 0 | 0 | 2 | 0 | 47 | 194 |
| 18:15:00 | 0 | 18 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 0 | 30 | 0 | 0 | 0 | 3 | 0 | 48 | 193 |
| 18:30:00 | 0 | 16 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 1 | 12 | 0 | 0 | 13 | 0 | 0 | 0 | 7 | 0 | 30 | 173 |
| 18:45:00 | 0 | 12 | 0 | 0 | 12 | 2 | 0 | 0 | 1 | 2 | 1 | 25 | 0 | 0 | 26 | 0 | 0 | 0 | 2 | 0 | 40 | 165 |
| Grand Total | 0 | 409 | 6 | 1 | 416 | 6 | 0 | 5 | 18 | 11 | 11 | 377 | 0 | 3 | 389 | 1 | 0 | 0 | 49 | 1 | 817 | - |
| Approach\% | 0\% | 98.3\% | 1.4\% |  | - | 54.5\% | 0\% | 45.5\% |  | - | 2.8\% | 96.9\% | 0\% |  | - | 100\% | 0\% | 0\% |  | - | - | - |
| Totals \% | 0\% | 50.1\% | 0.7\% |  | 50.9\% | 0.7\% | 0\% | 0.6\% |  | 1.3\% | 1.3\% | 46.1\% | 0\% |  | 47.6\% | 0.1\% | 0\% | 0\% |  | 0.1\% | - | - |
| Heavy | 0 | 4 | 1 |  | - | 1 | 0 | 0 |  | - | 0 | 5 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Heavy \% | 0\% | 1\% | 16.7\% |  | - | 16.7\% | 0\% | 0\% |  | - | 0\% | 1.3\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |
| Bicycles | 0 | 27 | 1 |  | - | 0 | 0 | 0 |  | - | 1 | 33 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Bicycle \% urning Moveme | 0\% Count | 6.6\% | 16.7\% |  | - | 0\% | 0\% | 0\% |  | - | $\begin{aligned} & 9.1 \% \\ & 1 \text { of } 6 \end{aligned}$ | 8.8\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | NXT16E7Z |

Peak Hour: 07:30 AM - 08:30 AM Weather: Clear (12.7 ${ }^{\circ} \mathrm{C}$ )

| Start Time | N Approach 6TH LINE |  |  |  |  | E Approach GERMORDA DR |  |  |  |  | S Approach 6TH LINE |  |  |  |  | W Approach LANEWAY |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total |  |
| 07:30:00 | 0 | 28 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 32 |
| 07:45:00 | 0 | 24 | 0 | 0 | 24 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 27 |
| 08:00:00 | 0 | 23 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 10 | 0 | 0 | 0 | 2 | 0 | 33 |
| 08:15:00 | 0 | 39 | 0 | 0 | 39 | 0 | 0 | 1 | 1 | 1 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 0 | 7 | 1 | 43 |
| Grand Total | 0 | 114 | 0 | 0 | 114 | 1 | 0 | 1 | 1 | 2 | 0 | 18 | 0 | 0 | 18 | 1 | 0 | 0 | 11 | 1 | 135 |
| Approach\% | 0\% | 100\% | 0\% |  | - | 50\% | 0\% | 50\% |  | - | 0\% | 100\% | 0\% |  | - | 100\% | 0\% | 0\% |  | - | - |
| Totals \% | 0\% | 84.4\% | 0\% |  | 84.4\% | 0.7\% | 0\% | 0.7\% |  | 1.5\% | 0\% | 13.3\% | 0\% |  | 13.3\% | 0.7\% | 0\% | 0\% |  | 0.7\% | - |
| PHF | 0 | 0.73 | 0 |  | 0.73 | 0.25 | 0 | 0.25 |  | 0.5 | 0 | 0.45 | 0 |  | 0.45 | 0.25 | 0 | 0 |  | 0.25 | - |
| Heavy | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0.9\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 5.6\% | 0\% |  | 5.6\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 0 | 113 | 0 |  | 113 | 1 | 0 | 1 |  | 2 | 0 | 17 | 0 |  | 17 | 1 | 0 | 0 |  | 1 | - |
| Lights \% | 0\% | 99.1\% | 0\% |  | 99.1\% | 100\% | 0\% | 100\% |  | 100\% | 0\% | 94.4\% | 0\% |  | 94.4\% | 100\% | 0\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0.9\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 5.6\% | 0\% |  | 5.6\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - | - | - | 5 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 8.3\% |  | - | - | - | 0\% |  | - | - | - | 41.7\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 6 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 50\% |  | - |
| Bicycles on Road | 0 | 11 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 3 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 05:00 PM - 06:00 PM Weather: Mostly Cloudy ( $25.2^{\circ} \mathrm{C}$ )

| Start Time | N Approach 6TH LINE |  |  |  |  | E Approach GERMORDA DR |  |  |  |  | S Approach 6TH LINE |  |  |  |  | W Approach LANEWAY |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total | Right | Thru | Left | Peds | Approach Total |  |
| 17:00:00 | 0 | 15 | 1 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 1 | 35 | 0 | 0 | 37 | 0 | 0 | 0 | 4 | 0 | 53 |
| 17:15:00 | 0 | 14 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 1 | 34 | 0 | 0 | 35 | 0 | 0 | 0 | 2 | 0 | 49 |
| 17:30:00 | 0 | 15 | 0 | 0 | 15 | 0 | 0 | 0 | 2 | 0 | 0 | 35 | 0 | 0 | 35 | 0 | 0 | 0 | 3 | 0 | 50 |
| 17:45:00 | 0 | 19 | 1 | 0 | 20 | 1 | 0 | 0 | 0 | 1 | 2 | 25 | 0 | 0 | 27 | 0 | 0 | 0 | 4 | 0 | 48 |
| Grand Total | 0 | 63 | 2 | 0 | 65 | 1 | 0 | 0 | 2 | 1 | 4 | 129 | 0 | 0 | 134 | 0 | 0 | 0 | 13 | 0 | 200 |
| Approach\% | 0\% | 96.9\% | 3.1\% |  | - | 100\% | 0\% | 0\% |  | - | 3\% | 96.3\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - |
| Totals \% | 0\% | 31.5\% | 1\% |  | 32.5\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 2\% | 64.5\% | 0\% |  | 67\% | 0\% | 0\% | 0\% |  | 0\% | - |
| PHF | 0 | 0.83 | 0.5 |  | 0.81 | 0.25 | 0 | 0 |  | 0.25 | 0.5 | 0.92 | 0 |  | 0.91 | 0 | 0 | 0 |  | 0 | - |
| Heavy | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.8\% | 0\% |  | 0.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 0 | 63 | 2 |  | 65 | 1 | 0 | 0 |  | 1 | 4 | 128 | 0 |  | 133 | 0 | 0 | 0 |  | 0 | - |
| Lights \% | 0\% | 100\% | 100\% |  | 100\% | 100\% | 0\% | 0\% |  | 100\% | 100\% | 99.2\% | 0\% |  | 99.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Single-Unit Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.8\% | 0\% |  | 0.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 2 | - | - | - | - | 0 | - | - | - | - | 5 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 13.3\% |  | - | - | - | 0\% |  | - | - | - | 33.3\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 8 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 53.3\% |  | - |
| Bicycles on Road | 0 | 2 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 1 | 12 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 07:30 AM - 08:30 AM Weather: Clear $\left(12.7^{\circ} \mathrm{C}\right)$



Peak Hour: 05:00 PM - 06:00 PM Weather: Mostly Cloudy ( $25.2^{\circ} \mathrm{C}$ )


## Turning Movement Count (2 . SUNNYCREST LN \& 6TH LINE)

| Start Time | N Approach 6TH LINE |  |  |  | S Approach 6TH LINE |  |  |  | W Approach SUNNYCREST LN |  |  |  | Int. Total (15 min) | Int. Total (1 hr) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | Peds N : | Approach Total | $\begin{aligned} & \text { Thru } \\ & \text { S:N } \end{aligned}$ | $\begin{aligned} & \text { Left } \\ & \text { S:W } \end{aligned}$ | $\begin{gathered} \text { Peds } \\ \mathrm{S}: \end{gathered}$ | Approach Total | Right W:S | $\begin{aligned} & \text { Left } \\ & \mathrm{W}: \mathrm{N} \end{aligned}$ | Peds W: | Approach Total |  |  |
| 07:00:00 | 0 | 8 | 0 | 8 | 7 | 0 | 0 | 7 | 0 | 0 | 2 | 0 | 15 |  |
| 07:15:00 | 0 | 19 | 0 | 19 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 21 |  |
| 07:30:00 | 0 | 31 | 0 | 31 | 4 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 35 |  |
| 07:45:00 | 0 | 24 | 0 | 24 | 3 | 0 | 0 | 3 | 0 | 0 | 2 | 0 | 27 | 98 |
| 08:00:00 | 0 | 22 | 0 | 22 | 10 | 0 | 0 | 10 | 0 | 1 | 1 | 1 | 33 | 116 |
| 08:15:00 | 0 | 38 | 0 | 38 | 2 | 0 | 0 | 2 | 1 | 0 | 2 | 1 | 41 | 136 |
| 08:30:00 | 0 | 23 | 0 | 23 | 5 | 0 | 0 | 5 | 0 | 0 | 1 | 0 | 28 | 129 |
| 08:45:00 | 1 | 18 | 0 | 19 | 6 | 0 | 0 | 6 | 0 | 1 | 0 | 1 | 26 | 128 |
| 09:00:00 | 0 | 14 | 0 | 14 | 5 | 1 | 0 | 6 | 0 | 1 | 0 | 1 | 21 | 116 |
| 09:15:00 | 0 | 14 | 0 | 14 | 3 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 17 | 92 |
| 09:30:00 | 0 | 12 | 0 | 12 | 5 | 0 | 0 | 5 | 0 | 0 | 2 | 0 | 17 | 81 |
| 09:45:00 | 1 | 12 | 0 | 13 | 9 | 0 | 0 | 9 | 0 | 1 | 1 | 1 | 23 | 78 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 1 | 7 | 0 | 8 | 21 | 0 | 0 | 21 | 0 | 0 | 1 | 0 | 29 |  |
| 16:15:00 | 0 | 17 | 0 | 17 | 20 | 0 | 0 | 20 | 0 | 0 | 2 | 0 | 37 |  |
| 16:30:00 | 0 | 14 | 0 | 14 | 28 | 0 | 0 | 28 | 0 | 0 | 1 | 0 | 42 |  |
| 16:45:00 | 1 | 12 | 0 | 13 | 27 | 0 | 0 | 27 | 0 | 0 | 0 | 0 | 40 | 148 |
| 17:00:00 | 0 | 17 | 0 | 17 | 34 | 0 | 0 | 34 | 0 | 0 | 1 | 0 | 51 | 170 |
| 17:15:00 | 0 | 14 | 0 | 14 | 36 | 0 | 0 | 36 | 0 | 0 | 2 | 0 | 50 | 183 |
| 17:30:00 | 0 | 16 | 0 | 16 | 35 | 0 | 0 | 35 | 0 | 0 | 2 | 0 | 51 | 192 |
| 17:45:00 | 0 | 19 | 0 | 19 | 25 | 0 | 0 | 25 | 0 | 0 | 3 | 0 | 44 | 196 |
| 18:00:00 | 0 | 18 | 0 | 18 | 34 | 0 | 0 | 34 | 0 | 0 | 2 | 0 | 52 | 197 |
| 18:15:00 | 0 | 18 | 3 | 18 | 30 | 0 | 0 | 30 | 0 | 0 | 1 | 0 | 48 | 195 |
| 18:30:00 <br> g Movement Cou | 0 | 18 | 0 | 18 | 13 | 0 | 0 | $\text { e } 1 \text { of } 6$ | 1 | 0 | 3 | 1 | 32 | $176$ <br> NXT16E7Z |

NexTrans 4261-A14 Highway 7 Eas Suite 489 Markham ON, CANADA, L3R 9W6

| 18:45:00 | 0 | 12 | 0 | 12 | 26 | 0 | 0 | 26 | 0 | 1 | 1 | 1 | 39 | 171 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grand Total | 4 | 417 | 3 | 421 | 390 | 1 | 0 | 391 | 2 | 5 | 32 | 7 | 819 | - |
| Approach\% | 1\% | 99\% |  | - | 99.7\% | 0.3\% |  | - | 28.6\% | 71.4\% |  | - | - | - |
| Totals \% | 0.5\% | 50.9\% |  | 51.4\% | 47.6\% | 0.1\% |  | 47.7\% | 0.2\% | 0.6\% |  | 0.9\% | - | - |
| Heavy | 0 | 4 |  | - | 6 | 0 |  | - | 0 | 0 |  | - | - | - |
| Heavy \% | 0\% | 1\% |  | - | 1.5\% | 0\% |  | - | 0\% | 0\% |  | - | - | - |
| Bicycles | 0 | 48 |  | - | 38 | 0 |  | - | 1 | 0 |  | - | - | - |
| Bicycle \% | 0\% | 11.5\% |  | - | 9.7\% | 0\% |  | - | 50\% | 0\% |  | - | - | - |

## Peak Hour: 07:30 AM - 08:30 AM Weather: Clear $\left(12.7^{\circ} \mathrm{C}\right)$

| Start Time | N Approach 6TH LINE |  |  |  | S Approach 6TH LINE |  |  |  | W Approach SUNNYCREST LN |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | Peds | Approach Total | Thru | Left | Peds | Approach Total | Right | Left | Peds | Approach Total |  |
| 07:30:00 | 0 | 31 | 0 | 31 | 4 | 0 | 0 | 4 | 0 | 0 | 1 | 0 | 35 |
| 07:45:00 | 0 | 24 | 0 | 24 | 3 | 0 | 0 | 3 | 0 | 0 | 2 | 0 | 27 |
| 08:00:00 | 0 | 22 | 0 | 22 | 10 | 0 | 0 | 10 | 0 | 1 | 1 | 1 | 33 |
| 08:15:00 | 0 | 38 | 0 | 38 | 2 | 0 | 0 | 2 | 1 | 0 | 2 | 1 | 41 |
| Grand Total | 0 | 115 | 0 | 115 | 19 | 0 | 0 | 19 | 1 | 1 | 6 | 2 | 136 |
| Approach\% | 0\% | 100\% |  | - | 100\% | 0\% |  | - | 50\% | 50\% |  | - | - |
| Totals \% | 0\% | 84.6\% |  | 84.6\% | 14\% | 0\% |  | 14\% | 0.7\% | 0.7\% |  | 1.5\% | - |
| PHF | 0 | 0.76 |  | 0.76 | 0.48 | 0 |  | 0.48 | 0.25 | 0.25 |  | 0.5 | - |
| Heavy | 0 | 1 |  | 1 | 1 | 0 |  | 1 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0.9\% |  | 0.9\% | 5.3\% | 0\% |  | 5.3\% | 0\% | 0\% |  | 0\% | - |
| Lights | 0 | 114 |  | 114 | 18 | 0 |  | 18 | 1 | 1 |  | 2 | - |
| Lights \% | 0\% | 99.1\% |  | 99.1\% | 94.7\% | 0\% |  | 94.7\% | 100\% | 100\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% |  | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 1 |  | 1 | 1 | 0 |  | 1 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0.9\% |  | 0.9\% | 5.3\% | 0\% |  | 5.3\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | 0 | - | - | - | 0 | - | - | - | 5 | - | - |
| Pedestrians\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 83.3\% |  | - |
| Bicycles on Crosswalk | - | - | 0 | - | - | - | 0 | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 16.7\% |  | - |
| Bicycles on Road | 0 | 20 | 0 | - | 4 | 0 | 0 | - | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 0\% |  | - |


| Peak Hour: 05:15 PM-06:15 PM Weather: Mostly Cloudy ( $25.2{ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach 6TH LINE |  |  |  | S Approach 6TH LINE |  |  |  | W Approach SUNNYCREST LN |  |  |  | Int. Total (15 min) |
|  | Right | Thru | Peds | Approach Total | Thru | Left | Peds | Approach Total | Right | Left | Peds | Approach Total |  |
| 17:15:00 | 0 | 14 | 0 | 14 | 36 | 0 | 0 | 36 | 0 | 0 | 2 | 0 | 50 |
| 17:30:00 | 0 | 16 | 0 | 16 | 35 | 0 | 0 | 35 | 0 | 0 | 2 | 0 | 51 |
| 17:45:00 | 0 | 19 | 0 | 19 | 25 | 0 | 0 | 25 | 0 | 0 | 3 | 0 | 44 |
| 18:00:00 | 0 | 18 | 0 | 18 | 34 | 0 | 0 | 34 | 0 | 0 | 2 | 0 | 52 |
| Grand Total | 0 | 67 | 0 | 67 | 130 | 0 | 0 | 130 | 0 | 0 | 9 | 0 | 197 |
| Approach\% | 0\% | 100\% |  | - | 100\% | 0\% |  | - | 0\% | 0\% |  | - | - |
| Totals \% | 0\% | 34\% |  | 34\% | 66\% | 0\% |  | 66\% | 0\% | 0\% |  | 0\% | - |
| PHF | 0 | 0.88 |  | 0.88 | 0.9 | 0 |  | 0.9 | 0 | 0 |  | 0 | - |
| Heavy | 0 | 0 |  | 0 | 1 | 0 |  | 1 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 0\% |  | 0\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 0\% |  | 0\% | - |
| Lights | 0 | 67 |  | 67 | 129 | 0 |  | 129 | 0 | 0 |  | 0 | - |
| Lights \% | 0\% | 100\% |  | 100\% | 99.2\% | 0\% |  | 99.2\% | 0\% | 0\% |  | 0\% | - |
| Single-Unit Trucks | 0 | 0 |  | 0 | 1 | 0 |  | 1 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0\% |  | 0\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 0 |  | 0 | 0 | 0 |  | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0\% |  | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | 0 | - | - | - | 0 | - | - | - | 6 | - | - |
| Pedestrians\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 66.7\% |  | - |
| Bicycles on Crosswalk | - | - | 0 | - | - | - | 0 | - | - | - | 3 | - | - |
| Bicycles on Crosswalk\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 33.3\% |  | - |
| Bicycles on Road | 0 | 3 | 0 | - | 8 | 0 | 0 | - | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | 0\% |  | - | - | 0\% |  | - | - | 0\% |  | - |

Peak Hour: 07:30 AM - 08:30 AM Weather: Clear (12.7 $\left.{ }^{\circ} \mathrm{C}\right)$


Peak Hour: 05:15 PM - 06:15 PM Weather: Mostly Cloudy $\left(25.2^{\circ} \mathrm{C}\right)$


Appendix B
Existing Traffic Level of Service Calculations


|  | 4 |  | 4 | $\dagger$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | 4 | $\dagger$ |  |  |
| Traffic Volume (veh/h) | , | 1 | 0 | 19 | 115 | 0 |  |
| Future Volume (Veh/h) | 1 | 1 | 0 | 19 | 115 | 0 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 0.50 | 0.50 | 0.48 | 0.48 | 0.76 | 0.76 |  |
| Hourly flow rate (vph) | 2 | 2 | 0 | 40 | 151 | 0 |  |
| Pedestrians | 6 |  |  |  |  |  |  |
| Lane Width (m) | 3.7 |  |  |  |  |  |  |
| Walking Speed (m/s) | 1.1 |  |  |  |  |  |  |
| Percent Blockage | 1 |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 197 | 157 | 157 |  |  |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 197 | 157 | 157 |  |  |  |  |
| tC, single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 100 | 100 | 100 |  |  |  |  |
| cM capacity (veh/h) | 792 | 889 | 1427 |  |  |  |  |
| Direction, Lane \# | EB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 4 | 40 | 151 |  |  |  |  |
| Volume Left | 2 | 0 | 0 |  |  |  |  |
| Volume Right | 2 | 0 | 0 |  |  |  |  |
| cSH | 837 | 1427 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.09 |  |  |  |  |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 9.3 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A |  |  |  |  |  |  |
| Approach Delay (s) | 9.3 | 0.0 | 0.0 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 17.4\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |


|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\uparrow$ | P | * | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ${ }_{*}$ |  |  | ¢ |  |  | $\dagger$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 6 | 7 | 2 | 3 | 4 | 95 | 0 | 18 | 1 | 439 | 105 | 1 |
| Future Volume (vph) | 6 | 7 | 2 | 3 | 4 | 95 | 0 | 18 | 1 | 439 | 105 | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.73 | 0.73 | 0.73 | 0.48 | 0.48 | 0.48 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate (vph) | 6 | 7 | 2 | 4 | 5 | 130 | 0 | 38 | 2 | 499 | 119 | 1 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 15 | 139 | 40 | 619 |
| Volume Left (vph) | 6 | 4 | 0 | 499 |
| Volume Right (vph) | 2 | 130 | 2 | 1 |
| Hadj (s) | 0.00 | -0.48 | 0.15 | 0.19 |
| Departure Headway (s) | 5.7 | 5.0 | 5.2 | 4.6 |
| Degree Utilization, x | 0.02 | 0.19 | 0.06 | 0.78 |
| Capacity (veh/h) | 571 | 651 | 647 | 777 |
| Control Delay (s) | 8.9 | 9.2 | 8.5 | 21.9 |
| Approach Delay (s) | 8.9 | 9.2 | 8.5 | 21.9 |
| Approach LOS | A | A | A | C |

Intersection Summary

| Delay | 18.8 |  |  |
| :---: | :---: | :---: | :---: |
| Level of Service | C |  |  |
| Intersection Capacity Utilization | 50.7\% | ICU Level of Service | A |
| Analysis Period (min) | 15 |  |  |




|  | $\checkmark$ |  |  | 7 |  | 4 | 4 | $\dagger$ | 7 | * | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ¢ |  |  | ${ }_{4}$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 3 | 3 | 3 | 7 | 6 | 315 | 1 | 125 | 4 | 202 | 59 | 6 |
| Future Volume (vph) | 3 | 3 | 3 | 7 | 6 | 315 | 1 | 125 | 4 | 202 | 59 | 6 |
| Peak Hour Factor | 0.45 | 0.45 | 0.45 | 0.91 | 0.91 | 0.91 | 0.90 | 0.90 | 0.90 | 0.86 | 0.86 | 0.86 |
| Hourly flow rate (vph) | 7 | 7 | 7 | 8 | 7 | 346 | 1 | 139 | 4 | 235 | 69 | 7 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 21 | 361 | 144 | 311 |
| Volume Left (vph) | 7 | 8 | 1 | 235 |
| Volume Right (vph) | 7 | 346 | 4 | 7 |
| Hadj (s) | -0.13 | -0.55 | 0.00 | 0.16 |
| Departure Headway (s) | 5.5 | 4.6 | 5.3 | 5.2 |
| Degree Utilization, x | 0.03 | 0.46 | 0.21 | 0.45 |
| Capacity (veh/h) | 557 | 733 | 622 | 650 |
| Control Delay (s) | 8.7 | 11.5 | 9.8 | 12.5 |
| Approach Delay (s) | 8.7 | 11.5 | 9.8 | 12.5 |
| Approach LOS | A | B | A | B |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | :--- |
| Delay | 11.5 |  |  |
| Level of Service | B | ICU Level of Service | A |
| Intersection Capacity Utilization | $52.6 \%$ |  |  |
| Analysis Period $(\min )$ | 15 |  |  |

# Appendix C <br> Future Background Level of Service Calculations 

|  | 4 |  |  |  |  |  |  | $\uparrow$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \$ |  |  | \$ |  |  | ¢ |  |  | ¢ |  |
| Traffic Volume (veh/h) | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 19 | 0 | 0 | 120 | 0 |
| Future Volume (Veh/h) | 0 | 0 | 1 | 1 | 0 | 1 | 0 | 19 | 0 | 0 | 120 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.25 | 0.25 | 0.25 | 0.50 | 0.50 | 0.50 | 0.45 | 0.45 | 0.45 | 0.73 | 0.73 | 0.73 |
| Hourly flow rate (vph) | 0 | 0 | 4 | 2 | 0 | 2 | 0 | 42 | 0 | 0 | 164 | 0 |
| Pedestrians |  | 11 |  |  | 1 |  |  |  |  |  |  |  |
| Lane Width (m) |  | 3.7 |  |  | 3.7 |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  | 1.1 |  |  | 1.1 |  |  |  |  |  |  |  |
| Percent Blockage |  | 1 |  |  | 0 |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| vC, conflicting volume | 219 | 218 | 175 | 211 | 218 | 43 | 175 |  |  | 43 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 219 | 218 | 175 | 211 | 218 | 43 | 175 |  |  | 43 |  |  |
| tC, single (s) | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 725 | 676 | 864 | 740 | 676 | 1032 | 1398 |  |  | 1577 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total | 4 | 4 | 42 | 164 |  |  |  |  |  |  |  |  |
| Volume Left | 0 | 2 | 0 | 0 |  |  |  |  |  |  |  |  |
| Volume Right | 4 | 2 | 0 | 0 |  |  |  |  |  |  |  |  |
| cSH | 864 | 862 | 1398 | 1577 |  |  |  |  |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.00 |  |  |  |  |  |  |  |  |
| Queue Length 95th (m) | 0.1 | 0.1 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 9.2 | 9.2 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 9.2 | 9.2 | 0.0 | 0.0 |  |  |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.3 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 18.5\% |  |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 | ICU Level of Service |  |  |  |  |  |  |  |  |


|  | $\rangle$ |  | 4 | $\uparrow$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | * |  |  | $\uparrow$ | $\uparrow$ |  |  |
| Traffic Volume (veh/h) | 1 | 1 | 0 | 20 | 121 | 0 |  |
| Future Volume (Veh/h) | 1 | 1 | 0 | 20 | 121 | 0 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 0.50 | 0.50 | 0.48 | 0.48 | 0.76 | 0.76 |  |
| Hourly flow rate (vph) | 2 | 2 | 0 | 42 | 159 | 0 |  |
| Pedestrians | 6 |  |  |  |  |  |  |
| Lane Width (m) | 3.7 |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) | 1.1 |  |  |  |  |  |  |
| Percent Blockage | 1 |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 207 | 165 | 165 |  |  |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 207 | 165 | 165 |  |  |  |  |
| tC , single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 100 | 100 | 100 |  |  |  |  |
| cM capacity (veh/h) | 781 | 880 | 1417 |  |  |  |  |
| Direction, Lane \# | EB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 4 | 42 | 159 |  |  |  |  |
| Volume Left | 2 | 0 | 0 |  |  |  |  |
| Volume Right | 2 | 0 | 0 |  |  |  |  |
| cSH | 828 | 1417 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.09 |  |  |  |  |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 9.4 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A |  |  |  |  |  |  |
| Approach Delay (s) | 9.4 | 0.0 | 0.0 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 17.6\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |


|  | $\rangle$ |  |  | 7 |  | 4 | 4 | $\uparrow$ | 7 | - | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{4}$ |  |  | ${ }_{*}$ |  |  | ¢ |  |  | ¢ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 6 | 7 | 2 | 3 | 4 | 100 | 0 | 19 | 1 | 461 | 110 | 1 |
| Future Volume (vph) | 6 | 7 | 2 | 3 | 4 | 100 | 0 | 19 | 1 | 461 | 110 | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.73 | 0.73 | 0.73 | 0.48 | 0.48 | 0.48 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate (vph) | 6 | 7 | 2 | 4 | 5 | 137 | 0 | 40 | 2 | 524 | 125 | 1 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 15 | 146 | 42 | 650 |
| Volume Left (vph) | 6 | 4 | 0 | 524 |
| Volume Right (vph) | 2 | 137 | 2 | 1 |
| Hadj (s) | 0.00 | -0.48 | 0.15 | 0.19 |
| Departure Headway (s) | 5.8 | 5.1 | 5.3 | 4.6 |
| Degree Utilization, x | 0.02 | 0.21 | 0.06 | 0.83 |
| Capacity (veh/h) | 564 | 659 | 643 | 650 |
| Control Delay (s) | 9.0 | 9.5 | 8.6 | 25.5 |
| Approach Delay (s) | 9.0 | 9.5 | 8.6 | 25.5 |
| Approach LOS | A | A | A | D |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | :--- |
| Delay | 21.6 |  |  |
| Level of Service | C | ICU Level of Service | A |
| Intersection Capacity Utilization | $52.5 \%$ |  |  |
| Analysis Period $(\min )$ | 15 |  |  |




|  | $\gamma$ |  |  | 7 |  | 4 | 4 | $\dagger$ | 1 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | ¢ |  |  | $\dagger$ |  |  | $\dagger$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 3 | 3 | 3 | 7 | 6 | 331 | 1 | 131 | 4 | 212 | 62 | 6 |
| Future Volume (vph) | 3 | 3 | 3 | 7 | 6 | 331 | 1 | 131 | 4 | 212 | 62 | 6 |
| Peak Hour Factor | 0.45 | 0.45 | 0.45 | 0.91 | 0.91 | 0.91 | 0.90 | 0.90 | 0.90 | 0.86 | 0.86 | 0.86 |
| Hourly flow rate (vph) | 7 | 7 | 7 | 8 | 7 | 364 | 1 | 146 | 4 | 247 | 72 | 7 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Volume Total (vph) | 21 | 379 | 151 | 326 |  |  |
| Volume Left (vph) | 7 | 8 | 1 | 247 |  |  |
| Volume Right (vph) | 7 | 364 | 4 | 7 |  |  |
| Hadj (s) | -0.13 | -0.56 | 0.00 | 0.16 |  |  |
| Departure Headway (s) | 5.7 | 4.7 | 5.4 | 5.3 |  |  |
| Degree Utilization, x | 0.03 | 0.49 | 0.23 | 0.48 |  |  |
| Capacity (veh/h) | 537 | 723 | 609 | 641 |  |  |
| Control Delay (s) | 8.9 | 12.1 | 10.0 | 13.1 |  |  |
| Approach Delay (s) | 8.9 | 12.1 | 10.0 | 13.1 |  |  |
| Approach LOS | A | B | B | B |  |  |
| Intersection Summary |  |  |  |  | A |  |
| Delay | 12.0 |  |  |  |  |  |
| Level of Service |  | B |  |  |  |  |
| Intersection Capacity Utilization | $54.6 \%$ | ICU Level of Service |  |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |

## Appendix D <br> Future Total Level of Service Calculations





HCM Unsignalized Intersection Capacity Analysis
8: Sixth Line Road \& Rancliffe Road/Leighland Avenue

|  | $\rangle$ |  |  | 1 |  | 4 | 4 | $\uparrow$ | 7 | * | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ${ }_{4}$ |  |  | ${ }_{\text {¢ }}$ |  |  | ¢ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 6 | 7 | 2 | 4 | 4 | 100 | 0 | 25 | 7 | 461 | 112 | 1 |
| Future Volume (vph) | 6 | 7 | 2 | 4 | 4 | 100 | 0 | 25 | 7 | 461 | 112 | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.73 | 0.73 | 0.73 | 0.48 | 0.48 | 0.48 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate (vph) | 6 | 7 | 2 | 5 | 5 | 137 | 0 | 52 | 15 | 524 | 127 | 1 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 15 | 147 | 67 | 652 |
| Volume Left (vph) | 6 | 5 | 0 | 524 |
| Volume Right (vph) | 2 | 137 | 15 | 1 |
| Hadj (s) | 0.00 | -0.47 | 0.01 | 0.19 |
| Departure Headway (s) | 5.9 | 5.2 | 5.1 | 4.6 |
| Degree Utilization, x | 0.02 | 0.21 | 0.10 | 0.84 |
| Capacity (veh/h) | 557 | 641 | 659 | 652 |
| Control Delay (s) | 9.1 | 9.6 | 8.7 | 26.6 |
| Approach Delay (s) | 9.1 | 9.6 | 8.7 | 26.6 |
| Approach LOS | A | A | A | D |

Intersection Summary
Delay 22.1
Level of Service C

Intersection Capacity Utilization $52.7 \%$
Analysis Period (min)
ICU Level of Service
A
15


|  | $\dagger$ |  | $\uparrow$ | $p$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| Lane Configurations | M |  | $\uparrow$ |  |  | $\uparrow$ |  |
| Traffic Volume (veh/h) | 0 | 1 | 150 | 4 | 2 | 73 |  |
| Future Volume (Veh/h) | 0 | 1 | 150 | 4 | 2 | 73 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\% |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.25 | 0.25 | 0.91 | 0.91 | 0.81 | 0.81 |  |
| Hourly flow rate (vph) | 0 | 4 | 165 | 4 | 2 | 90 |  |
| Pedestrians | 2 |  |  |  |  |  |  |
| Lane Width (m) | 3.7 |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) | 1.1 |  |  |  |  |  |  |
| Percent Blockage | , |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 263 | 169 |  |  | 171 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu, unblocked vol | 263 | 169 |  |  | 171 |  |  |
| tC , single (s) | 6.4 | 6.2 |  |  | 4.1 |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 |  |  | 2.2 |  |  |
| p0 queue free \% | 100 | 100 |  |  | 100 |  |  |
| cM capacity (veh/h) | 728 | 878 |  |  | 1416 |  |  |
| Direction, Lane \# | WB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 4 | 169 | 92 |  |  |  |  |
| Volume Left | 0 | 0 | 2 |  |  |  |  |
| Volume Right | 4 | 4 | 0 |  |  |  |  |
| cSH | 878 | 1700 | 1416 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.10 | 0.00 |  |  |  |  |
| Queue Length 95th (m) | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 9.1 | 0.0 | 0.2 |  |  |  |  |
| Lane LOS | A |  | A |  |  |  |  |
| Approach Delay (s) | 9.1 | 0.0 | 0.2 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 18.5\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |



|  | 4 |  | 4 | $\dagger$ |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |
| Lane Configurations | M |  |  | ${ }_{4}$ | $\dagger$ |  |  |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 143 | 80 | 0 |  |
| Future Volume (Veh/h) | 0 | 0 | 0 | 143 | 80 | 0 |  |
| Sign Control | Stop |  |  | Free | Free |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 0.90 | 0.90 | 0.88 | 0.88 |  |
| Hourly flow rate (vph) | 0 | 0 | 0 | 159 | 91 | 0 |  |
| Pedestrians | 9 |  |  |  |  |  |  |
| Lane Width (m) | 3.7 |  |  |  |  |  |  |
| Walking Speed (m/s) | 1.1 |  |  |  |  |  |  |
| Percent Blockage | 1 |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |
| Median type |  |  |  | None | None |  |  |
| Median storage veh) |  |  |  |  |  |  |  |
| Upstream signal (m) |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |
| vC , conflicting volume | 259 | 100 | 100 |  |  |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  |  |  |  |
| vCu , unblocked vol | 259 | 100 | 100 |  |  |  |  |
| tC, single (s) | 6.4 | 6.2 | 4.1 |  |  |  |  |
| tC, 2 stage (s) |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |
| p0 queue free \% | 100 | 100 | 100 |  |  |  |  |
| cM capacity (veh/h) | 728 | 953 | 1492 |  |  |  |  |
| Direction, Lane \# | EB 1 | NB 1 | SB 1 |  |  |  |  |
| Volume Total | 0 | 159 | 91 |  |  |  |  |
| Volume Left | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 1492 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.05 |  |  |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 10.9\% | ICU Level of Service |  |  | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8: Sixth Line Road \& Rancliffe Road/Leighland Avenue

|  | $\checkmark$ |  |  | 7 |  | 4 | 4 | $\uparrow$ | 7 | * | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  |  | ¢ |  |  | ${ }_{4}$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Traffic Volume (vph) | 3 | 3 | 3 | 12 | 6 | 331 | 1 | 134 | 7 | 212 | 69 | 6 |
| Future Volume (vph) | 3 | 3 | 3 | 12 | 6 | 331 | 1 | 134 | 7 | 212 | 69 | 6 |
| Peak Hour Factor | 0.45 | 0.45 | 0.45 | 0.91 | 0.91 | 0.91 | 0.90 | 0.90 | 0.90 | 0.86 | 0.86 | 0.86 |
| Hourly flow rate (vph) | 7 | 7 | 7 | 13 | 7 | 364 | 1 | 149 | 8 | 247 | 80 | 7 |


| Direction, Lane \# | EB 1 | WB 1 | NB 1 | SB 1 |
| :--- | ---: | ---: | ---: | ---: |
| Volume Total (vph) | 21 | 384 | 158 | 334 |
| Volume Left (vph) | 7 | 13 | 1 | 247 |
| Volume Right (vph) | 7 | 364 | 8 | 7 |
| Hadj (s) | -0.13 | -0.55 | -0.01 | 0.16 |
| Departure Headway (s) | 5.7 | 4.7 | 5.4 | 5.3 |
| Degree Utilization, x | 0.03 | 0.50 | 0.24 | 0.50 |
| Capacity (veh/h) | 527 | 714 | 606 | 638 |
| Control Delay (s) | 8.9 | 12.4 | 10.1 | 13.5 |
| Approach Delay (s) | 8.9 | 12.4 | 10.1 | 13.5 |
| Approach LOS | A | B | B | B |


| Intersection Summary |  |  |  |
| :--- | ---: | :--- | :--- |
| Delay | 12.3 |  |  |
| Level of Service | B | B |  |
| Intersection Capacity Utilization | $55.7 \%$ | Level of Service |  |
| Analysis Period $(\min )$ | 15 |  |  |



