



# **FUNCTIONAL SERVICING REPORT**

Water, Sanitary, and Stormwater Management

## **SPRUCE ROSE INC. SUBDIVISION**

304 & 318 SPRUCE STREET  
TOWN OF OAKVILLE

OUR FILE: 1819

**PREPARED FOR SPRUCE ROSE INC.**

**FEBRUARY 29<sup>TH</sup>, 2024**

Functional Servicing and Stormwater Management Report  
304 & 318 Spruce Street  
Spruce Rose Inc. Subdivision

Our File: 1819

**REVISION HISTORY**

<b>DATE</b>	<b>REVISION</b>	<b>SUBMISSION</b>
February 29 <sup>th</sup> , 2024	1	First ZBA/DPS Application

## TABLE OF CONTENTS

1.0 INTRODUCTION .....	1
1.1 Scope of Functional Servicing Report.....	1
1.2 Reference Documents.....	1
1.3 Site Location and Description .....	1
1.4 Proposed Development.....	2
2.0 MUNICIPAL WATER AND WASTEWATER .....	2
2.1 Water .....	2
2.2 Wastewater .....	3
3.0 STORM DRAINAGE AND STORMWATER MANAGEMENT .....	4
3.1 Existing Storm Drainage .....	4
3.1.1 Minor System .....	4
3.1.2 Major System .....	5
3.2 Proposed Storm Drainage .....	5
3.2.1 Minor and Major System .....	5
3.3 Stormwater Management.....	5
3.3.1 Stormwater Quantity Control (Peak Flow Control).....	6
3.3.2 Stormwater Runoff Volume Reduction (Water Balance) .....	7
3.3.3 Stormwater Quality Control.....	8
4.0 GRADING.....	8
5.0 CONCLUSION.....	9

## LIST OF TABLES

<b>Table 1: Estimated Water Demands Reynolds Street (L/min) .....</b>	<b>3</b>
<b>Table 2: Estimated Water Demands Spruce Street (L/min) .....</b>	<b>3</b>
<b>Table 3: Estimated Wastewater Flow to Reynolds Street (L/s) .....</b>	<b>4</b>
<b>Table 4: Estimated Wastewater Flow to Spruce Street (L/s) .....</b>	<b>4</b>
<b>Table 5: Catchment Imperviousness and SCS Curve Number.....</b>	<b>6</b>
<b>Table 6: Total Stormwater Flows.....</b>	<b>7</b>
<b>Table 7: Pre- to Post-Development Flow Comparison .....</b>	<b>7</b>

## **APPENDICES**

### **APPENDIX 'A'**

- Draft Plan of Subdivision
- Topographic Survey
- Architectural Site Plan

### **APPENDIX 'B'**

- Engineering Record Drawings
- Town of Oakville Stormwater Management Master Plan, Drawings 7.3 -7.4, 7.7

### **APPENDIX 'C'**

- Estimated Water Demand
- Estimated Sanitary Flow
- Stormwater Calculations

### **APPENDIX 'D'**

- Engineering Drawings

### **APPENDIX 'E'**

- HydroCAD Model Output

## 1.0 INTRODUCTION

### 1.1 Scope of Functional Servicing Report

This report has been prepared in support of the Rezoning and Draft Plan of Subdivision Application for a proposed residential development located at 304 & 318 Spruce Street in Oakville.

The Draft Plan of Subdivision for the subject lands was prepared by SGL Planning & Design Inc. dated February 9, 2023 and can be found in Appendix 'A'. The Draft Plan of Subdivision consist of 1 Block (Block 1) and 7 Lots. Block 1 consists of a 5 m x 5 m daylight triangle at the northeast corner of the site. The 7 lots will all have a single family detached home. The topographic survey prepared by R-PE Surveying Ltd. can also be found in Appendix 'A'.

This report outlines how the subdivision can be serviced by the existing infrastructure for water, wastewater, and storm drainage. This report should be read in conjunction with the other plans and reports submitted in support of the planning approvals being sought for the project. For the purposes of this report, north is defined as running parallel to Reynolds Street.

### 1.2 Reference Documents

The following studies/reports/documents were reviewed in the preparation of this report.

- Pre-Consultation Comments Report, Town of Oakville, July 19, 2023
- Drawing 7.3 to 7.4 - "Stormwater Management Master Plan, Town of Oakville"
- Development Engineering Procedures & Guidelines Manual, Town of Oakville, May 2023 (**Town's Manual**)
- Stormwater Management Planning and Guidelines Manual, Ministry of Environment, March, 2003 (**MOE Manual**).
- "Water and Wastewater Linear Design Manual", Region of Halton October, 2019. (**Region's Manual**)

### 1.3 Site Location and Description

As previously mentioned, the site is known municipally as 304 & 318 Spruce Street. The 0.412 ha property is located on the southeast corner of Spruce Street and Reynolds Street. The east and south sides of the property abut existing low density residential uses. There is a single family dwelling at 318 Spruce Street and the Grace Lutheran Church of Oakville at 304 Spruce Street on the subject lands. East between the church and the residential dwelling is a large

parking lot with mature trees between it and the property to the south. Two driveway accesses are provided to the parking lot, both from Spruce Street and there is a residential driveway to spruce street at the residential dwelling. The existing site is relatively flat with drainage generally from back to front, draining towards Spruce and Reynolds Street.

#### **1.4 Proposed Development**

The development block created by the Plan of Subdivision will be further divided into 7 parcels/units and developed with 7 detached single family dwellings, complete with basements, three fronting Reynolds Street, and four fronting Spruce Street. Each dwelling will have its own driveway entrance, the sidewalks along Spruce and Reynolds Street will be maintained. A copy of the preliminary site plan is included in Appendix 'A' for reference.

### **2.0 MUNICIPAL WATER AND WASTEWATER**

Municipal water and wastewater services for the subject site are to be designed in accordance with the Region of Halton water and Wastewater Linear Design Manual.

Per the Halton Water & Wastewater Linear Design Manual, for detached residential dwellings, the equivalent population density is 55 persons per hectare. Based on this density, the site would have an equivalent of 23 persons (55 persons/ha x 0.412 ha).

#### **2.1 Water**

There is an existing 300 mm diameter watermain along Spruce Street and an existing 150 mm diameter watermain along Reynolds Street. Both watermains are relatively new, being constructed in 1982. The existing church is connected to the Reynolds Street watermain while the residential dwelling is connected to the Spruce Street watermain. See the engineering record drawings in Appendix 'B' for further detail.

The three proposed residential dwellings fronting to Reynolds Street (Lots 1-3) will be serviced by the 150 mm diameter along Reynolds Street, while the four proposed residential dwellings fronting Spruce Street (Lots 4-7) will be serviced by the 300 mm diameter watermain along Spruce Street. A 9.6 m long section of the 150 mm diameter watermain on Spruce Street will be lowered between Lots 1 and 2 to allow sanitary servicing to these lots. See the Servicing Plan (S1), and the Sections and Details Plan (D1) for details.

Using the development area and Region of Halton design criteria, the expected domestic water usage for each watermain is estimated and summarized below (see Appendix 'C' for supporting calculations). The fire flow is estimated for demand purposes only using the Fire Underwriter's Survey methodology and should be confirmed at the building permit stage.

**Table 1: Estimated Water Demands Reynolds Street (L/min)**

Average Daily Demand	0.5
Minimum Hourly Demand	0.5
Maximum Hourly Demand	1.9
Maximum Daily Demand	1.1
Estimated Fire Demand (FUS 1999)	5000
Maximum Daily Plus Fire Demand	5001.1

**Table 2: Estimated Water Demands Spruce Street (L/min)**

Average Daily Demand	0.5
Minimum Hourly Demand	0.5
Maximum Hourly Demand	2.0
Maximum Daily Demand	1.1
Estimated Fire Demand (FUS 1999)	5000
Maximum Daily Plus Fire Demand	5001.1

Fire hydrants exist at the northeast corner of Spruce and Reynolds as well as adjacent to the site on the north side of Spruce Street at 321 Spruce Street. Flow testing will be undertaken at the earliest possible date to confirm the system can provide adequate fire flow to meet the above demands.

The locations of the nearby hydrants on Spruce Street provide adequate coverage for the proposed development and are within 90 m of all principal entrances.

Each dwelling will have typical 25 mm individual service connections. The existing water connections to Spruce and Reynolds Street will be disconnected. Refer to the Servicing Plan, S1 in Appendix 'D' for details.

## **2.2 Wastewater**

There are existing 200 mm diameter sanitary sewers along Spruce Street and Reynolds Street. The sanitary on Reynolds Street originates at a manhole approximately 22 m north of the southern property line and flows south along Reynolds Street, this main is approximately 2 m deep along the development's frontage. The connectivity of the sewer along Reynolds Street is not clear on the Region's operating maps. The sanitary sewer on Spruce Street flows west to the Trafalgar Road trunk sewer. This sewer is approximately 2 m deep along the development's frontage. Records show that the existing church and residential dwelling are connected to the existing sewer along Spruce Street.

The two southernmost residential dwellings fronting Reynolds Street (Lots 1 and 2) will be serviced by the 200 mm diameter sanitary sewer on Reynolds Street, while the remaining five residential dwellings (lots 3-7) will be serviced by the 200 mm diameter sanitary sewer along

Spruce Street. The sewage flows were calculated for the development and the results for each sanitary main are as summarized below. Further detail can be found in Appendix 'C'.

**Table 3: Estimated Wastewater Flow to Reynolds Street (L/s)**

Average Residential Daily Dry Weather Flow	0.07
Modified Harmon Residential Peaking Factor	4.37
Infiltration Allowance (0.26L/s-ha)	0.12
Peak Daily Flow	0.43

**Table 4: Estimated Wastewater Flow to Spruce Street (L/s)**

Average Residential Daily Dry Weather Flow	0.07
Modified Harmon Residential Peaking Factor	4.37
Infiltration Allowance (0.26L/s-ha)	0.12
Peak Daily Flow	0.43

Each residential dwelling will have typical 125mm individual service connections. The existing sanitary services to the buildings will be disconnected.

The Spruce Street and Reynolds Street sanitary sewers are tributary to the Trafalgar Road/Rebecca Street Trunk sewers. An analysis of the downstream sewer system can be provided once the Region's Infoworks model is available.

### **3.0 STORM DRAINAGE AND STORMWATER MANAGEMENT**

#### **3.1 Existing Storm Drainage**

##### 3.1.1 Minor System

There is an existing 675 mm diameter storm sewer running along Spruce Street adjacent to the subject site. This sewer flows west to Reynolds Street. From the intersection of Reynolds and Spruce Street there is an existing 750 mm diameter storm sewer flowing south along Reynolds. The sewer system is tributary to the Sixteen Mile Creek.

Based on a review of Oakville's Stormwater Master Plan (Drawing 7.3 and 7.4 – see Appendix 'B' for further detail), the storm sewers on Reynolds Street and Spruce Street in the vicinity of the site is identified as below ½ surcharging depth and above the obvert during the 5-year event and above ½ surcharging depth and below the rim elevation during the 100-year storm in the existing condition.



The topographic survey indicates the majority of the site drains to the Spruce Street and Reynolds Street sewers, with a small portion of the lands flowing south to the adjacent property.

### 3.1.2 Major System

Based on a review of Oakville's Stormwater Master Plan (Drawing 7.7 – See Appendix 'B' for further detail), the flow is contained within the Right-of-Way during the 100-year storm in the existing condition.

A review of the existing major overland flow along streets adjacent to the subject lands using lidar data indicates that overland flow travels south along Reynolds Street and east along Spruce street within the municipal rights-of-way.

## **3.2 Proposed Storm Drainage**

### 3.2.1 Minor and Major System

The Town's Stormwater Management Master Plan sets out evaluation criteria and hierarchy for conveyance capacity improvements (major systems) within the Town's network. Figure 8.2.1 from the Master Plan provides a flow chart for making those evaluations. As the major system is contained within the municipal ROW no conveyance capacity improvements are required.

The front yards and driveways will sheet flow from the buildings to Spruce Street and Reynolds Street. The roof areas will splash to grade and be directed to the property line swales which lead to rear lot catchbasins. The rear lot catchbasins between properties which front to Spruce will have catchbasin leads to the 675 mm diameter storm sewer on Spruce Street, while the remaining catchbasin will have catchbasin leads to the 750 mm diameter storm sewer on Reynolds Street.

Every dwelling will feature 150 mm diameter storm service connections to the adjacent storm sewers. Each dwelling will have a sump pump to protect the basement in the event the storm sewer surcharges.

## **3.3 Stormwater Management**

The Town of Oakville requirements for stormwater management are as follows:

1. Stormwater Quantity Control (Peak Flow Control)

The minimum control is to maintain post-development peak runoff rates to pre-development levels for all events up to and including the 100-year storm.

2. Stormwater Runoff Volume Reduction (Water Balance)

As per the draft Oakville Development Engineering Procedures and Guidelines (May 2023), sites are to be designed such that the runoff from a 25 mm event shall be retained on site.

3. Stormwater Quality Control

- i) Construction Phase (Erosion and Sediment Control)
- ii) Post Construction: Achieve Enhanced Level 1 Protection, as per the Ministry of Environment’s Stormwater Management Planning and Design Manual (March 2003).

3.3.1 Stormwater Quantity Control (Peak Flow Control)

The required quantity control for the site is to limit the peak post-development flows to the 5-year pre-development rate for all storms up to the 100-year event. To control post-development flows to the 5-year pre-development level, three 600 mm dia. oversized sewers are proposed from each of the rear lot catchbasins to property line manholes. The manholes will be fitted with a 75 mm dia. orifice plate on the upstream side of the manhole.

To estimate the pre- and post-development flows, HydroCAD was used to model the system. The existing impervious and pervious areas were estimated using the topographic survey and resulted in a weighted SCS curve number of 88. The proposed imperviousness was estimated for the uncontrolled area, and the area tributary to each catchbasin. See Table 5 below for a summary of the imperviousness of each drainage area and corresponding weighted SCS curved number.

**Table 5: Catchment Imperviousness and SCS Curve Number**

<b>Catchment</b>	<b>Pervious Area (m<sup>2</sup>)</b>	<b>Impervious Area (m<sup>2</sup>)</b>	<b>Weighted SCS Curve Number</b>
Existing Condition	2395	1721	88
Uncontrolled Area	607	507	88
Catchbasin (Lot 1)	487	552	90
Catchbasin (Lot 5)	589	337	86
Catchbasin (Lot 6)	644	393	87

The 75 mm dia. orifice plates were modeled with a discharge coefficient of 0.64 and invert elevation’s matching those on the servicing plan. The length and slope of each oversized storm sewer and catchbasin top of grate modeled match those on the servicing plan. The grading plan was used to estimate surface storage and spill elevations. See Appendix ‘E’ for the HydroCAD

model output. See Table 6 below for a summary of the total pre- and post-development stormwater flows.

**Table 6: Total Stormwater Flows**

<b>Return</b>	<b>Pre-Dev Total (L/s)</b>	<b>Post-Dev Uncontrolled (L/s)</b>	<b>Post-Dev Controlled (L/s)</b>	<b>Post-Dev Total (L/s)</b>	<b>Storage Required (m<sup>3</sup>)</b>	<b>Storage Provided (m<sup>3</sup>)</b>
5-yr	75	20	29	49	12.3	49.3
10-yr	96	26	36	62	16.4	49.3
25-yr	125	34	43	75	24.1	49.3
50-yr	146	39	48	87	29.9	49.3
100-yr	166	45	53	98	36.5	49.3

The three 75 mm dia. orifice plates are sufficient in reducing post-development flows to less than pre-development rates for all storms. The orifice plates are able to restrict the post-development 5-year, 10-year, and 25-year storms to the 5-year pre-development flow rate. The 50-year and 100-year post development flows are greater than the 5-year pre-development rate as 75 mm is the smallest acceptable orifice size for practical reasons and in keeping with to the Town’s Development Engineering Procedures & Guidelines Manual. See Table 7 below for a comparison of pre-post development flows for the 5- to 100-year storm events.

**Table 7: Pre- to Post-Development Flow Comparison**

<b>Return</b>	<b>Pre-Dev Total (L/s)</b>	<b>Post-Dev Total (L/s)</b>	<b>Pre-Post Percent Change</b>	<b>Comparison to 5-Year Pre-Dev</b>
5-yr	75	49	-35%	-35%
10-yr	96	62	-35%	-17%
25-yr	125	75	-40%	0%
50-yr	146	87	-40%	16%
100-yr	166	98	-40%	31%

As illustrated in Table 7, the post development flows are well below the pre-development flow rates for all storm systems up to the 100-year, and the 5- to 25-year post-development flow rates are at or below the 5-year pre-development flow rate.

### 3.3.2 Stormwater Runoff Volume Reduction (Water Balance)

As per the Town’s Development Manual, it is recommended that 25 mm of water is retained across the site. This would result in 102.9 m<sup>3</sup> of retention volume. Given the tenure of the development, space limitation, and desired tree preservation, the opportunity to incorporate meaningful LID measures is limited. Due to the size of the rear yard and desired tree protection, no formal volume reduction by means of infiltration is proposed. We would note that that the

grading design, specifically swale slopes are generally flat and enhance infiltration. Incorporating French drains along and in key locations of the swales would provide further mitigation.

### 3.3.3 Stormwater Quality Control

Stormwater quality controls will need to be implemented during the construction phase as well as post-construction.

#### i) Construction Phase (Erosion and Sediment Control)

The primary source of sediment laden runoff will be as a result of vehicle mud tracking. In addition to on-site controls, off-site controls in the vicinity of the site will be required to mitigate sediment transport. Prior to any construction activity, all sediment and erosion control measures shall be implemented. These measures include sediment control fence, mud mat at construction entrance, catch basin sediment control and routine 'housekeeping' such as sweeping and flushing of the surrounding roads.

All controls shall be inspected on a regular basis and after rainfall events that generate runoff. Of particular importance are the controls placed at catch basins. If not maintained, the tendency for these to become obstructed is high and hence there is a potential for localized pooling and/or drainage issues.

#### ii) Post Construction

Approximately 92% of the site's drainage will be from the roof of the buildings, and the front and rear yards, all of which can be considered clean and will not require treatment. No measures are proposed for the driveways. All drainage from the roofs will be directed through grassed swales in the front and rear yards, which will provide filtration prior to discharge into the rear lot catchbasin and municipal sewer. No further quality control measures are proposed.

## **4.0 GRADING**

The grading of the subdivision must take into account the boundary conditions that exist along all sides of the property such that existing drainage patterns are maintained, as well as any efforts related to tree protection. The grading to the north is controlled by the existing curb and sidewalk on Spruce Street, while the grading to the west is controlled by the existing curb and sidewalk on Reynolds Street. The west and south sides of the site must match into the existing elevations along the adjoining properties. In addition, the south side of the site provides some further constraints due to several trees along the property line that are to be protected. In general, the grades within the tree protection zone remain unaffected, however there are a few localized areas where minor grading is proposed to construct the drainage swales to the rear

yard catchbasin. This grading is to be done by hand, under the direct supervision of an arborist. Refer to the Grading Plan (G1) in Appendix 'D' for further information.

It is proposed that the lots follow a split drainage approach. The highpoint between the lots will be set towards the front of the houses such that rainwater leaders can be directed to the rear lot catchbasins and stormwater controls, limiting the amount of uncontrolled discharge.

## 5.0 CONCLUSION

Adequate municipal infrastructure exists within the abutting road allowances to support the proposed Draft Plan of Subdivision and Rezoning Amendments being sought. The information in this report provides the framework from which detailed engineering designs can evolve as the development progresses through the planning approval and subdivision registration process.

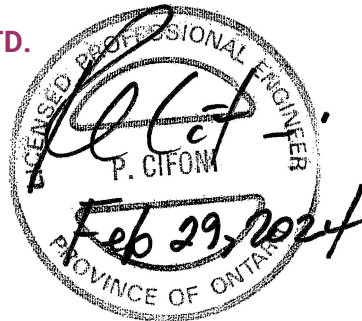
Through the use of rear lot catchbasins, oversized storm sewers, and orifice plates, the development proposal results in decreased flows from the subject lands for all storms up to the 100-year event. No formal stormwater quality controls are proposed.

Implementation of the servicing and grading designs presented in this report will provide the expected level of service for low density infill residential developments. No adverse impact to the abutting properties is expected.

**PREPARED BY TRAFALGAR ENGINEERING LTD.**



**Malcolm Wallace, EIT**  
Intermediate Designer



**Paul Cifoni, P.Eng.**  
Consulting Engineer  
Principal

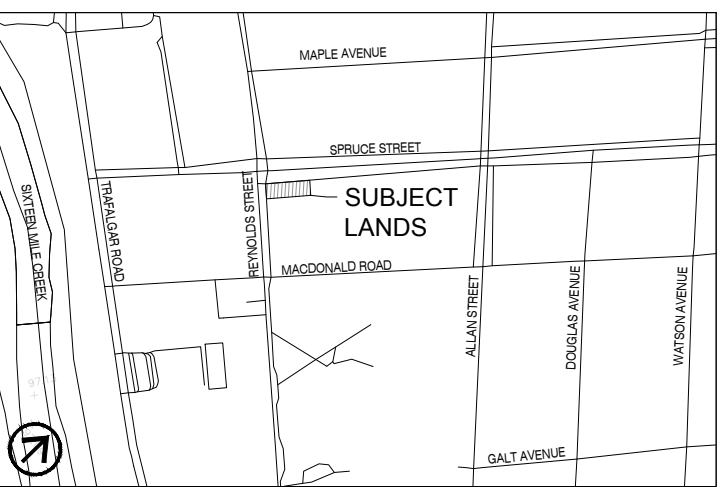
## **APPENDIX 'A'**

Draft Plan of Subdivision

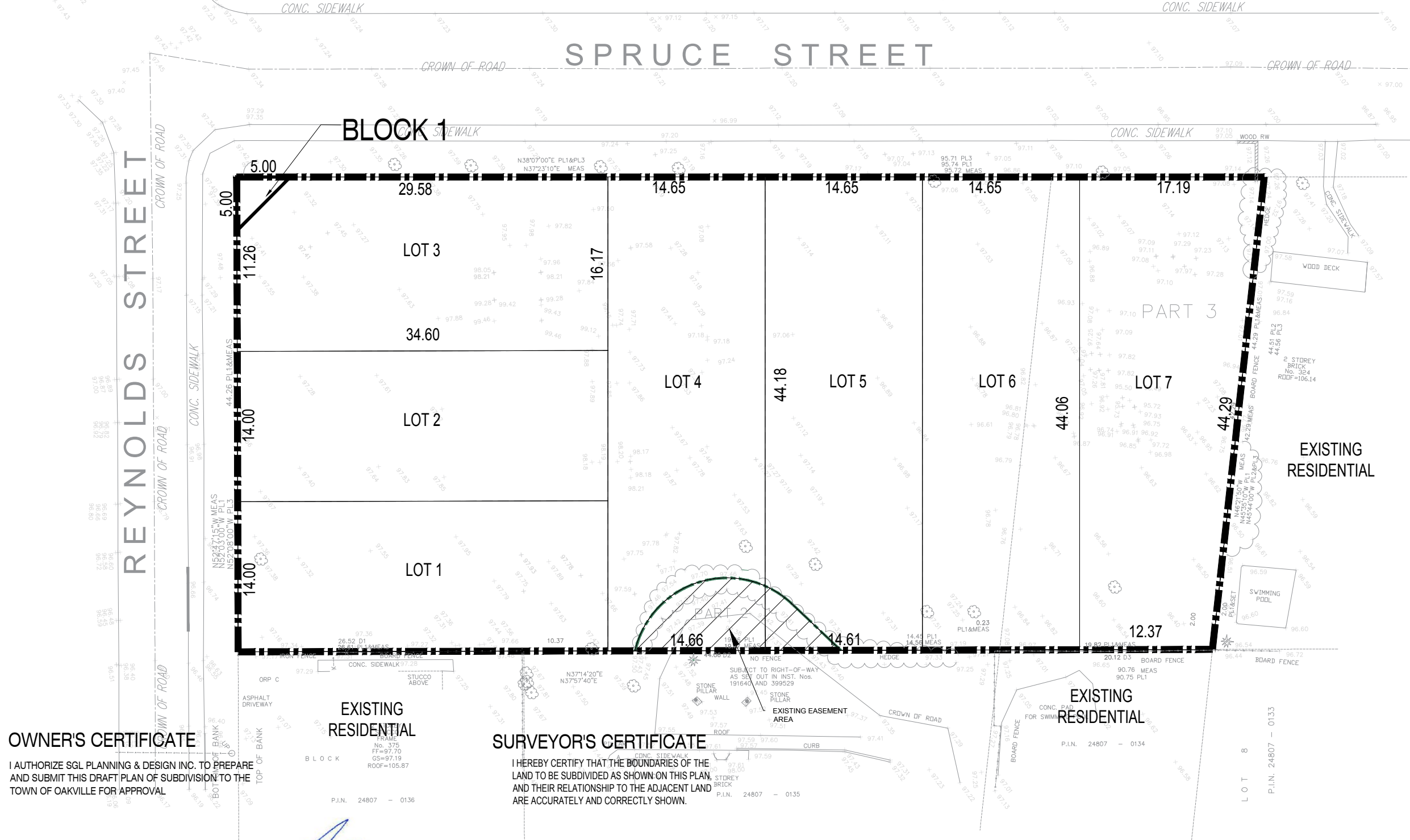
Topographic Survey

Architectural Site Plan

DRAFT PLAN OF SUBDIVISION  
 PART OF BLOCK A  
 REGISTERED PLAN 121  
 TOWN OF OAKVILLE  
 REGIONAL MUNICIPALITY OF HALTON  
 1:400



KEY PLAN SCALE: 1:1000



SECTION 51, PLANNING ACT,  
 ADDITIONAL INFORMATION

- A. AS SHOWN ON DRAFT PLAN
- B. NOT APPLICABLE
- C. AS SHOWN ON DRAFT PLAN
- D. AS SHOWN ON DRAFT PLAN
- E. AS SHOWN ON DRAFT PLAN
- F. AS SHOWN ON DRAFT PLAN
- G. AS SHOWN ON DRAFT PLAN
- H. MUNICIPAL WATER SERVICES
- I. CLAY-LOAM
- J. AS SHOWN ON DRAFT PLAN
- K. MUNICIPAL SANITARY AND STORM SEWER AVAILABLE FROM ADJACENT STREET

SCHEDULE OF LAND USE

	BLOCKS	RES. UNITS	+Ha.	+Acs.
BLOCK 1	DAYLIGHT TRIANGLE	1	0.001	0.003
LOT 1	SINGLE-DETACHED	1	0.048	0.119
LOT 2	SINGLE-DETACHED	1	0.048	0.119
LOT 3	SINGLE-DETACHED	1	0.055	0.136
LOT 4	SINGLE-DETACHED	1	0.065	0.161
LOT 5	SINGLE-DETACHED	1	0.065	0.161
LOT 6	SINGLE-DETACHED	1	0.065	0.161
LOT 7	SINGLE-DETACHED	1	0.065	0.161

**OWNER'S CERTIFICATE**  
 I AUTHORIZE SGL PLANNING & DESIGN INC. TO PREPARE AND SUBMIT THIS DRAFT PLAN OF SUBDIVISION TO THE TOWN OF OAKVILLE FOR APPROVAL

DATE FEBRUARY 23, 2024 SILVIO GUGLIETTI A.S.O.

**SURVEYOR'S CERTIFICATE**  
 I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED AS SHOWN ON THIS PLAN AND THEIR RELATIONSHIP TO THE ADJACENT LAND ARE ACCURATELY AND CORRECTLY SHOWN.

DATE FEBRUARY 23, 2024 R. DENBROEDER O.L.S.

TOTAL	8	7	0.412	1.02
-------	---	---	-------	------

# PLAN OF SURVEY AND TOPOGRAPHY OF PART OF BLOCK A REGISTERED PLAN 121 TOWN OF OAKVILLE REGIONAL MUNICIPALITY OF HALTON

SCALE 1:250  
10m 5m 0 10m 20metres

R-PE SURVEYING LTD., O.L.S.

METRIC  
DISTANCES AND COORDINATES SHOWN ON THIS PLAN ARE IN METRES AND CAN BE CONVERTED TO FEET BY DIVIDING BY 0.3048.

## LEGEND

- BELLPED DENOTES BELL BOX
- BXC DENOTES COMMUNICATION CABLE BOX
- CB DENOTES CATCH BASIN
- CONC DENOTES CONCRETE
- P DENOTES PORCH
- RW DENOTES RETAINING WALL
- BF DENOTES BOARD FENCE
- IF DENOTES IRON FENCE
- PWF DENOTES POST WIRE FENCE
- FF DENOTES FINISHED FLOOR
- ST DENOTES STAIRS
- DS DENOTES DOOR SILL
- GS DENOTES GARAGE SILL
- UP DENOTES UTILITY POLE
- MH DENOTES MANHOLE
- MHSA DENOTES SANITARY MANHOLE
- MHST DENOTES STORM MANHOLE
- WV DENOTES WATER VALVE
- W- DENOTES OVERHEAD WIRE
- E/W/N/S DENOTES EAST/WEST/NORTH/SOUTH
- Ø DENOTES DIAMETER
- 0.500 \* DENOTES DECIDUOUS TREE
- 0.150 \* DENOTES CONIFEROUS TREE
- x --- DENOTES FENCE LINE

## NOTES

- DENOTES MONUMENT FOUND
- SIB DENOTES STANDARD IRON BAR
- IB DENOTES IRON BAR
- IP DENOTES IRON PIPE
- P.I.N. DENOTES PROPERTY IDENTIFIER NUMBER
- D1 DENOTES INST. No. 0C21070
- D2 DENOTES INST. No. 399525
- D3 DENOTES INST. No. 824827
- PL1 DENOTES PLAN 20R-10208
- PL2 DENOTES SURVEYOR'S REAL PROPERTY REPORT BY J. H. GELBLOOM SURVEYING LIMITED., O.L.S., DATED JANUARY 18, 2023
- PL3 DENOTES REGISTERED PLAN 121
- (626) DENOTES H. D. SEWELL, O.L.S.
- (760) DENOTES MCCONNELL, MAUGHAN LIMITED, O.L.S.
- (950) DENOTES CUNNINGHAM MCCONNELL LIMITED, O.L.S.
- (1808) DENOTES J. H. GELBLOOM SURVEYING LIMITED., O.L.S.
- (WIT) DENOTES WITNESS
- (NI) DENOTES NOT IDENTIFIED
- ORP DENOTES OBSERVED REFERENCE POINT

## BENCHMARK NOTE

ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES.  
TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD.  
ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928-1978).

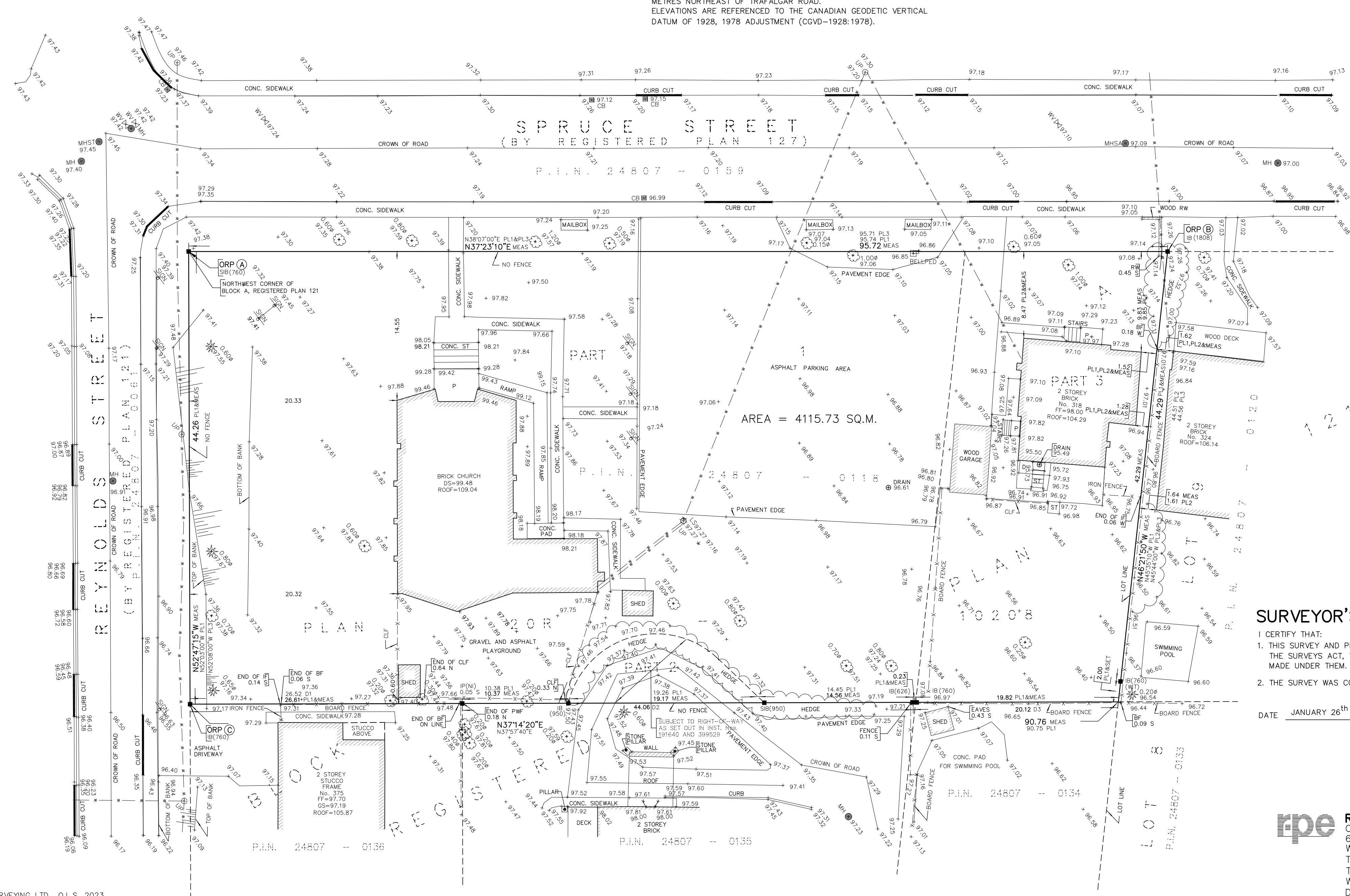
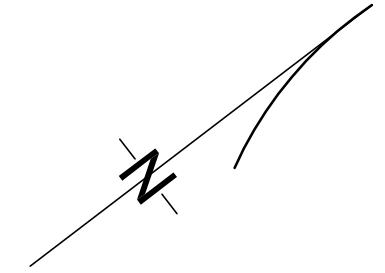
## INTEGRATION NOTE

BEARINGS ARE GRID, UTM, NAD83 (CSRS:CBNv6:2010.0), DERIVED FROM OBSERVED REFERENCE POINTS FROM REAL TIME NETWORK STATION 20120110009 (NORTHING 4801633.529, EASTING 597944.44).

COORDINATES ARE UTM, ZONE 17, NAD83 (CSRS:CBNv6:2010.0), TO URBAN ACCURACY PER SEC. 14 (2) OF O.REG. 216/10, AND CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN.

POINT	NORTHING	EASTING
ORP (A)	4812129.16	607084.35
ORP (B)	4812205.19	607142.45
ORP (C)	4812102.40	607119.59

DISTANCES ARE GROUND AND CAN BE CONVERTED TO GRID BY MULTIPLYING BY THE COMBINED SCALE FACTOR OF 0.999732.



## SURVEYOR'S CERTIFICATE

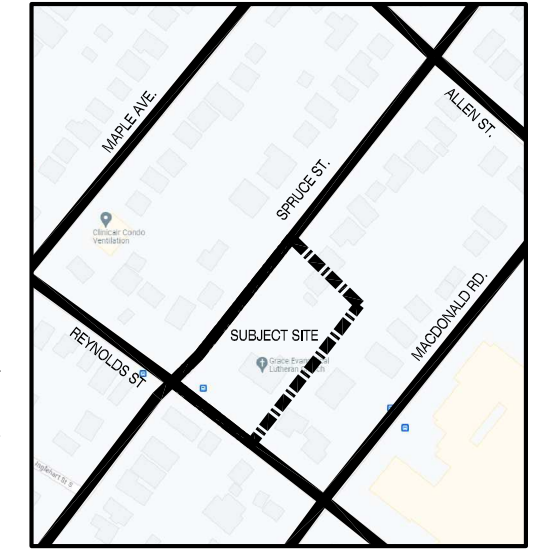
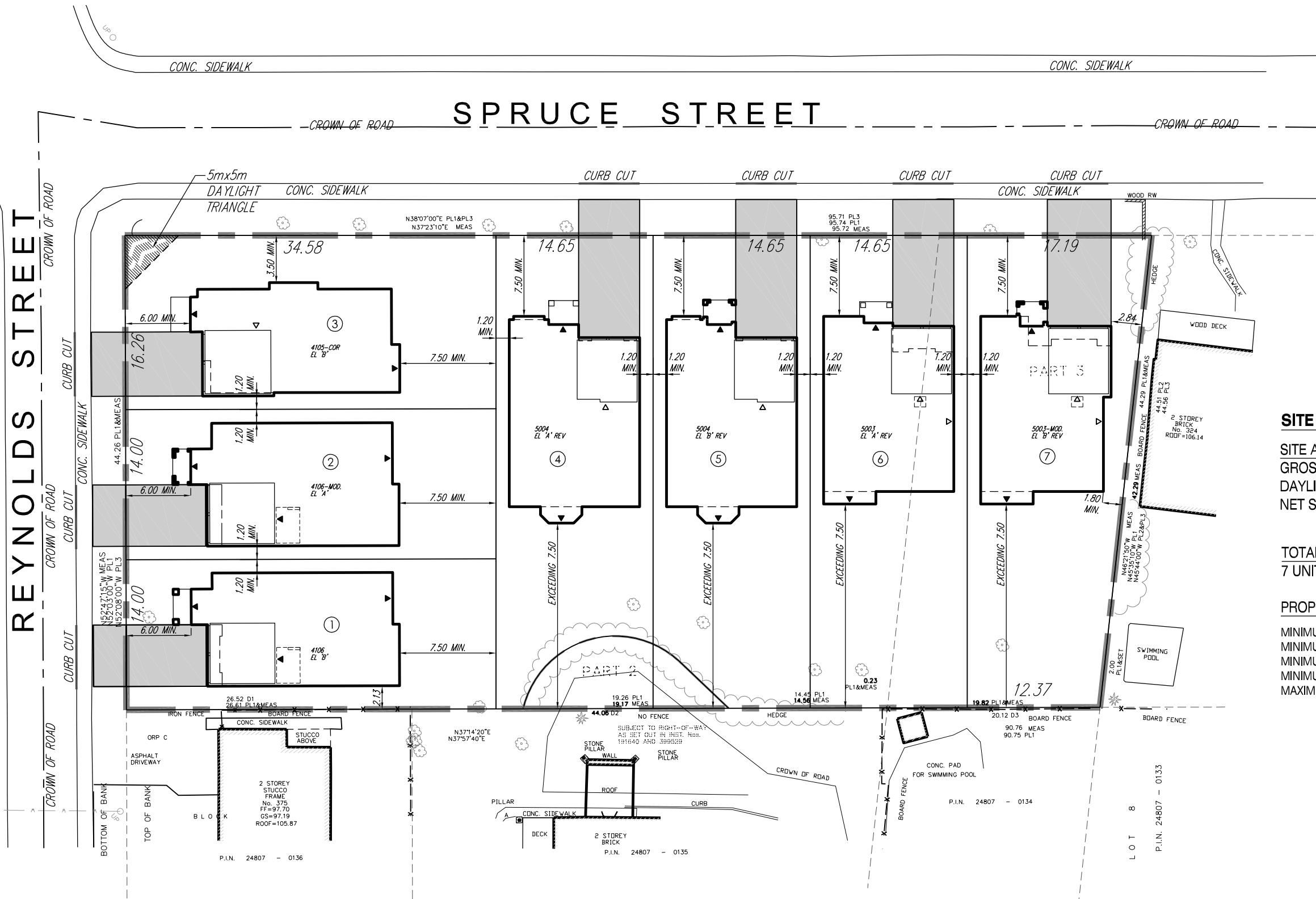
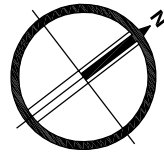
- I CERTIFY THAT:
- THIS SURVEY AND PLAN ARE CORRECT AND IN ACCORDANCE WITH THE SURVEYS ACT, THE SURVEYORS ACT AND THE REGULATIONS MADE UNDER THEM.
  - THE SURVEY WAS COMPLETED ON THE 20<sup>th</sup> DAY OF JANUARY, 2023
- DATE JANUARY 26<sup>th</sup>, 2023

*R. Denbroeder*  
R. DENBROEDER  
ONTARIO LAND SURVEYOR

THIS PLAN OF SURVEY RELATES TO AOLS PLAN SUBMISSION FORM NUMBER 2203822.

**rpe** R-PE SURVEYING LTD.  
ONTARIO LAND SURVEYORS  
643 Chrised Road, Suite 7  
Woodbridge, Ontario L4L 8A3  
Tel.(416)635-5000 Fax (416)635-5001  
Tel.(905)264-0881 Fax (905)264-2099  
Website: www.r-pe.ca  
DRAWN: S.L. CHECKED: R.D.  
JOB No. 23-005 FILE No.23-005TP01





**SITE STATISTICS**

SITE AREA:  
 GROSS SITE AREA = 4115.64 S.M.  
 DAYLIGHT TRIANGLE = 12.50 S.M.  
 NET SITE AREA = 4103.14 S.M.

TOTAL UNITS:  
 7 UNITS

**PROPOSED ZONING STANDARDS:**

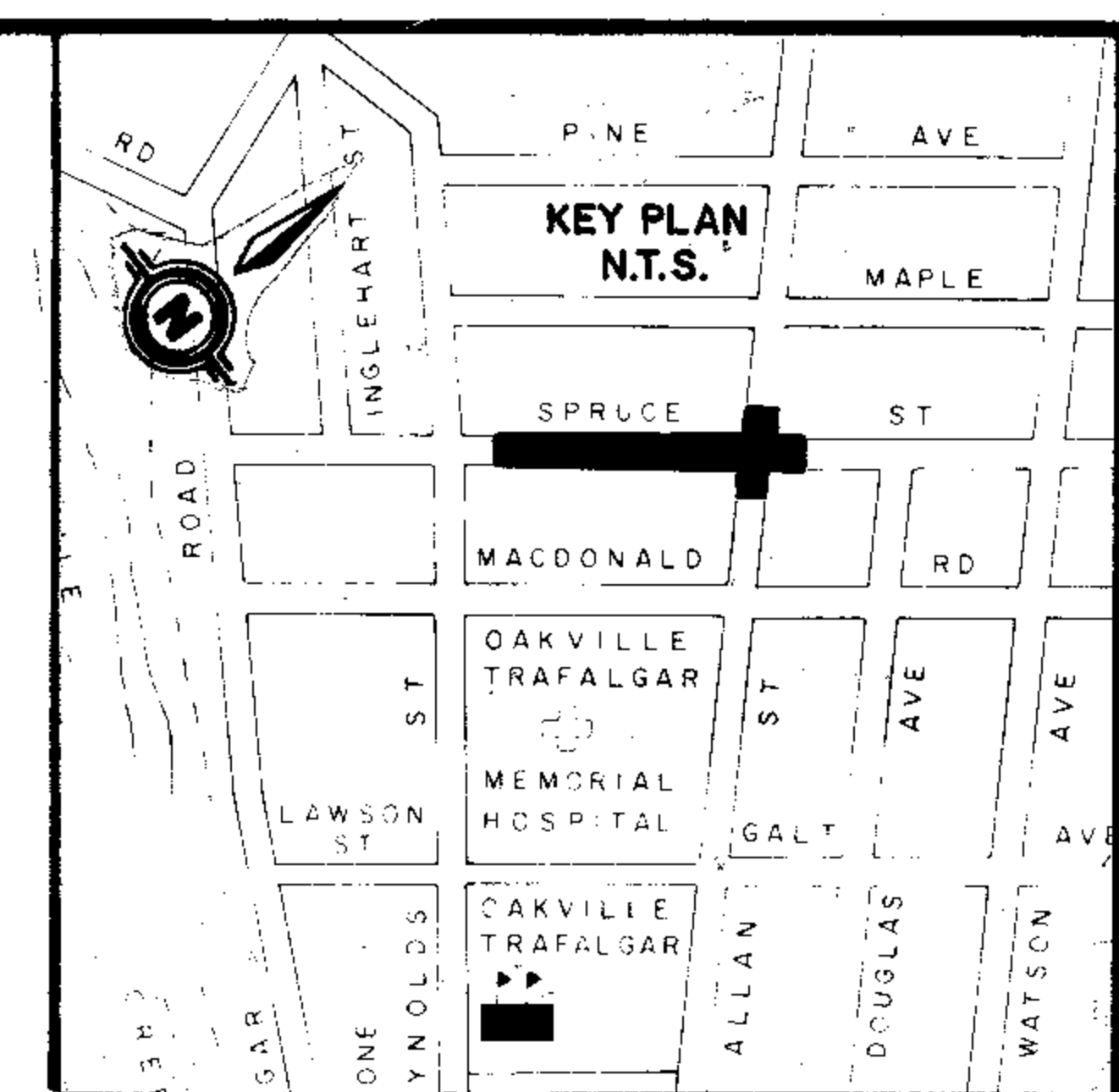
MINIMUM FRONT YARD: 7.5m (6m FOR LOTS 1, 2 & 3)  
 MINIMUM REAR YARD: 7.5m  
 MINIMUM INTERIOR SIDE YARD: VARIES (SEE SITE PLAN)  
 MINIMUM EXTERIOR SIDE YARD: 3.5m  
 MAXIMUM LOT COVERAGE: 35% (41% FOR LOT 1)  
 (44% FOR LOT 2)

LOT	COVERAGE CALCULATIONS			
	LOT AREA (S.M.)	UNIT COVERAGE (S.M.)	UNIT COVERAGE (S.F.)	UNIT COVERAGE (%)
1	482.58	196.00	2109.73	40.6%
2	483.21	212.16	2283.67	43.9%
3	547.70	188.24	2026.2	34.4%
4	646.83	215.75	2322.31	33.4%
5	646.28	215.25	2316.93	33.3%
6	645.73	205.33	2210.15	31.8%
7	650.78	198.58	2137.5	30.5%

**APPENDIX 'B'**

Engineering Record Drawings

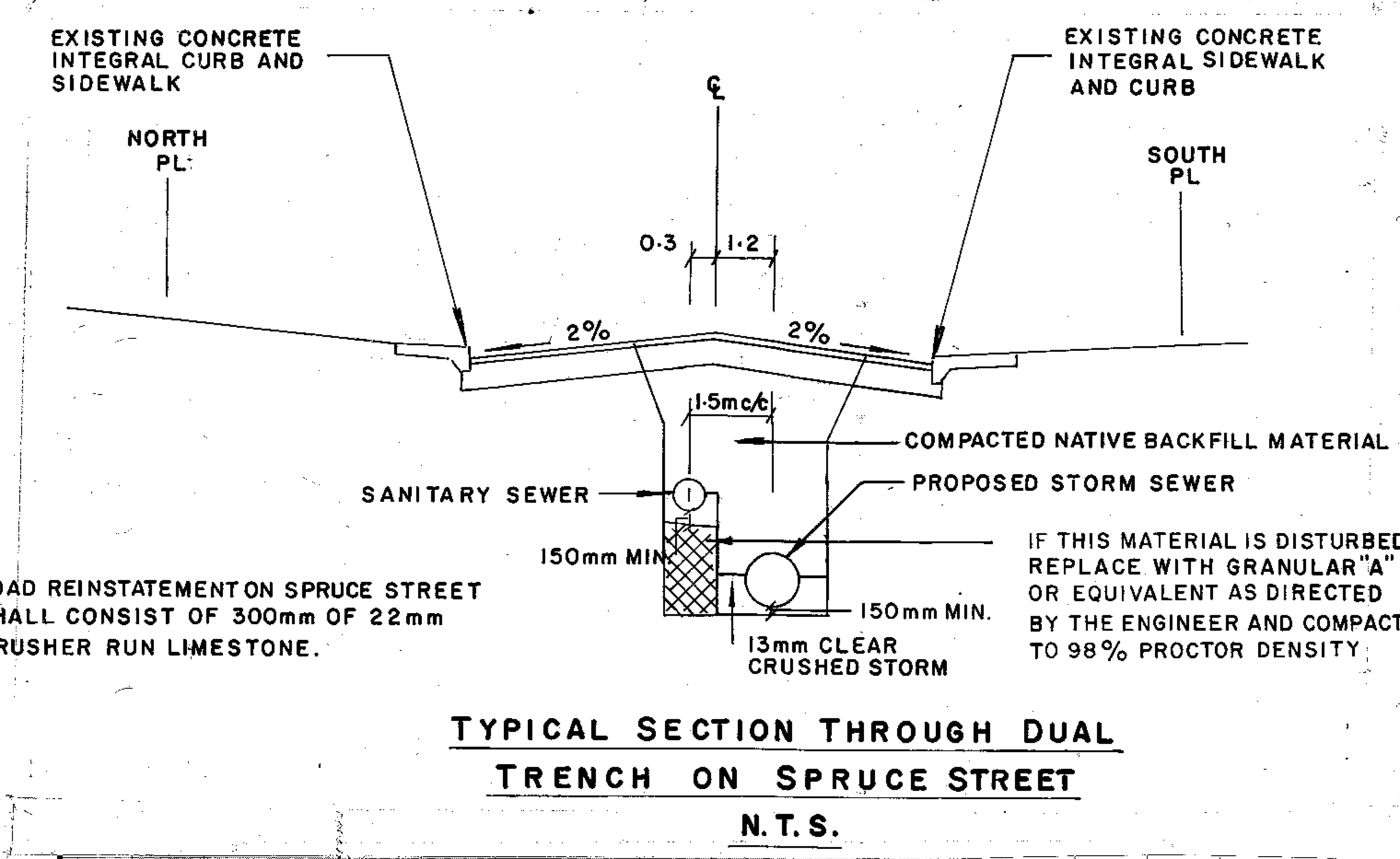
*Town of Oakville Stormwater Management Master Plan, Drawings 7.3 - 7.4, 7.7*



SANITARY SEWER DATA						
M.H.	STATION	CONSTR. OFFSET	STD.	INVERTS		REMARKS
				INLET	OUTLET	
MH4	0+274.2	0.6m LT.	322	-	W. 95.090 E. 95.020	MATCH TOP OF GRATE TO EXIST. PAVEMENT ELEV.
MH5	0+411.4	0.7m LT.	322	W. 94.501	-	
MH6	0+332.1	3.2m RT.	322	-	E. 94.856	
MH6	0+411.8	2.0m RT.	322	W. 94.490	-	

WATERMAIN DATA					
ITEM	STATION	CONSTR. OFFSET	STD.	INVERT ELEV.	REMARKS
HYD. LAT. & SEC. G.V.	0+267.8	8.2m LT.	441	94.907	COMPLETE WITH 150 OFF 300mm M.J. ANCHOR TEE
150 OFF 300mm FL. ANCHOR TEE & 150mm FL. GATE VALVE & V.B.	0+402.2	2.8m LT.	405	94.357	
90° HORIZ. BEND FL.		4.5m LT.		94.357	150mm DIA.
300mm DIAMETER VALVE & 300mm x 750mm TAPPING SADDLE	0+410	2.0m LT.		92.20 (ASSUMED)	CONNECT TO EX. 750mm (30") HYPRESCON WATERMAIN AWWA
150 TO 100mm REDUCER	0+419.2	4.0m ±LT.		95.30 (ASSUMED)	CONNECT TO EX. 100x150mm CROSS



Sanitary tees locations on Spruce Street Oakville East of Manhole No. 4 to Manhole No. 5

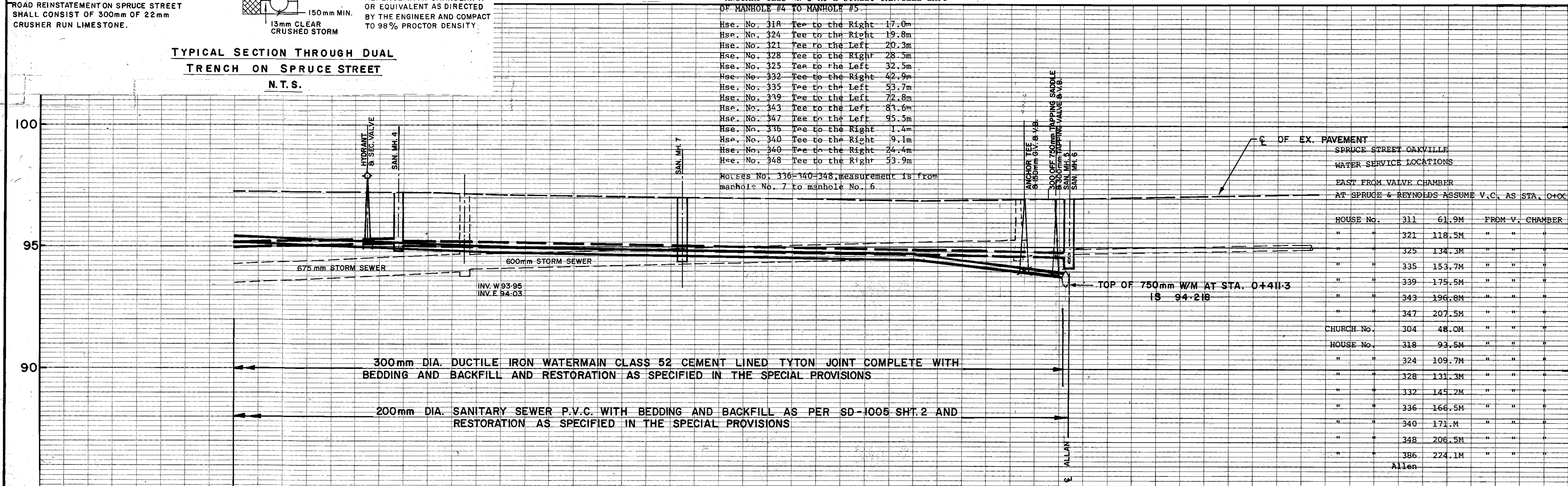
Hse. No. 318 Tee to the Right 4.1m  
 Hse. No. 324 Tee to the Right 10.1m  
 Hse. No. 321 Tee to the Left 12.8m

- NOTES
- SANITARY SEWER LATERALS REPLACED TO SOLID PIPE (OR TO LIMIT OF R) AND RECONNECTED TO NEW SEWER.
  - WATER SERVICE LATERALS INSTALLED PER STD. DWG. 431.
  - WHERE THE WATERMAIN CROSSES UNDER A SANITARY OR STORM LATERAL, THE CONTRACTOR SHALL PROVIDE CONCRETE ENCASUREMENT OF THE SEWER AND WATERMAIN.

SANITARY TEES ON SPRUCE STREET OAKVILLE EAST OF MANHOLE #4 TO MANHOLE #5

Hse. No. 318	Tee to the Right	17.0m
Hse. No. 324	Tee to the Right	19.8m
Hse. No. 321	Tee to the Left	20.3m
Hse. No. 328	Tee to the Right	28.5m
Hse. No. 325	Tee to the Left	32.5m
Hse. No. 332	Tee to the Right	42.9m
Hse. No. 335	Tee to the Left	53.7m
Hse. No. 339	Tee to the Left	72.8m
Hse. No. 343	Tee to the Left	81.0m
Hse. No. 347	Tee to the Left	95.5m
Hse. No. 346	Tee to the Right	1.4m
Hse. No. 340	Tee to the Right	9.1m
Hse. No. 340	Tee to the Right	24.4m
Hse. No. 348	Tee to the Right	53.9m

NOTES: Nos. 336-340 measurement is from manhole No. 7 to manhole No. 6



SPRUCE STREET OAKVILLE WATER SERVICE LOCATIONS EAST FROM VALVE CHAMBER AT SPRUCE & REYNOLDS ASSUME V.C. AS STA. 0+000

HOUSE No.	Distance from V. Chamber	From V. Chamber
311	61.9M	"
321	118.5M	"
325	134.3M	"
335	153.7M	"
339	175.5M	"
343	196.8M	"
347	207.5M	"
CHURCH No.	304	48.0M
HOUSE No.	318	93.5M
"	324	109.7M
"	328	131.3M
"	332	145.2M
"	336	166.5M
"	340	171.1M
"	348	206.5M
"	385	224.1M

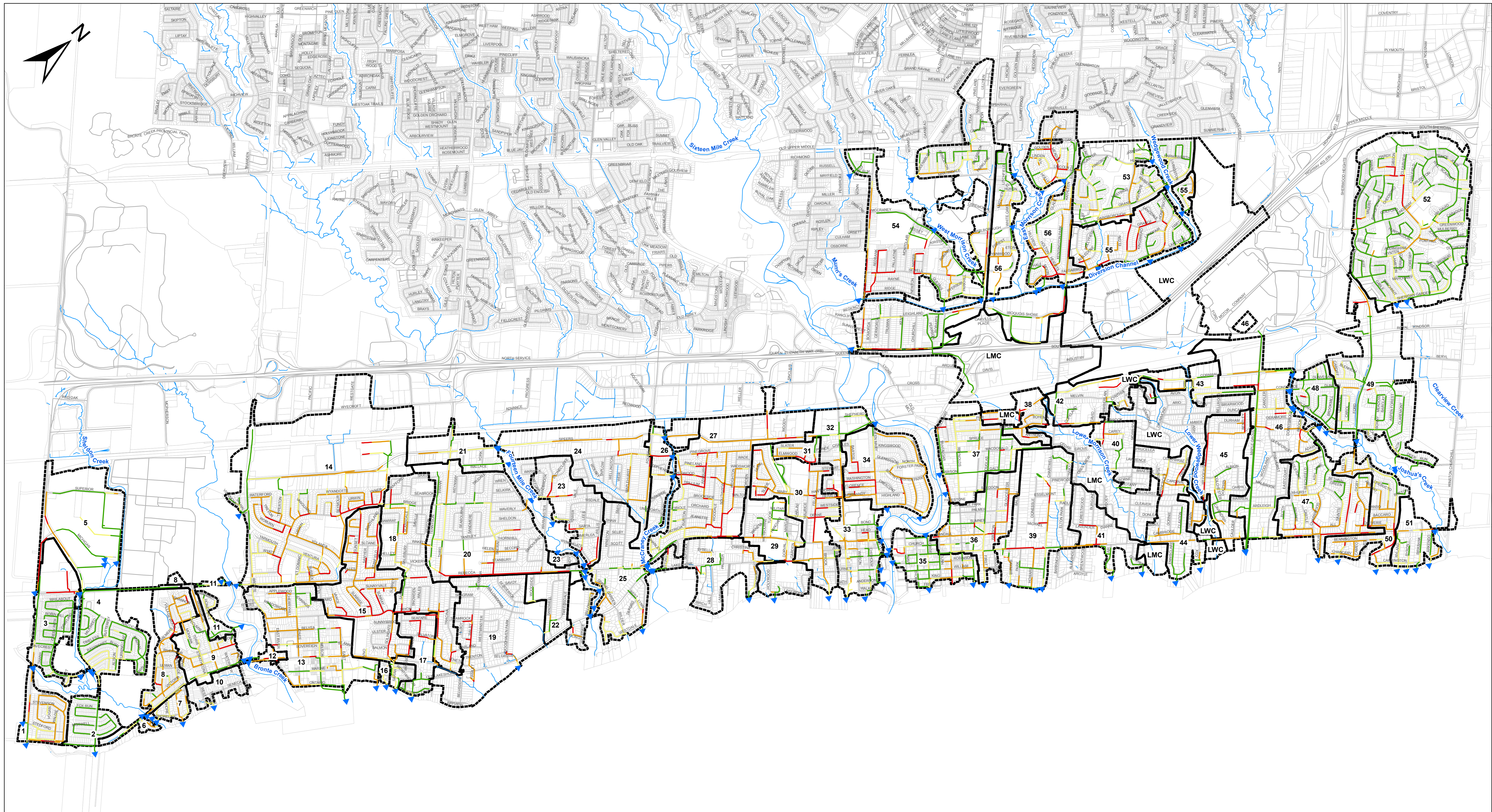
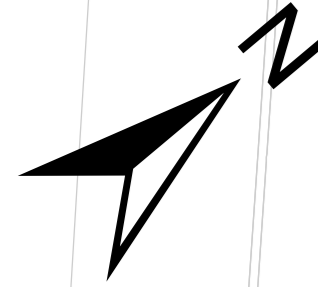
Allen

SANITARY INVERTS	100.2m AT +0.47%	137.2m AT -0.38%	SANITARY INVERTS														
WATERMAIN INVERTS	117.7m AT 0.79%	115.0m AT 0.30%	WATERMAIN INVERTS														
CHAINAGE	0+240	0+260	0+274.2	0+280	0+295	0+300	0+320	0+340	0+360	0+380	0+400	0+402.2	0+409.4	0+420	0+440	0+460	CHAINAGE

2	AUG/82	J.S.	"AS-CONSTRUCTED"
1	8/09/23	M.J.H.	REVISE PROP. STM. SEWER SIZE.
No	Date	By	REVISIONS
Design	G.E.R.	Checked	Date
Drawn	M.J.H.	Checked	AUGUST 1981
Scale	HORIZ. 1:100	VERT. 1:20	REFERENCES
APPROVALS			FIELD NOTES
Municipal			STAMP
DIRECTOR OF PUBLIC WORKS			
Regional			
DIRECTOR OF PUBLIC WORKS			
MANAGER OF DESIGN (1981 08 2)			
MUNICIPALITY		REGIONAL MUNICIPALITY OF HALTON	
TOWN OF OAKVILLE		PUBLIC WORKS DEPARTMENT	
PUBLIC WORKS DEPARTMENT		PUBLIC WORKS DEPARTMENT	
TITLE		300mm Ø WATERMAIN	
MUNICIPAL DRAWING NO.		REGIONAL DRAWING NO.	
CONTRACT NO.		0-4400	
WS-579-81		SHEET 2 OF 12	







Legend	
	Network
	Parcels
	Streams
	Roads
	Outfalls
Minor System Performance	
	Unsurcharged
	Below 1/2 Surcharging Depth and Above Obvert
	Above 1/2 Surcharging Depth and Below Rim Elevation
	Surcharged Above Rim Elevation

**Stormwater Management  
Master Plan**

**Phase 2**

**Town of Oakville**

**5 Year Storm Event  
Urban and Hybrid  
Performance Assessment**

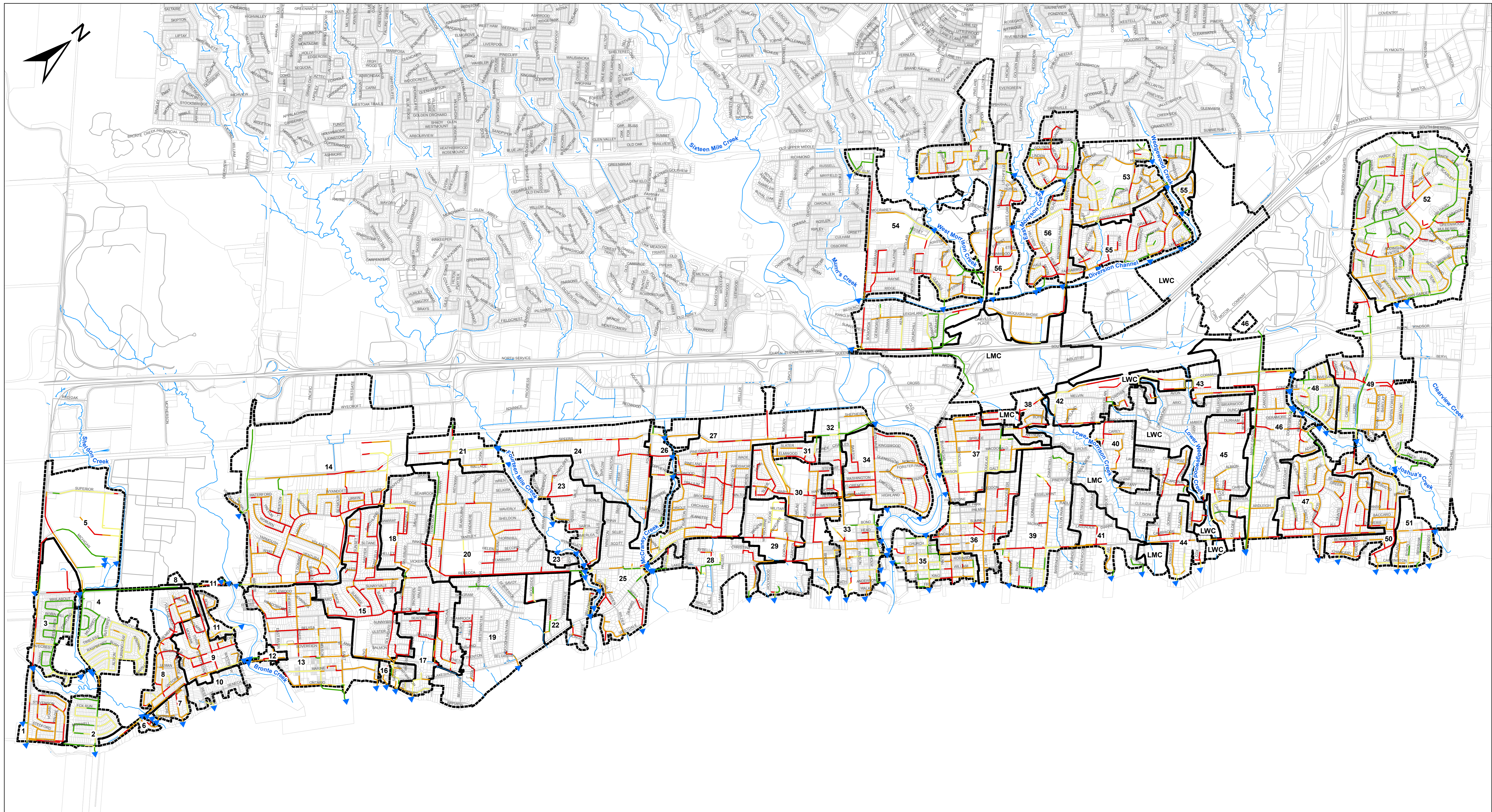
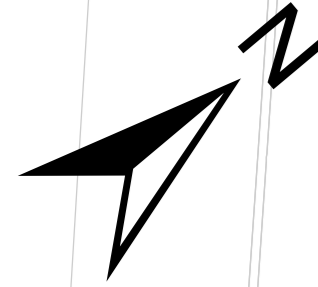
**-  
Existing Condition**





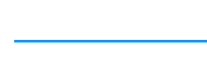






Scale **1:17,000**

Project No.  
**TP 115045**

Drawing No.  
**7.3**



**Legend**

-  Network
  -  Parcels
  -  Streams
  -  Roads
  -  Outfalls
- Minor System Performance**
-  Unsurcharged
  -  Below 1/2 Surcharging Depth and Above Obvert
  -  Above 1/2 Surcharging Depth and Below Rim Elevation
  -  Surcharged Above Rim Elevation

**Stormwater Management  
Master Plan**

**Phase 2**

**Town of Oakville**

**100 Year Storm Event  
Minor System  
Performance**

**-  
Existing Condition**



Scale **1:17,000**

0 250 500 1,000 1,500 Meters

Project No.  
**TP 115045**

Drawing No.  
**7.4**

## **APPENDIX 'C'**

Estimated Water Demand

Estimated Sanitary Flow



**TRAFALGAR ENGINEERING LTD.**

**ESTIMATED PROPOSED WATER DEMAND**

**Project:** Spruce Rose Inc.  
**Desc:** Draft Plan of Subdivision

**Project No.:** 1819  
**Prepared By:** MW  
**Checked By:** PC

Land Use / Occupancy Type	Occupancy Data					Peaking Factors			Demand Flow		
	Site Area (ha)	Population Density (pers/ha)	Eq. Population (cap.)	Per Cap. Demand (L/cap. Day)	Average Daily Demand (L/min)	Min. Hour	Peak Hour	Max. Daily	Min. Hour Demand (L/min)	Max. Hour Demand (L/min)	Max. Daily Demand (L/min)
Single Family Residential	0.07	55	4	191	0.5	1.00	4.00	2.25	0.5	1.9	1.1
											0.0
<b>TOTAL</b>	<b>0.07</b>		<b>4</b>		<b>0.5</b>				<b>0.5</b>	<b>1.9</b>	<b>1.1</b>

**Fire Flow**

Using Fire Underwriters Survey Methodology:

**Average Daily Demand:** 0.5 (L/min)  
**Minimum Hourly Demand:** 0.5 (L/min)  
**Maximum Hourly Demand:** 1.9 (L/min)  
**Maximum Daily Demand:** 1.1 (L/min)  
**Max. Daily Plus Fire:** 5001.1 (L/min)

1. An estimate of the fire flow is given by the formula  $F = 220C\sqrt{A}$   
 Where:  
 F = The required fire flow in litres per minute  
 C = Coefficient related to the type of construction  
 A = The total floor area in square metres (including all storeys but excluding basements at least 50% below grade)

Type of Construction: **Ordinary** Coefficient: 1.00 Total Floor Area: **383** (m<sup>2</sup>)  
 F = **4000** (L/min) Adequately Protected Vertical Openings: **No**

**Area Note:** For adequately protected vertical openings consider only the area of the largest floor plus 25% of each of the two immediately adjoining floors.

2. Adjust the value in No. 1 for occupancy surcharge/reduction  
 Occupancy Contents: **Combustible** Factor: 0%  
 F = **4000** (L/min)

3. Adjust the value in No. 2 for sprinkler
- |                        |            |            |            |
|------------------------|------------|------------|------------|
| NFPA 13 Sprinkler:     | <b>No</b>  | Reduction: | <b>20%</b> |
| Standard Water Supply: | <b>Yes</b> | Reduction: | <b>10%</b> |
| Fully Supervised:      | <b>No</b>  | Reduction: | <b>10%</b> |

4. Adjust the value in No. 2 for exposure
- |                             | Separation (m)      | Charge |
|-----------------------------|---------------------|--------|
| North                       | <b>2.5</b>          | 25%    |
| East                        | <b>10</b>           | 15%    |
| South                       | <b>2.5</b>          | 25%    |
| West                        | <b>30</b>           | 5%     |
| <b>Total Reduction:</b>     | <b>40%</b>          |        |
| <b>Sprinkler Reduction:</b> | <b>1600</b> (L/min) |        |
| <b>Total Charge:</b>        | <b>70%</b>          |        |
| <b>Exposure Charge:</b>     | <b>2800</b> (L/min) |        |

5. Estimated Fire Flow is value in No. 2 less *Sprinkler Reduction* plus *Exposure Charge*, rounded to the nearest 1000  
 F = **5000** (L/min)

**TRAFALGAR ENGINEERING LTD.**

**ESTIMATED PROPOSED WATER DEMAND**

**Project:** Spruce Rose Inc.  
**Desc:** Draft Plan of Subdivision

**Project No.:** 1819  
**Prepared By:** MW  
**Checked By:** PC

Land Use / Occupancy Type	Occupancy Data					Peaking Factors			Demand Flow		
	Site Area (ha)	Population Density (pers/ha)	Eq. Population (cap.)	Per Cap. Demand (L/cap. Day)	Average Daily Demand (L/min)	Min. Hour	Peak Hour	Max. Daily	Min. Hour Demand (L/min)	Max. Hour Demand (L/min)	Max. Daily Demand (L/min)
Single Family Residential	0.07	55	4	191	1	1.00	4.00	2.25	1	2	1
											0
<b>TOTAL</b>	<b>0.07</b>		<b>4</b>		<b>1</b>				<b>1</b>	<b>2</b>	<b>1</b>

**Fire Flow**

Using Fire Underwriters Survey Methodology:

**Average Daily Demand:** 0.5 (L/min)  
**Minimum Hourly Demand:** 0.5 (L/min)  
**Maximum Hourly Demand:** 2 (L/min)  
**Maximum Daily Demand:** 1.1 (L/min)  
**Max. Daily Plus Fire:** 5001.1 (L/min)

1. An estimate of the fire flow is given by the formula  $F = 220C\sqrt{A}$   
 Where:  
 F = The required fire flow in litres per minute  
 C = Coefficient related to the type of construction  
 A = The total floor area in square metres (including all storeys but excluding basements at least 50% below grade)

Type of Construction: **Ordinary** Coefficient: 1.00 Total Floor Area: **400** (m<sup>2</sup>)  
 F = **4000** (L/min) Adequately Protected Vertical Openings: **No**

**Area Note:** For adequately protected vertical openings consider only the area of the largest floor plus 25% of each of the two immediately adjoining floors.

2. Adjust the value in No. 1 for occupancy surcharge/reduction  
 Occupancy Contents: **Combustible** Factor: 0%  
 F = **4000** (L/min)

3. Adjust the value in No. 2 for sprinkler
- |                             |            |            |                     |
|-----------------------------|------------|------------|---------------------|
| NFPA 13 Sprinkler:          | <b>Yes</b> | Reduction: | <b>20%</b>          |
| Standard Water Supply:      | <b>Yes</b> | Reduction: | <b>10%</b>          |
| Fully Supervised:           | <b>Yes</b> | Reduction: | <b>10%</b>          |
| <b>Total Reduction:</b>     |            |            | <b>40%</b>          |
| <b>Sprinkler Reduction:</b> |            |            | <b>1600 (L/min)</b> |

4. Adjust the value in No. 2 for exposure
- |                         |                |                     |
|-------------------------|----------------|---------------------|
|                         | Separation (m) | Charge              |
| North                   | <b>30</b>      | 5%                  |
| East                    | <b>2.5</b>     | 25%                 |
| South                   | <b>30</b>      | 5%                  |
| West                    | <b>2.5</b>     | 25%                 |
| <b>Total Charge:</b>    |                | <b>60%</b>          |
| <b>Exposure Charge:</b> |                | <b>2400 (L/min)</b> |

5. Estimated Fire Flow is value in No. 2 less *Sprinkler Reduction* plus *Exposure Charge*, rounded to the nearest 1000  
 F = **5000** (L/min)

# TRAFALGAR ENGINEERING LTD.

## ESTIMATED PROPOSED SANITARY FLOW

**Project:** Spruce Rose Inc.  
**Desc:** Draft Plan of Subdivision

**Project No.:** 1819  
**Prepared By:** MW  
**Checked By:** PC

### Residential

Land Use / Occupancy Type	Site Area (ha)	Population Density (pers/ha)	Eq. Population (cap.)	Per Cap. Demand (L/cap. Day)	Average Daily Dry Weather Flow (L/s)
Single Family Residential	0.41	55.0	23	275	0.07
<b>TOTAL</b>	<b>0.41</b>		<b>23</b>		<b>0.07</b>

### Industrial / Commercial / Institutional

Land Use / Occupancy Type	Site Area (ha)	Population Density (pers/ha)	Eq. Population (cap.)	Unit Sewage Flow (L/Ha. Day)	Average Daily Dry Weather Flow (L/s)
			0	24750	0.0
<b>TOTAL</b>	<b>0.00</b>		<b>0</b>		<b>0.00</b>

Residential Peaking Factor:	4.37
ICI Peaking Factor:	4.50
Include ICI Peaking?	No
Tributary Area:	0.41 (ha)
Infiltration Allowance:	0.286 (L/s ha)
Foundation Drain Allowance:	0.00 (L/s ha)

Residential + Infiltration Avg Flow:	0.19 (L/s)
ICI Average Flow:	0.00 (L/s)
Groundwater Discharge:	(L/s)
<b>Total Average Flow:</b>	<b>0.19 (L/s)</b>

Residential Peak + Infiltration Flow:	0.43 (L/s)
ICI Peak Flow:	0.00 (L/s)
Groundwater Discharge:	(L/s)
<b>Total Peak Flow:</b>	<b>0.43 (L/s)</b>

## **APPENDIX 'D'**

Cover Sheet

Erosion and Sediment Control Plan

General Servicing Plan

Storm Drainage Area Plan

Sanitary Drainage Area Plan

Composite Utility Plan

Grading Plan

Sections and Details Plan

Standard Notes

# SPRUCE ROSE INC. SUBDIVISION

24T-XXXXXX/XXX

20M-XXXX

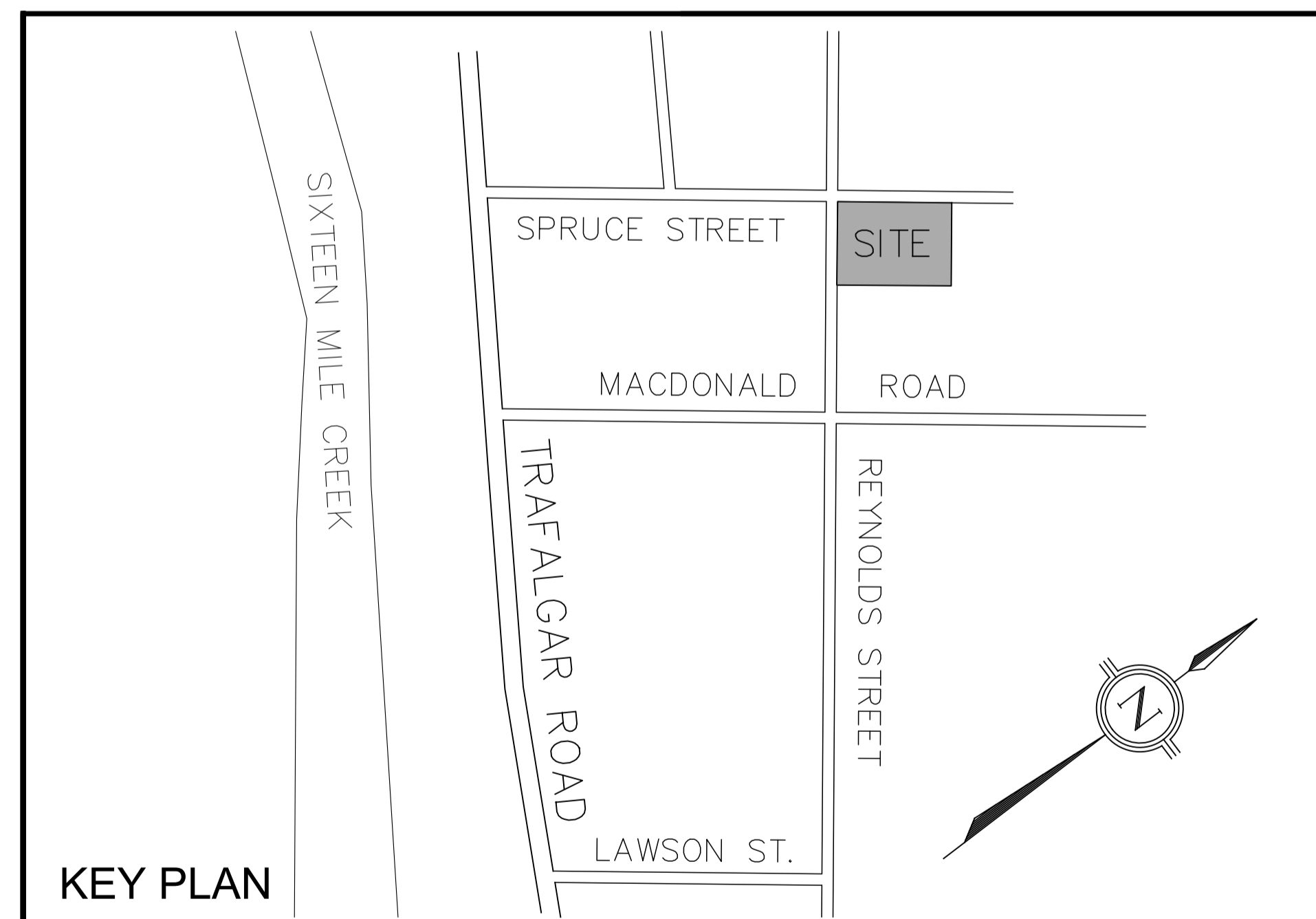
308 & 318 SPRUCE STREET

TOWN OF OAKVILLE



## DRAWING INDEX

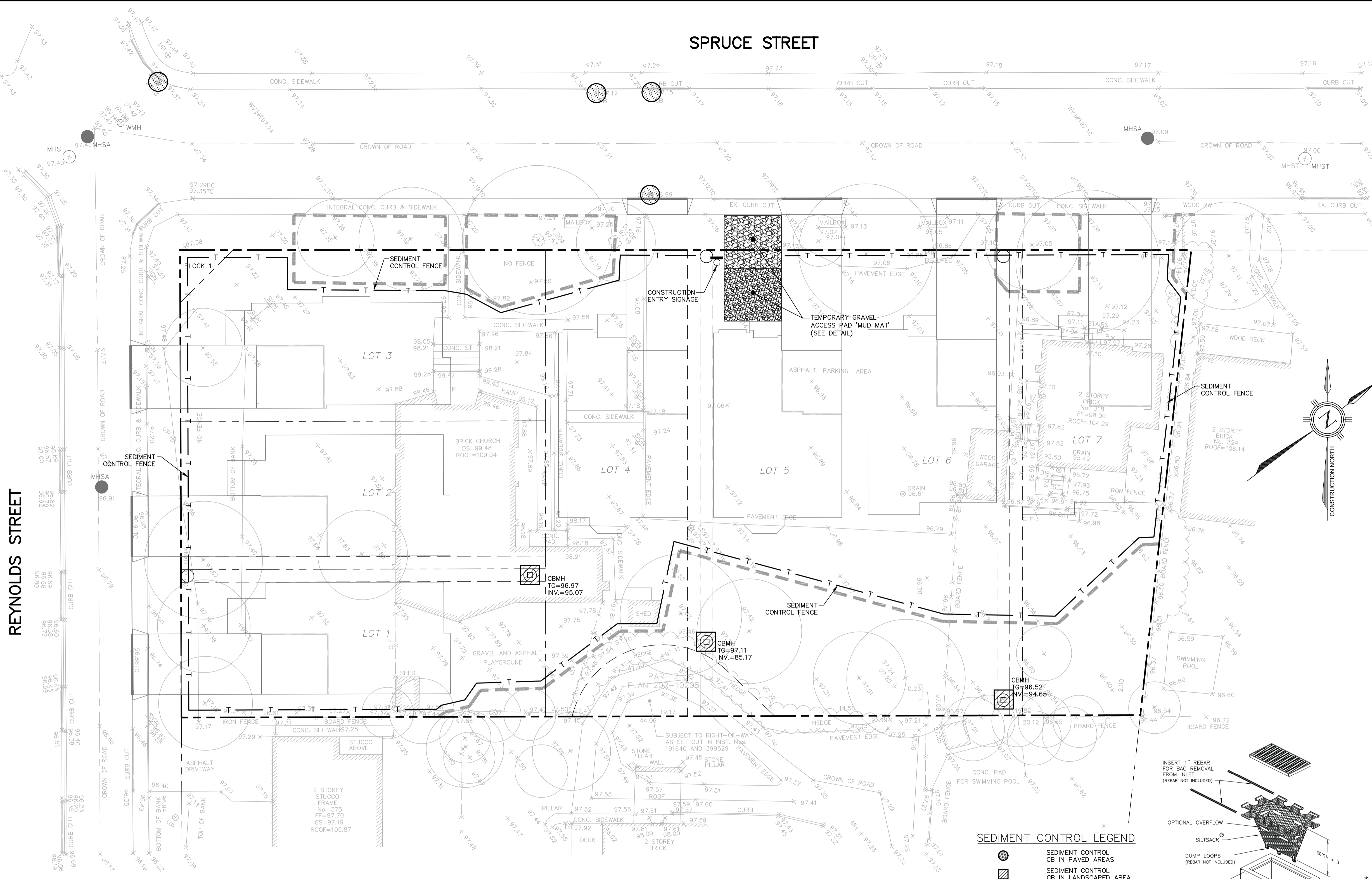
<u>Sheet</u>	<u>Title</u>
E1	EROSION AND SEDIMENT CONTROL PLAN
S1	GENERAL SERVICING PLAN
S2	STORM DRAINAGE AREA PLAN
S3	SANITARY DRAINAGE AREA PLAN
CU1	COMPOSITE UTILITY PLAN
G1	GRADING PLAN
D1	SECTIONS AND DETAILS PLAN
N1	STANDARD NOTES



 **TRAFALGAR  
ENGINEERING**  
#1-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
www.trafalgareng.com

CONSULTANT FILE: 1819  
TOWN FILE: 24T-XXXXX

SPRUCE STREET



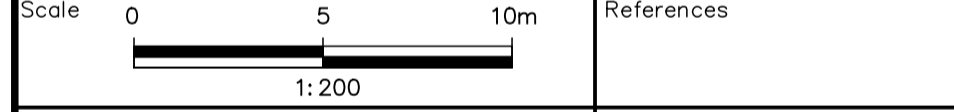
- LEGEND**
- ⊕ PROPOSED CATCHBASIN MANHOLE
  - ⊙ PROPOSED STORM MANHOLE
  - ⊗ PROPOSED VALVE & BOX
  - PROPOSED CURB STOP
  - EXISTING CURB STOP
  - PROPERTY LINE
  - - - SUBDIVISION LOT LINE
  - 96.88 EXISTING ELEVATION
  - PROPOSED DRAINAGE DIRECTION
  - PROPOSED SWALE DRAINAGE DIRECTION
  - TREE PROTECTION FENCE (GREEN PRINT CONSULTING, 2023)

**BENCHMARK**  
 ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928/1978).

**NOTE**  
 THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	07/12/23	MW/MW	ISSUED FOR COORDINATION
No	DD/MM/YY	By/DRN	REVISIONS

Design	MW	Chk'd	PC	Cad File	1819E.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24



**APPROVALS**

Municipal: APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.

Manager of Development Services: \_\_\_\_\_ Date: \_\_\_\_\_

Regional Approval: \_\_\_\_\_

DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

PROFESSIONAL ENGINEER: P. CIFON (Seal: Feb 29, 2024)

**TRAFALGAR ENGINEERING**  
 81-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
 www.trafalgareng.com

**OAKVILLE Halton REGION**

**PROJECT**  
 SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION

**DRAWING TITLE**  
 EROSION AND SEDIMENT CONTROL PLAN

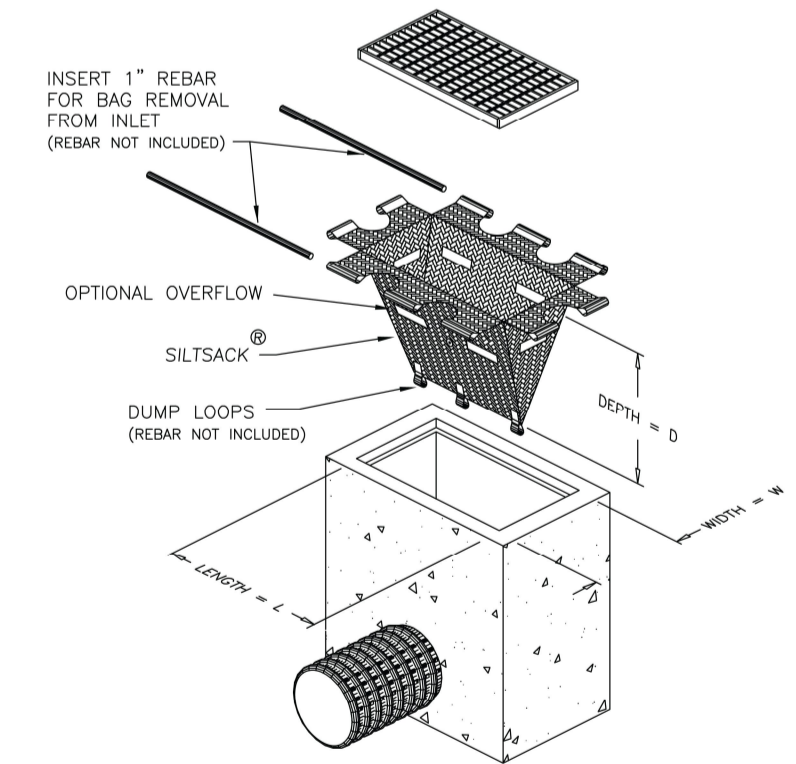
Municipal No.	24T-XXXX	Regional No.	1819
Contract No.	-	Consultant No.	1819
		Sheet	E1

**EROSION AND SEDIMENT CONTROL NOTES**

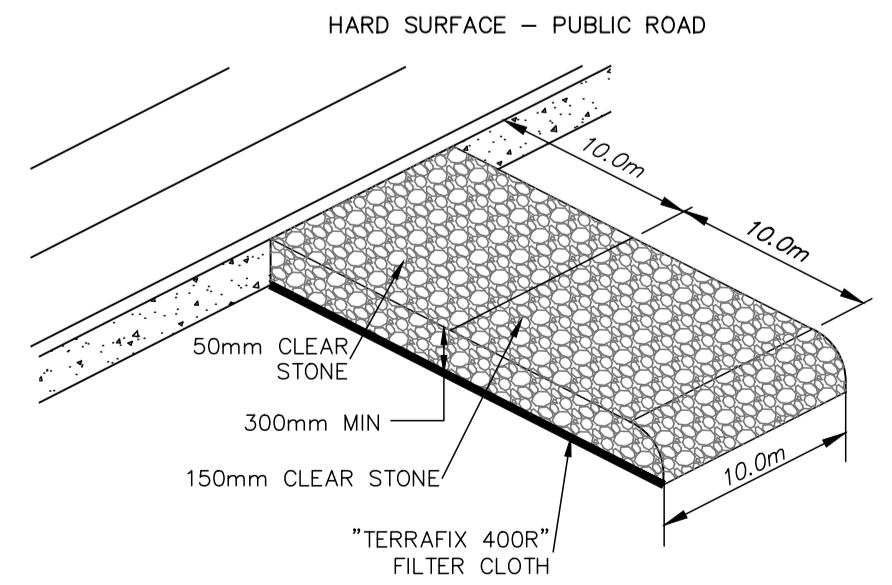
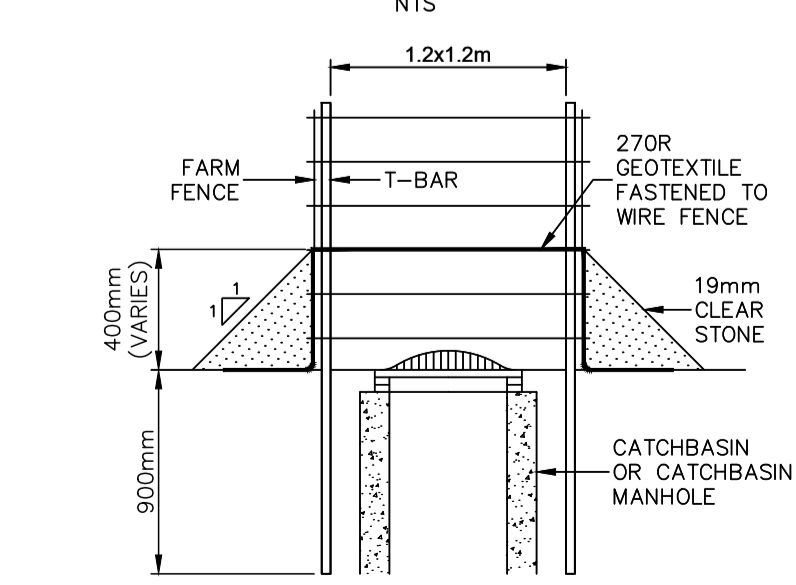
1. ALL EROSION AND SEDIMENT MEASURES/DEVICES SHALL BE INSTALLED PRIOR TO ANY SITE DISTURBANCE/CONSTRUCTION
2. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE INSPECTED, REPAIRED/MAINTAINED WEEKLY AND FOLLOWING ALL SIGNIFICANT RAINFALLS.
3. THE MEASURES AS PROPOSED MAY BE MODIFIED AT THE DISCRETION OF THE ENGINEER TO SUIT THE PROPOSED CONSTRUCTION PROGRAMS. THE GENERAL INTENT OF THE PROPOSED EROSION CONTROL MEASURES WILL BE MAINTAINED AT ALL TIMES.
4. DECOMMISSIONING OF ALL EROSION CONTROL MEASURES SHALL OCCUR ONLY ONCE VEGETATIVE COVER IS ESTABLISHED.
5. DESIGNATED ENTRANCE FOR ALL CONSTRUCTION TRAFFIC TO BE INSTALLED WITH MUD CONTROL DEVICE AS PER MUD MAT DETAIL. MUD CONTROL DEVICES TO BE INSTALLED PRIOR TO START OF CONSTRUCTION AND ARE TO BE MAINTAINED IN GOOD WORKING ORDER UNTIL GRADING WORKS ARE COMPLETED. MUD MAT MAY BE DELETED WITH THE APPROVAL OF THE TOWN OF OAKVILLE.
6. ANY DISTURBED AREA NOT SCHEDULED FOR FURTHER CONSTRUCTION WITHIN 30 DAYS SHALL BE PROVIDED WITH A TEMPORARY SEED.
7. INSTALL CATCHBASIN SEDIMENT CONTROL ON EXISTING CATCHBASINS PRIOR TO START OF CONSTRUCTION.
8. INSTALL CATCHBASIN SEDIMENT CONTROL ON NEW CATCHBASINS AT TIME OF INSTALLATION.
9. EROSION AND SEDIMENT CONTROLS SHALL BE INSPECTED BY THE BUILDER/DEVELOPER:
  - WEEKLY
  - BEFORE AND AFTER ANY PREDICTED RAINFALL EVENT
  - FOLLOWING AN UNPREDICTED RAINFALL EVENT
  - DAILY, DURING EXTENDED DURATION RAINFALL EVENTS
  - AFTER SIGNIFICANT SNOW MELT EVENTS
10. WHERE A SITE REQUIRES DEWATERING AND WHERE THE EXPELLED WATER CAN BE FREELY RELEASED TO A SUITABLE RECEIVER, THE EXPELLED WATER SHALL BE TREATED TO CAPTURE SUSPENDED PARTICLES GREATER THAN 40 MICRON IN SIZE. THE CAPTURED SEDIMENT SHALL BE DISPOSED OF PROPERLY PER MOECC GUIDELINES. THE CLEAN EXPELLED WATER SHALL BE FREELY RELEASED TO A SUITABLE RECEIVER THAT DOES NOT CREATE DOWNSTREAM ISSUES INCLUDING BUT NOT LIMITED TO EROSION, FLOODING - NUISANCE OR OTHERWISE, INTERFERENCE ISSUES, ETC.
11. EXISTING STORM SEWER AND DRAINAGE DITCHES ADJACENT TO THE WORKS SHALL BE PROTECTED AT ALL TIMES FROM THE ENTRY OF SEDIMENT/SILT THAT MAY MIGRATE FROM THE SITE. FOR STORM SEWERS: ALL INLETS (REAR LOT CATCHBASINS, ROAD CATCHBASINS, PIPE INLETS, ETC.) MUST BE SECURED/FITTED WITH SILTATION CONTROL MEASURES. FOR DRAINAGE DITCHES: THE INSTALLATION OF ROCK CHECK DAMS, SILTATION FENCE, SEDIMENT CONTAINMENT DEVICES MUST BE INSTALLED TO TRAP AND CONTAIN SEDIMENT. THESE SILTATION CONTROL DEVICES SHALL BE INSPECTED AND MAINTAINED PER ITEMS B AND C ABOVE.
12. IN THE EVENT OF A SPILL (RELEASE OF DELETERIOUS MATERIAL) ON OR EMANATING FROM THE SITE, THE OWNER OR OWNERS AGENT SHALL IMMEDIATELY NOTIFY ALL APPLICABLE AGENCIES INCLUDING BUT NOT LIMITED TO MOECC, LOCAL AND REGIONAL AUTHORITIES AND FOLLOW ANY PRESCRIBED CLEAN UP PROCEDURE. THE OWNER OR OWNERS AGENT WILL ADDITIONALLY IMMEDIATELY NOTIFY THE TOWN.

**SEDIMENT CONTROL LEGEND**

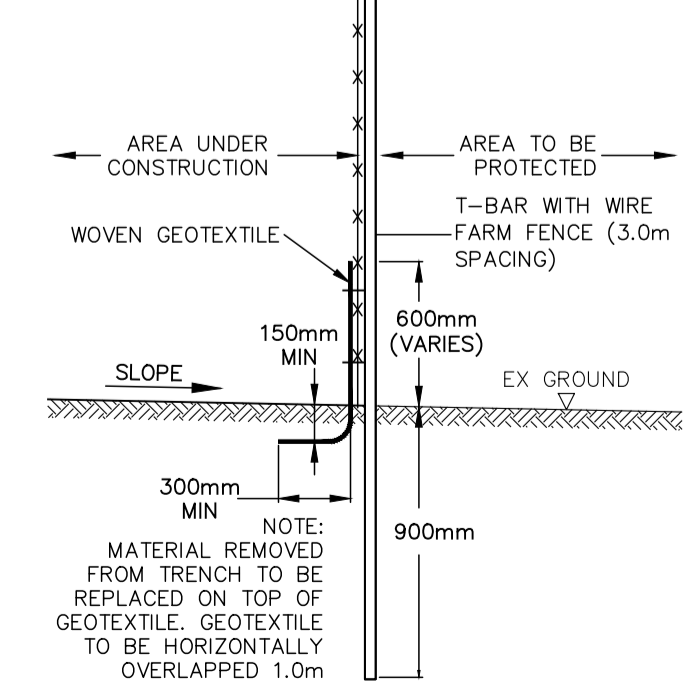
- ⊕ SEDIMENT CONTROL CB IN PAVED AREAS
- ⊙ SEDIMENT CONTROL AREA CB IN LANDSCAPED AREA
- T SEDIMENT CONTROL FENCE
- ▨ MUD MAT
- ~ FIBRE ROLL



**CATCHBASIN SEDIMENT CONTROL IN PAVED AREAS**



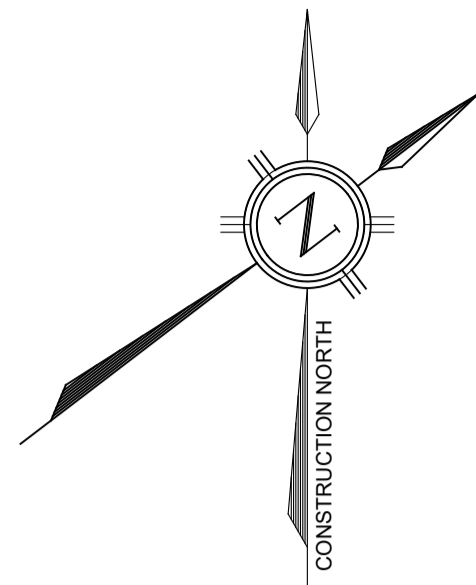
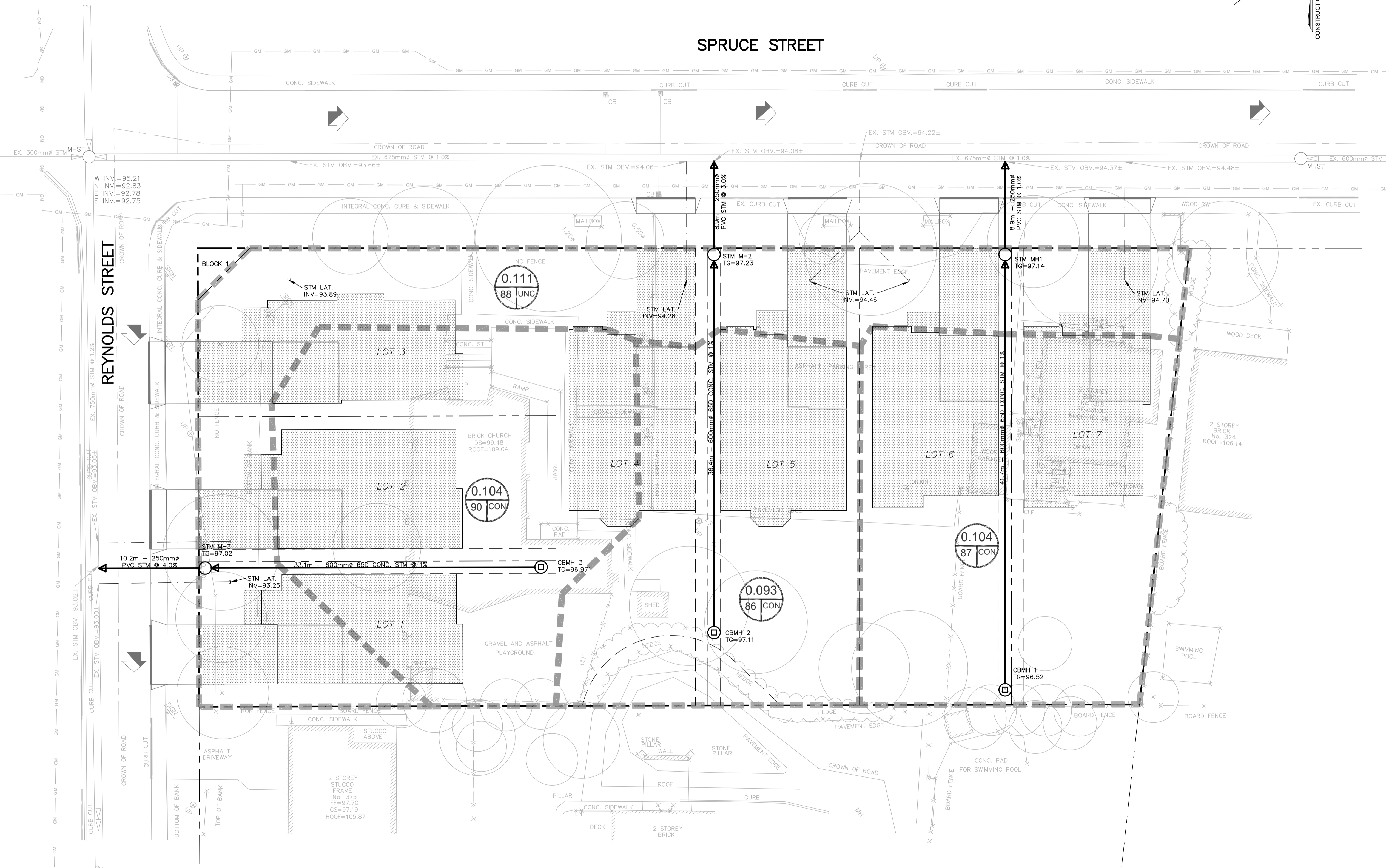
**GRAVEL ACCESS PAD (MUD MAT)**



**SEDIMENT CONTROL FENCE**



FILENAME: P:\1819 Spruce Street Oakville\04-CAD\04-Subdivision\1819S2.dwg  
 C:\DATE: Feb 29, 2024 12:05pm



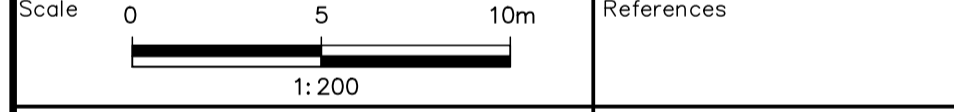
- LEGEND**
- 0.814  
88 UNC DRAINAGE AREA IN HECTARES
  - 88 UNC CONTROLLED/UNCONTROLLED FLOWS
  - SCS CURVE NUMBER
  - STORM DRAINAGE AREA BOUNDARY
  - ⊙ PROPOSED CATCHBASIN MANHOLE
  - ⊙ PROPOSED STORM MANHOLE
  - PROPOSED STORM SEWER
  - PROPERTY LINE
  - PROPOSED STORM LATERAL
  - ➔ OVERLAND FLOW ROUTE
  - IMPERVIOUS AREA

**BENCHMARK**  
 ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD.  
 ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

**NOTE**  
 THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	13/02/24	MW/MW	ISSUED FOR COORDINATION
No	DD/MM/YY	By/DRN	REVISIONS

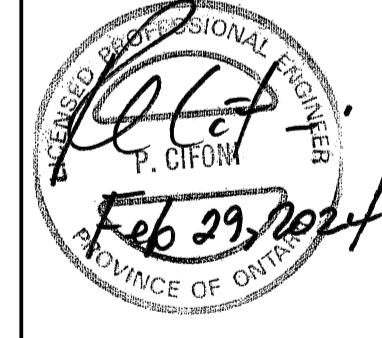
Design	MW	Chk'd	PC	Cad File	1819S2.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24



**APPROVALS**

Municipal  
 APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.  
 Date: \_\_\_\_\_  
 Manager of Development Services

Regional Approval



SIGNED: \_\_\_\_\_ DATE: \_\_\_\_\_  
 LEGISLATIVE AND PLANNING SERVICES DEPT.  
 Consultant

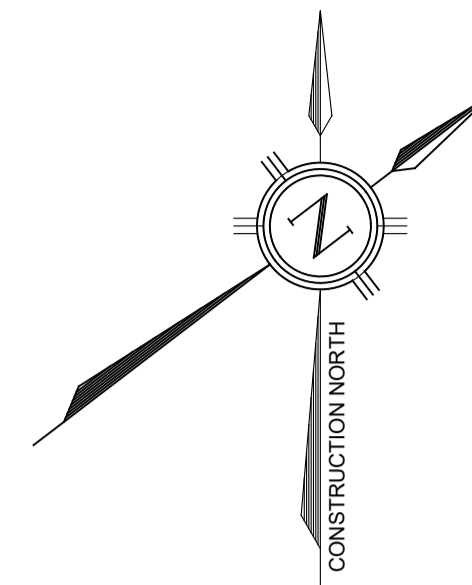
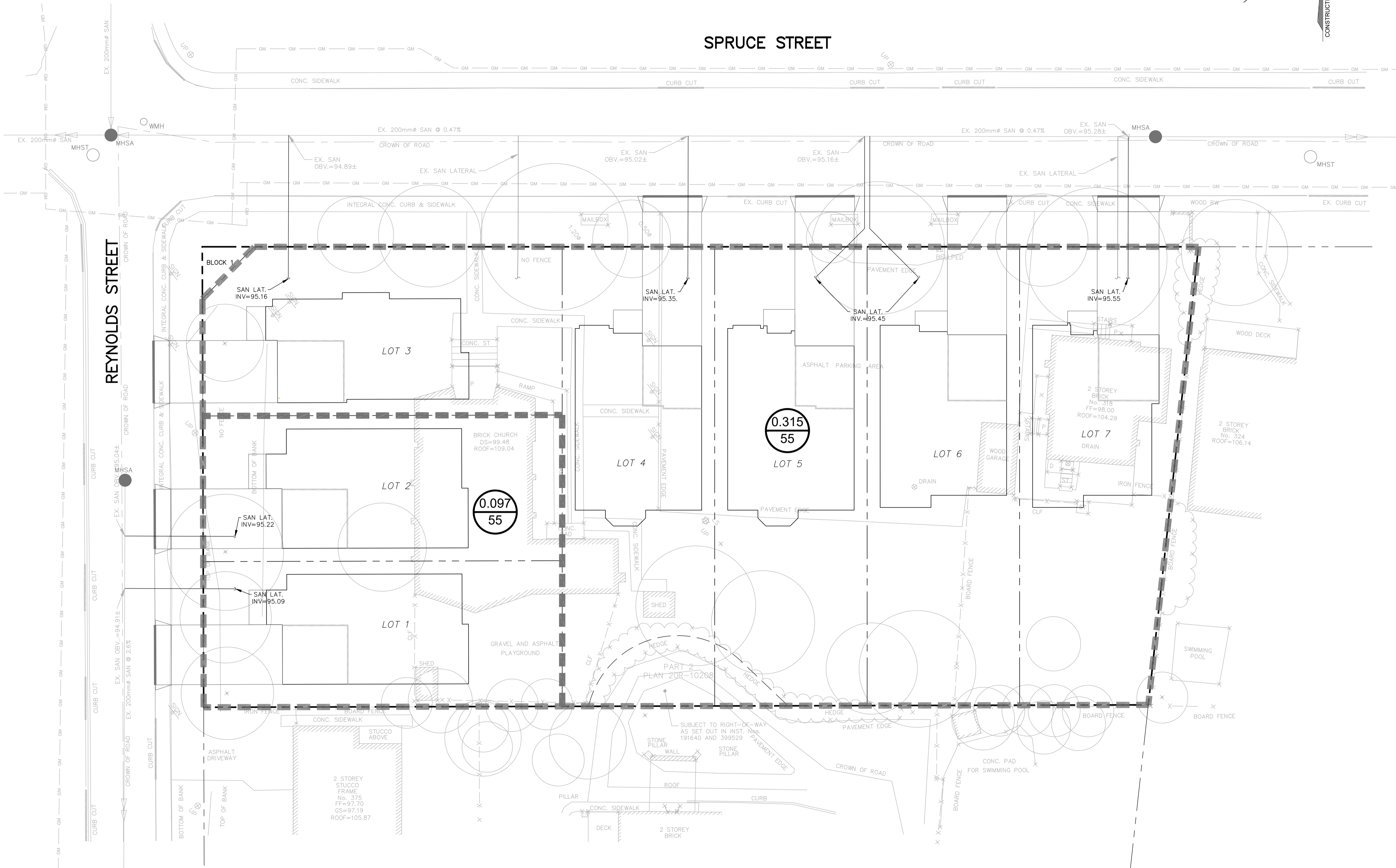


**PROJECT**  
 SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION

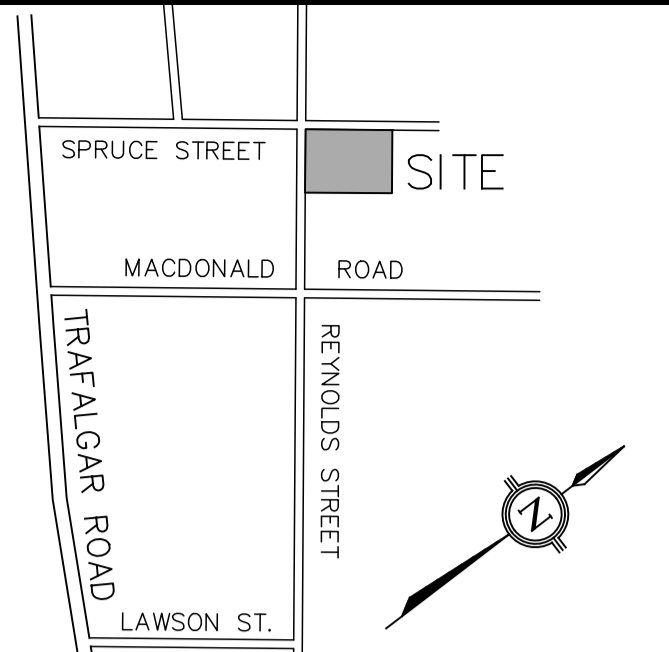
**DRAWING TITLE**  
 STORM DRAINAGE AREA PLAN

Municipal No.	24T-XXXX	Regional No.	
Contract No.	-	Consultant No.	1819
		Sheet	S2





**KEY PLAN**  
NTS



**LEGEND**

- 0.283** DRAINAGE AREA IN HECTARES
- 135** POPULATION DENSITY (PERSONS/HECTARE)
- DRAINAGE AREA BOUNDARY
- - - - - PROPERTY LINE
- EXISTING SANITARY SEWER
- EXISTING SANITARY MANHOLE
- EXISTING SANITARY LATERAL
- PROPOSED SANITARY LATERAL

**BENCHMARK**

ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

**NOTE**

THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	13/02/24	MW/MW	ISSUED FOR COORDINATION

No	DD/MM/YY	By/DRN	REVISIONS

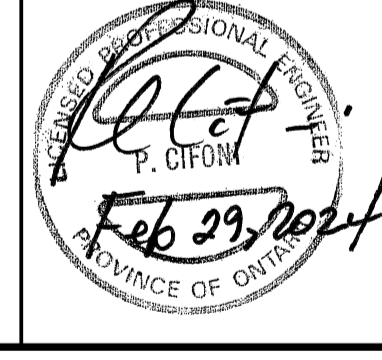
Design	MW	Chk'd	PC	Cad File	1819S3.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24

Scale	0	5	10m
Scale	1:200		

**APPROVALS**

Municipal APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.  
 Date: \_\_\_\_\_  
 Manager of Development Services

Regional Approval  
 DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.  
 SIGNED: \_\_\_\_\_ DATE: \_\_\_\_\_  
 LEGISLATIVE AND PLANNING SERVICES DEPT.  
 Consultant



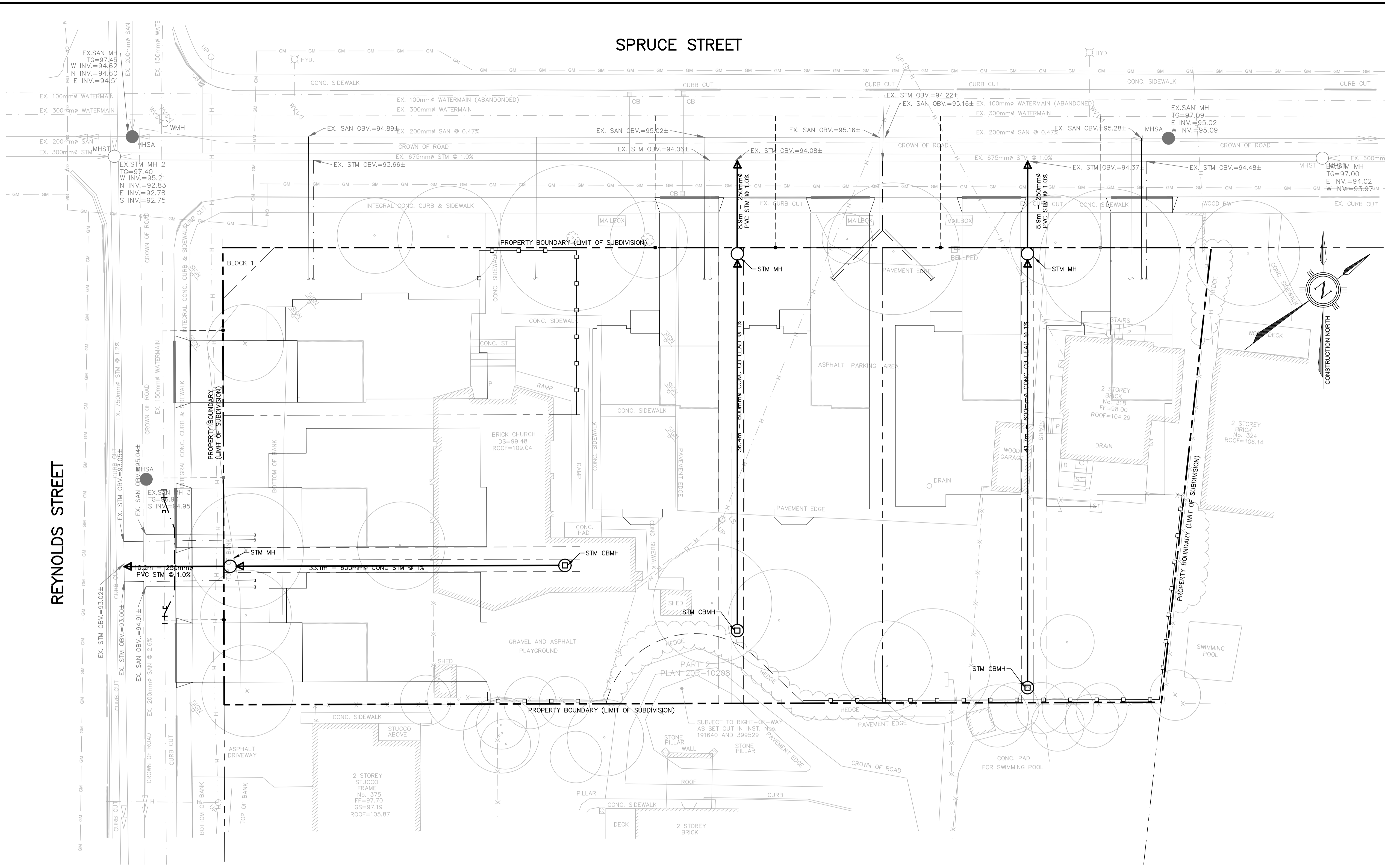
PROJECT  
**SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION**

DRAWING TITLE  
**SANITARY DRAINAGE AREA PLAN**

Municipal No.	24T-XXXX	Regional No.	
Contract No.	-	Consultant No.	1819
		Sheet	S3

SPRUCE STREET

REYNOLDS STREET



KEY PLAN



LEGEND

- PROPOSED CATCHBASIN
- PROPOSED STORM MANHOLE
- PROPOSED VALVE & BOX
- PROPOSED PLUG
- PROPOSED WATER METER
- PROPOSED STORM SEWER
- PROPOSED WATERMAIN
- PROPERTY BOUNDARY
- PROPOSED SUMP PUMP
- PROPOSED WATER SERVICE AND CURB STOP
- PROPOSED SANITARY SERVICE
- PROPOSED STORM SERVICE
- EXISTING STORM SEWER
- EXISTING SANITARY SEWER
- EXISTING WATERMAIN
- EXISTING BURIED GAS MAIN
- EXISTING OVERHEAD WIRE

BENCHMARK

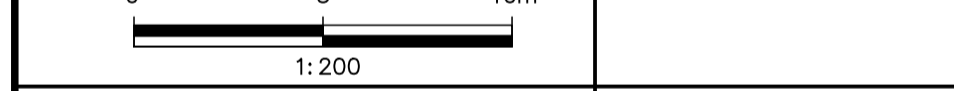
ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 23.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

NOTE

THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

No.	29/02/24	MW/CL	ISSUED FOR ZBA/DPS
No.	07/12/23	MW/MW	ISSUED FOR COORDINATION

Design	MW	Chk'd	PC	Cad File	1819CU.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24



APPROVALS

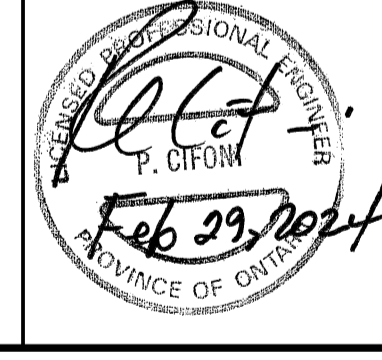
Municipal APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.

Manager of Development Services

Regional Approval

DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

SIGNED: \_\_\_\_\_ DATE: \_\_\_\_\_ LEGISLATIVE AND PLANNING SERVICES DEPT.



BELL CANADA	OAKVILLE HYDRO**
NAME	NAME
DATE	DATE
CANADA POST	COGECO CABLE
NAME	NAME
DATE	DATE
	ENBRIDGE GAS*
	NAME
	DATE

\*GAS LINES ARE SHOWN FOR LOCATION PURPOSES ONLY. GAS WILL BE SUPPLIED ON END USER REQUIREMENTS.

\*\*OAKVILLE HYDRO UTILITY ASSET LOCATIONS SHOWN ON THIS DRAWING ARE BASED ON DESIGN DRAWINGS AND ARE SUBJECT TO CHANGE DURING CONSTRUCTION. OAKVILLE HYDRO RESERVES THE RIGHT TO APPROVE OR DENY TREES IN THE VICINITY OF TRANSFORMERS OR ANY OTHER ASSETS. NO UTILITY PEDESTAL, MAILBOX, TREE AND/OR OTHER ASSETS ALLOWED TO BE INSTALLED ON TOP OF TRENCH.

Consultant

81-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
www.trafalgareng.com

Municipality

PROJECT

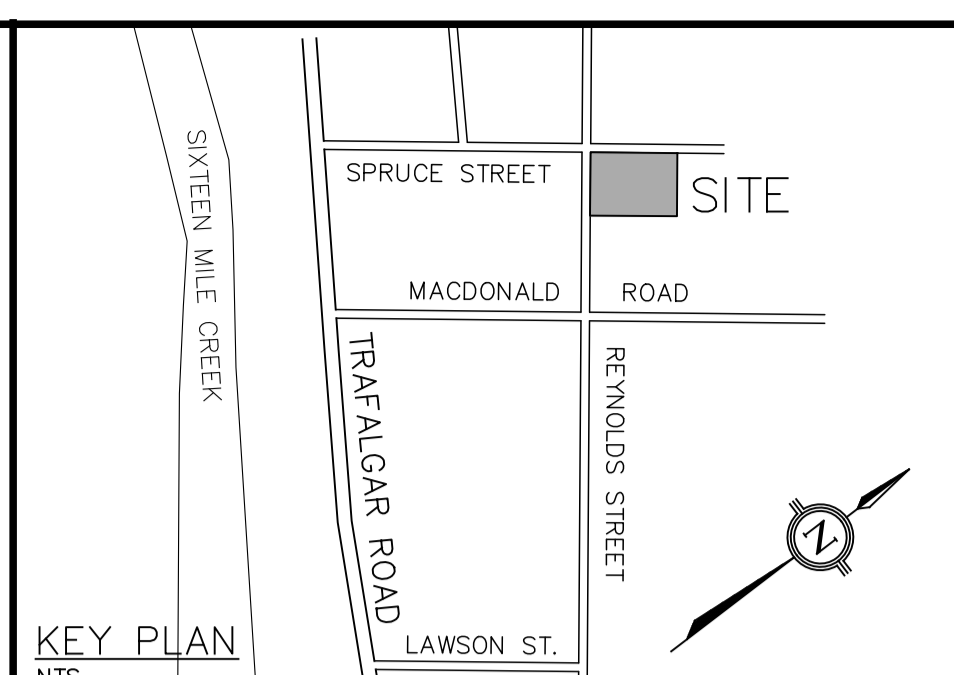
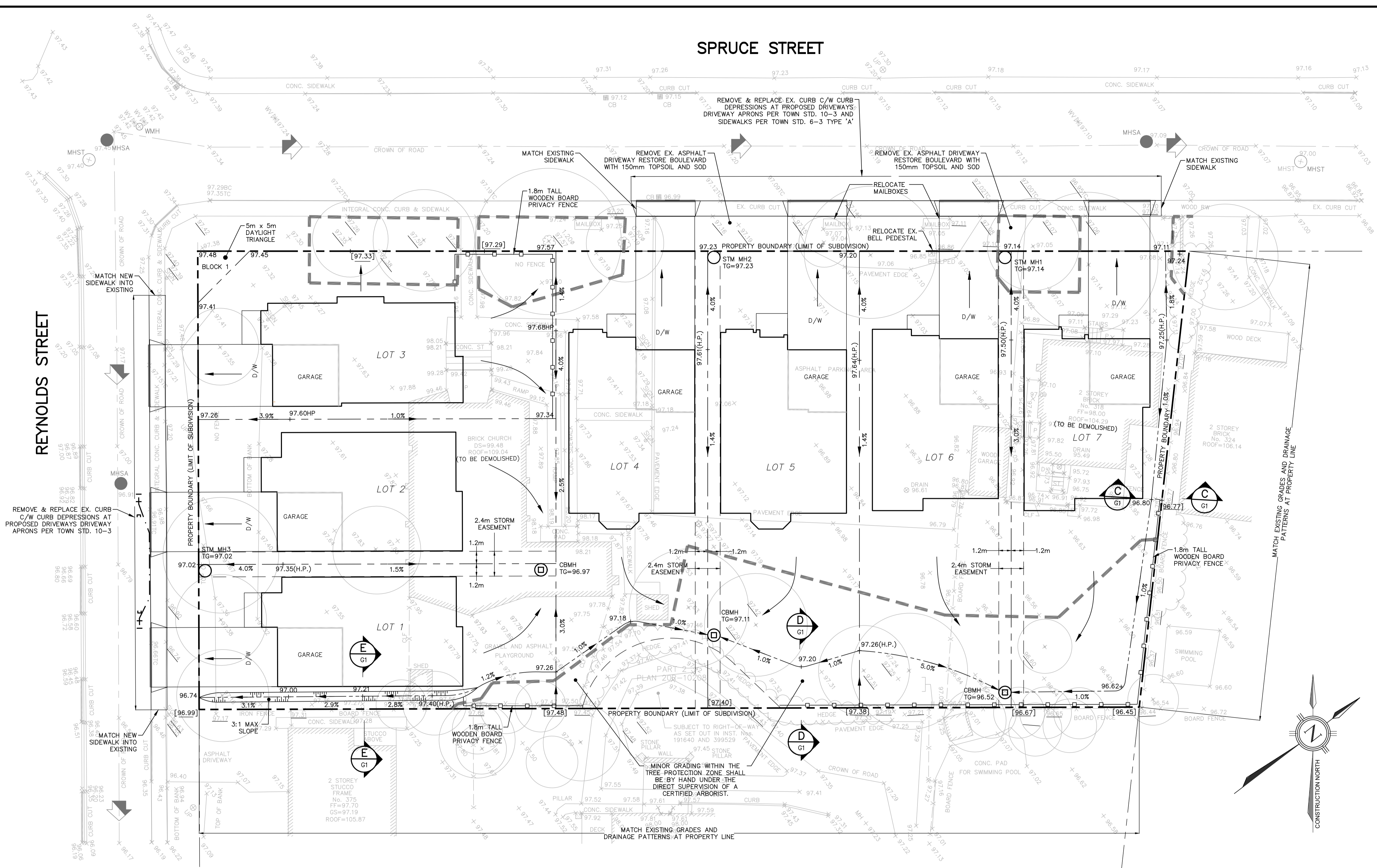
**SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION**

DRAWING TITLE

**COMPOSITE UTILITY PLAN**

Municipal No.	24T-XXXX	Regional No.	1819
Contract No.	-	Consultant No.	1819
		Sheet	CU1

SPRUCE STREET



- LEGEND**
- PROPOSED CATCHBASIN
  - PROPOSED STORM MANHOLE
  - PROPOSED VALVE & BOX
  - 97.57 EXISTING ELEVATION
  - 97.57 EXISTING ELEVATION TO REMAIN
  - [97.57] INTERPOLATED EXISTING ELEVATION TO REMAIN
  - 94.56 PROPOSED FINISHED ELEVATION
  - PROPOSED DRAINAGE DIRECTION
  - PROPOSED SWALE DRAINAGE DIRECTION
  - EXISTING OVERLAND FLOW DIRECTION
  - PROPOSED OVERLAND FLOW DIRECTION
  - PROPOSED SLOPE
  - TREE PROTECTION FENCE (GREEN PRINT CONSULTING, 2023)
  - PROPERTY LINE
  - SUBDIVISION LOT LINE

**BENCHMARK**  
 ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

**NOTE**  
 THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

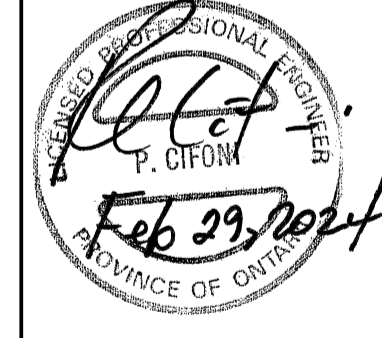
2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	13/02/24	MW/MW	ISSUED FOR COORDINATION
No	DD/MM/YY	By/DRN	REVISIONS

Design	MW	Chk'd	PC	Cad File	1819G.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24

Scale 0 5 10m  
 1:200

**APPROVALS**

Municipal	APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.	Date:	
Manager of Development Services			



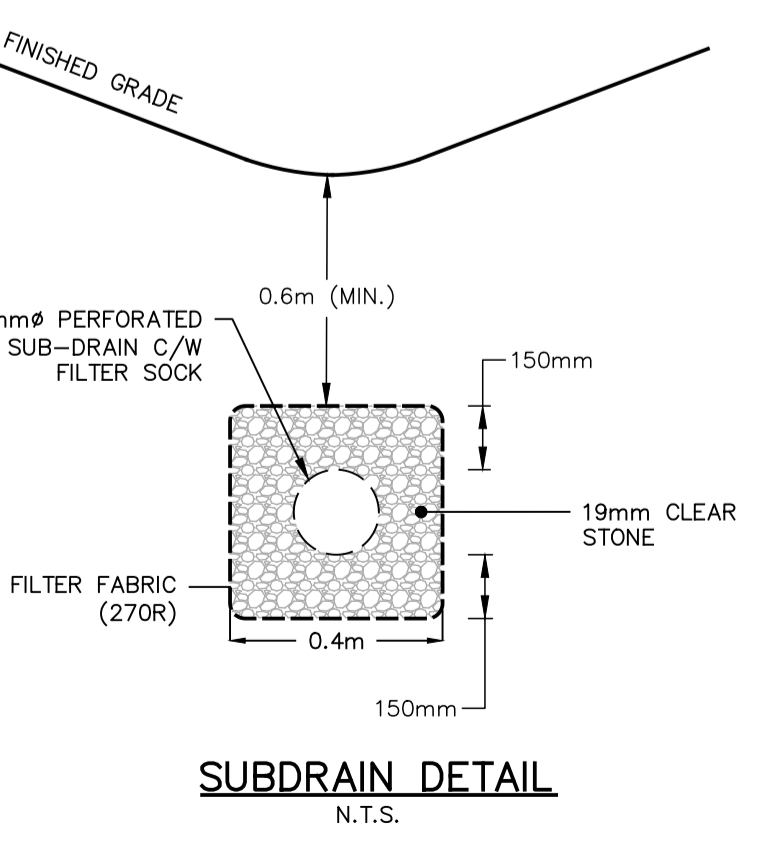
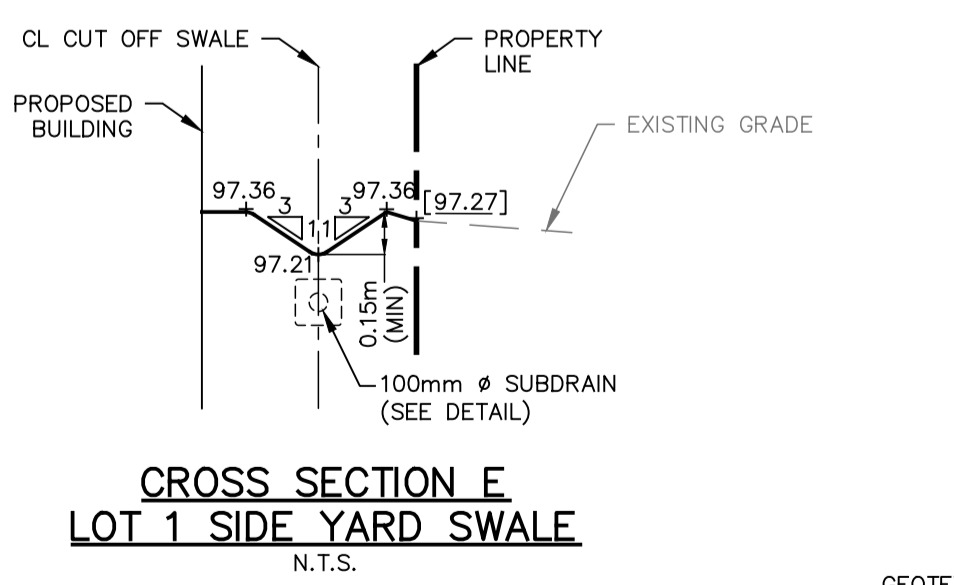
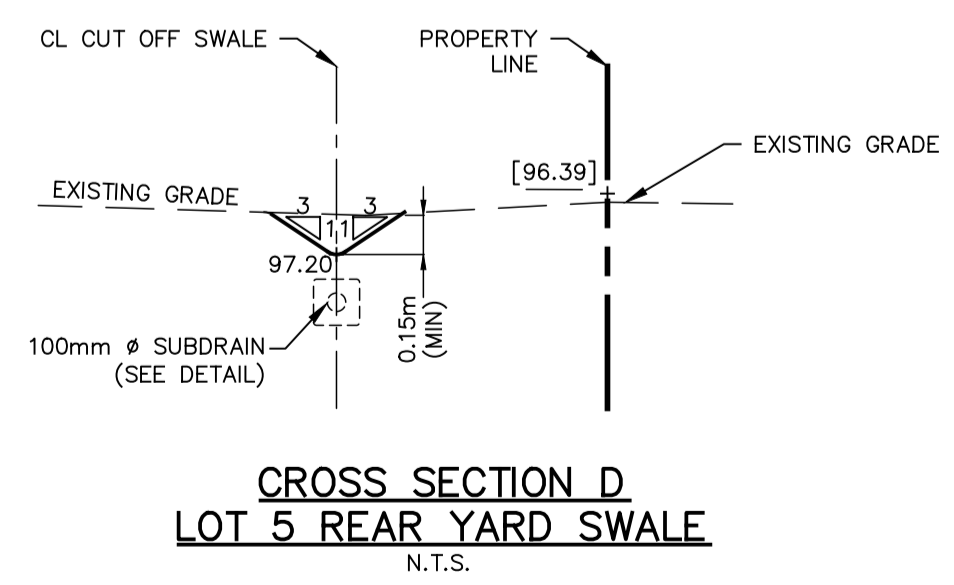
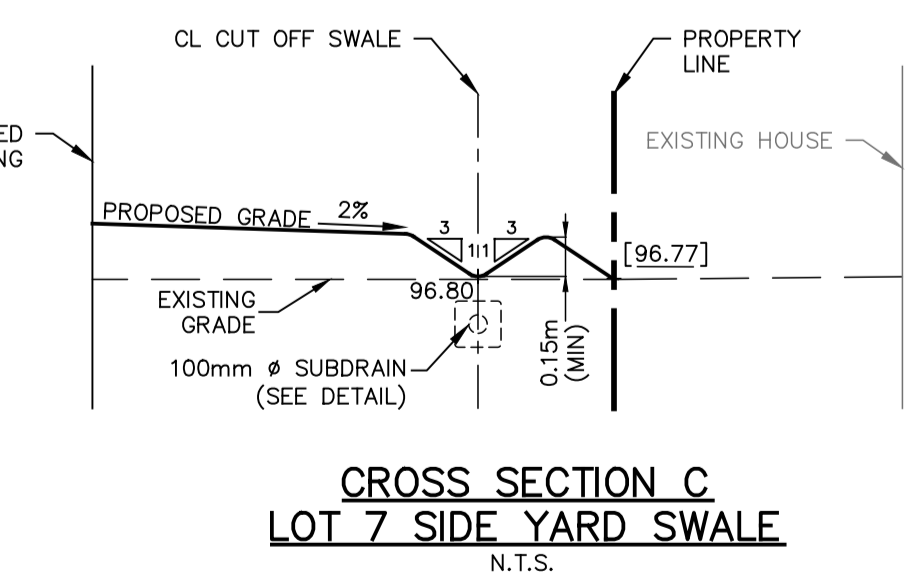
Consultant  
**TRAFALGAR ENGINEERING**  
 81-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
 www.trafalgareng.com

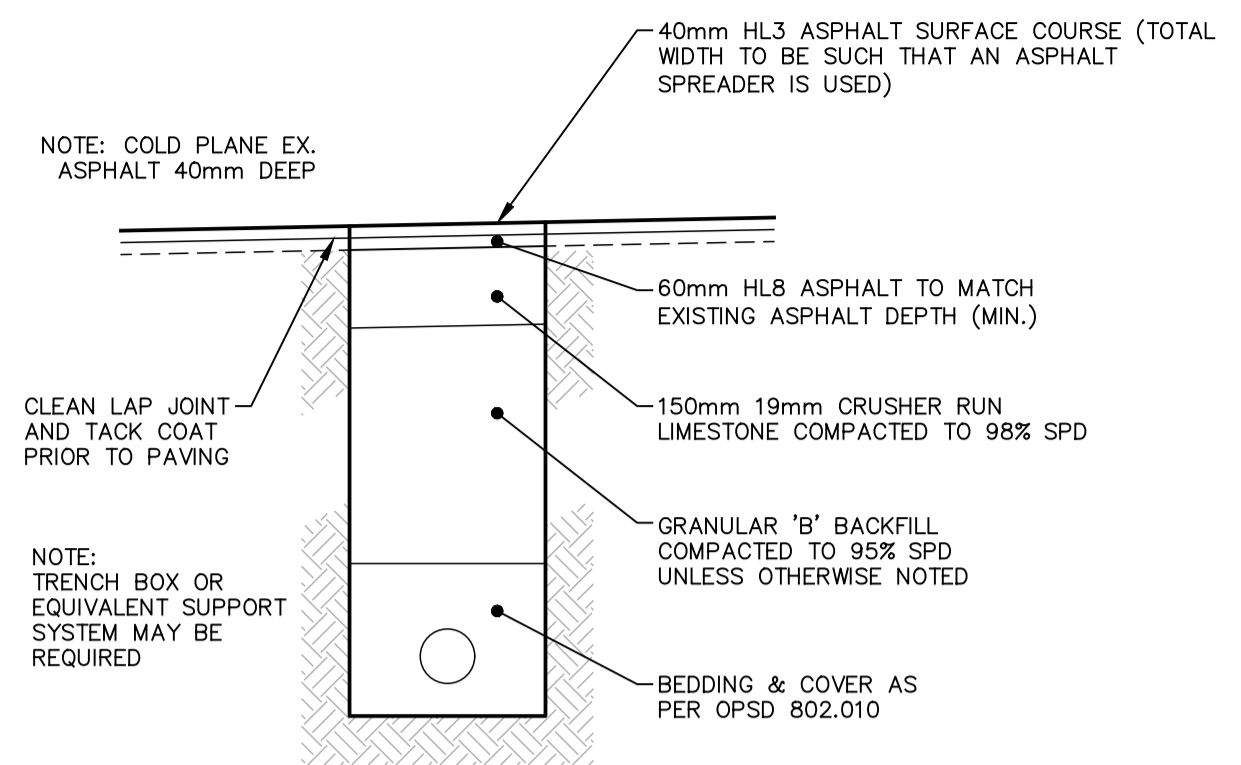
Municipality  
**OAKVILLE** **Halton REGION**

PROJECT  
**SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION**

DRAWING TITLE  
**GRADING PLAN**

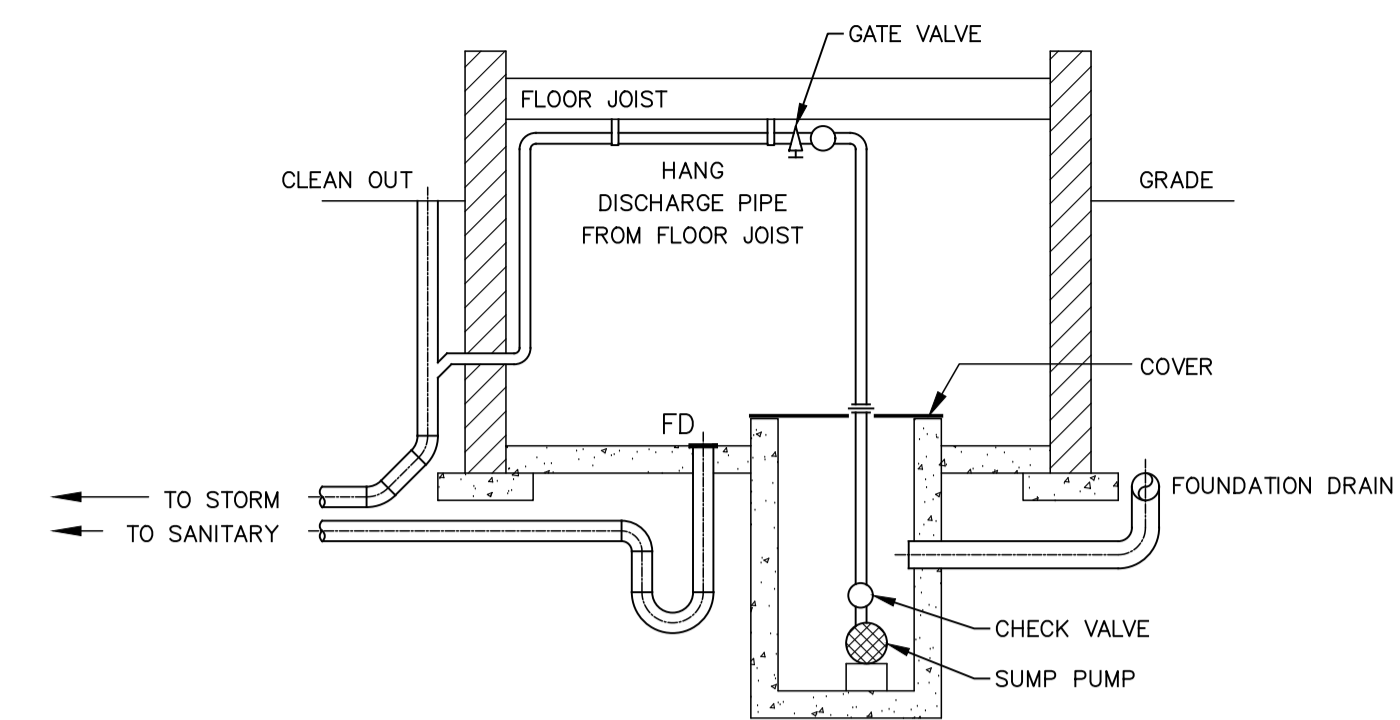
Municipal No.	24T-XXXX	Regional No.	
Contract No.	-	Consultant No.	1819
		Sheet	G1





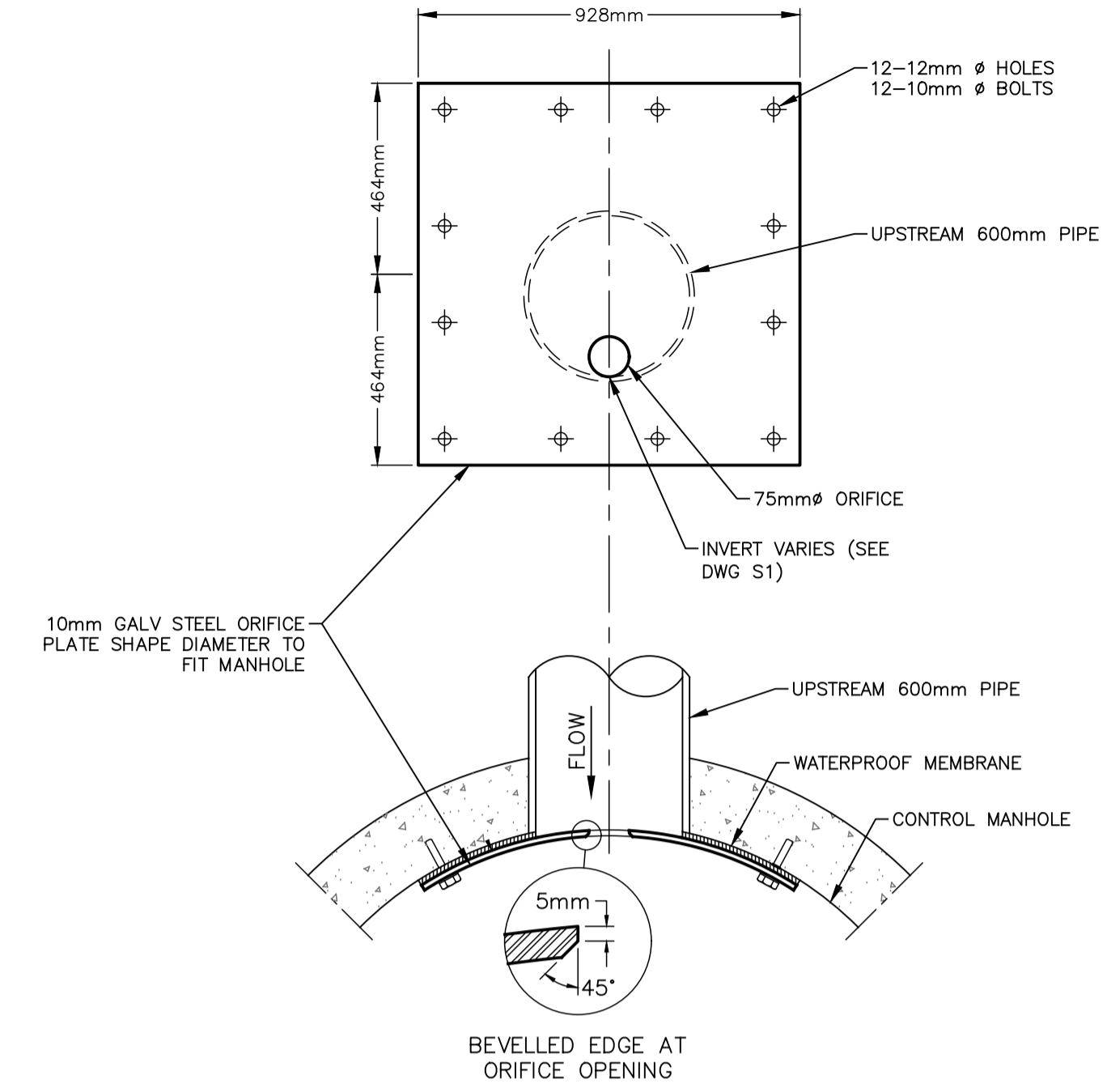
**NOTE:**  
 1. PLACE HL8 ASPHALT TO MATCH EX SURFACE.  
 2. IN FOLLOWING CONSTRUCTION SEASON GRIND ASPHALT 40mm DEEP AND PLACE 40mm HL3 ASPHALT

**TYPICAL TRENCH RESTORATION**  
 N.T.S.



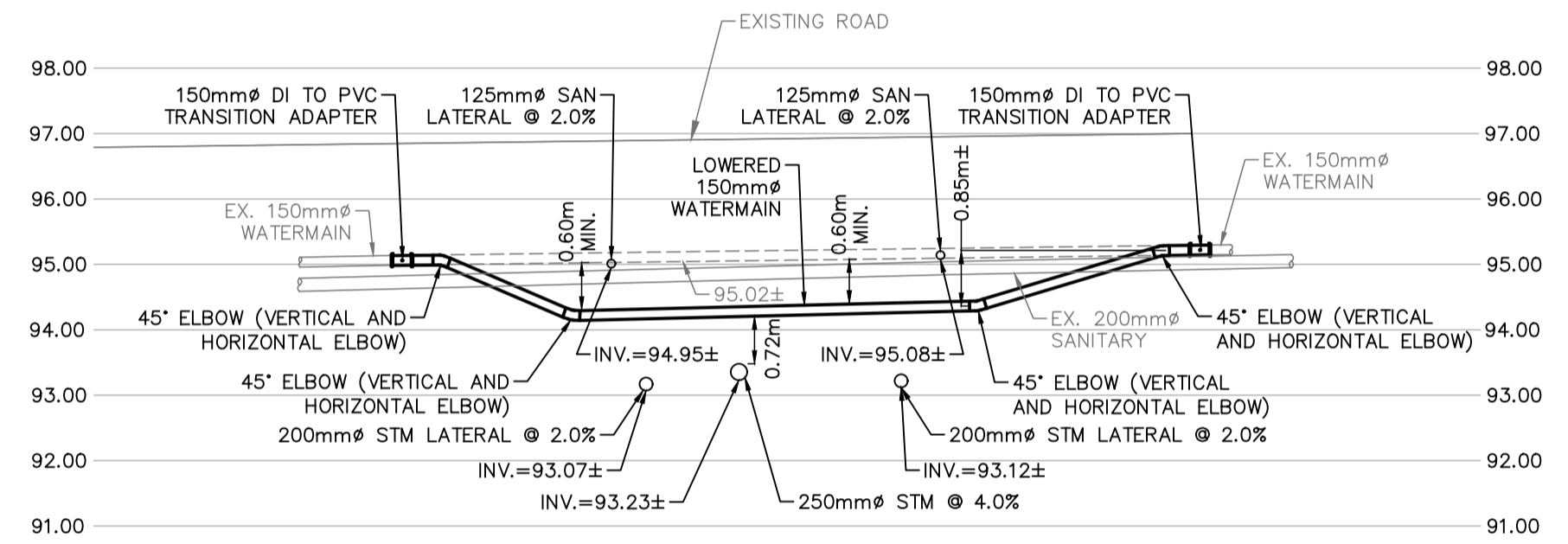
**NOTE:**  
 INTERNAL PLUMBING IS THE RESPONSIBILITY OF THE BUILDER AND SHALL BE SUBJECT TO REVIEW BY TOWN OF OAKVILLE AND SUBJECT TO A BUILDING PERMIT. DETAIL SHOWN HERE IS PROVIDED FOR ILLUSTRATION OF THE DESIGN INTENT ONLY INsofar AS TO PROTECT THE BASEMENT FROM STORM SEWER SURCHARGE.

**TYPICAL SUMP PUMP DETAIL**  
 N.T.S.

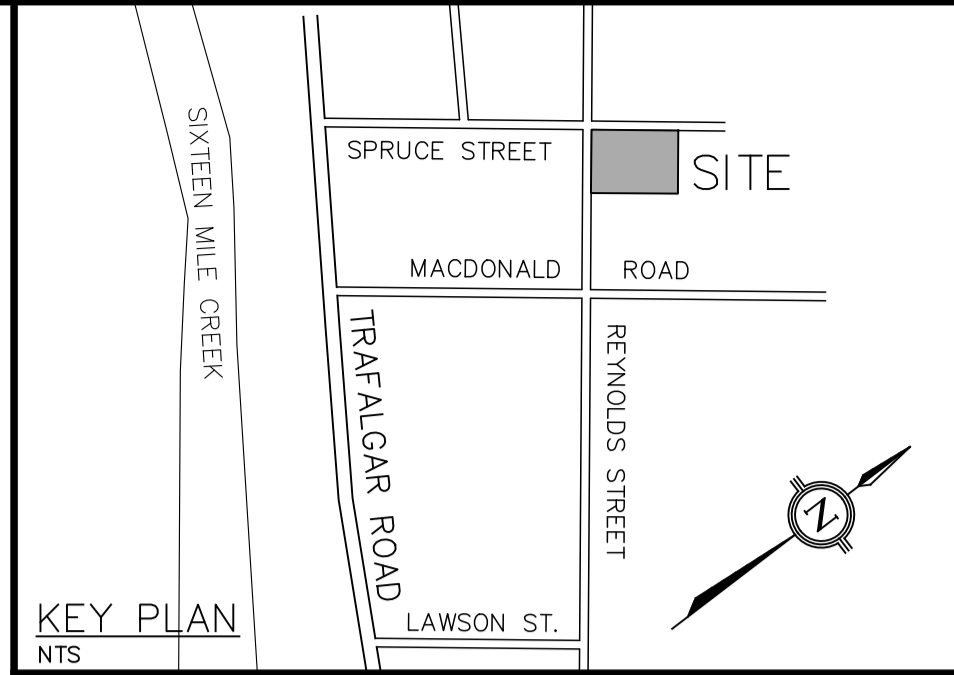


**NOTE:**  
 - ALL STEEL TO BE HOT DIPPED GALVANIZED AFTER  
 - FABRICATION ORIFICE PLATE TO BE WATERTIGHT  
 - PROVIDE 0.60m SUMP AT CONTROL MANHOLE

**CONTROL ORIFICE DETAIL**  
 N.T.S.



**WATERMAIN DEFLECTION DETAIL**  
 1:100



**KEY PLAN**  
 NTS

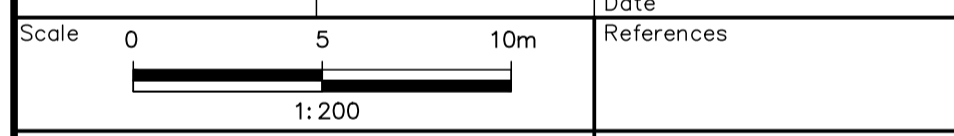
**LEGEND**

**BENCHMARK**  
 ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD.  
 ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

**NOTE**  
 THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01

No	DD/MM/YY	By/DRN	REVISIONS
2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	13/02/24	MW/MW	ISSUED FOR COORDINATION

Design	MW	Chkd	PC	Cad File	1819D.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24



**APPROVALS**

Municipal  
 APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.

Date: \_\_\_\_\_  
 Manager of Development Services

Regional Approval



DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

SIGNED: \_\_\_\_\_ DATE: \_\_\_\_\_  
 LEGISLATIVE AND PLANNING SERVICES DEPT.

Consultant

81-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
 www.trafalgareng.com

Municipality

**PROJECT**  
 SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION

**DRAWING TITLE**  
 SECTIONS AND DETAILS

Municipal No.	Regional No.
24T-XXXX	
Contract No.	Consultant No. 1819
-	Sheet D1

**GENERAL NOTES**

- ALL ROADS, STORM SEWERS AND OTHER MISCELLANEOUS ITEMS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE TOWN OF OAKVILLE REQUIREMENTS. SANITARY SEWERS AND WATERMAINS SHALL BE IN ACCORDANCE WITH THE REGION OF HALTON REQUIREMENTS. IN ABSENCE OF LOCAL STANDARDS, ONTARIO PROVINCIAL STANDARDS AND SPECIFICATIONS SHALL BE USED, AS MODIFIED BY THE LOCAL MUNICIPALITY. ALL MATERIALS SHALL MEET OR EXCEED ONTARIO PROVINCIAL STANDARDS AND TOWN STANDARD SPECIFICATIONS.
- ONTARIO PROVINCIAL STANDARD DRAWINGS (O.P.S.D.) ARE TO BE USED WHEN INDICATED (EXAMPLE: O.P.S.D. 600.04) TOWN OF OAKVILLE STANDARDS ARE USED FOR ROADS, STORM SEWERS AND MISCELLANEOUS WHEN INDICATED (EXAMPLE: 6-1). THE REGION OF HALTON STANDARDS ARE USED ON WATERMAINS AND SANITARY SEWERS AS INDICATED (EXAMPLE: RH 400.01).
- ALL INFORMATION SHOWN ON THE ENGINEERING DRAWINGS REGARDING THE SIZE AND LOCATION OF EXISTING UTILITIES AND/OR SERVICES HAS NOT BEEN VERIFIED IN THE FIELD. BEFORE STARTING WORK, THE CONTRACTOR IS RESPONSIBLE FOR VERIFICATION AND LOCATION OF SAID UTILITIES, PROTECTING AND MAINTAINING UTILITIES DURING CONSTRUCTION, AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.
- THE CONTRACTOR SHALL REPORT ALL DISCREPANCIES TO THE ENGINEER.
- MINIMUM 1.8m (6 FOOT) HEIGHT CONSTRUCTION FENCE SHALL BE ERECTED PRIOR TO ANY GRADING OR CONSTRUCTION AND SHALL REMAIN IN PLACE AND IN GOOD REPAIR THROUGHOUT THE CONSTRUCTION AND GRADING PHASE AND REMOVED ONLY AS DIRECTED BY THE ENGINEER.
- PRIOR TO THE PLACEMENT OF ANY FILL MATERIAL ALL TOPSOIL IS TO BE REMOVED AND SUBGRADE IS TO BE CERTIFIED BY THE SOILS ENGINEER.
- THE CONTRACTOR SHALL NOT DAMAGE TREES OUTSIDE AREAS INDICATED TO BE CLEARED AND GRUBBED.
- TRAFFIC DETOURS AND SIGNAGE TO BE APPROVED BY OAKVILLE TRAFFIC DEPARTMENT. MAINTAIN ONE LANE OPEN TO TRAFFIC AT ALL TIMES.
- TOWN OF OAKVILLE AND REGION OF HALTON STANDARD DRAWINGS, O.P.S.S. AND O.P.S.D. WITH REGIONAL AMENDMENTS FOR SANITARY SEWERS AND WATERMAINS SHALL CONSTITUTE PART OF THE ENGINEERING DESIGN AND CONSTRUCTION CONTRACT.
- ALL WATERMAIN AND SANITARY MAIN APPURTENANCES, MATERIALS AND COMPONENTS SHALL COMPLY WITH THE REGION'S APPROVED MANUFACTURER'S PRODUCT LIST FOR WATER SYSTEMS AND SANITARY SYSTEMS. ALTERNATIVE MATERIALS MAY BE ACCEPTABLE, PROVIDED APPROVAL HAS FIRST BEEN OBTAINED FROM THE CITY/TOWN ENGINEER AND/OR THE REGIONAL COMMISSIONER OF PUBLIC WORKS.
- NO BLASTING IS PERMITTED.
- MANHOLE AND VALVE CHAMBER COVERS ARE TO BE SET FLUSH WITH BASE COURSE ASPHALT AND ADJUSTED TO FINAL GRADE PRIOR TO INSTALLING TOP LIFT OF ASPHALT.
- ALL TRENCHES WITHIN EXISTING RIGHT-OF-WAY ARE TO BE BACKFILLED IN ACCORDANCE WITH TOWN OF OAKVILLE REQUIREMENTS.
- ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE IN PLACE PRIOR TO COMMENCING ANY CONSTRUCTION.
- ALL OVERLY MOIST, SOFT OR OTHERWISE UNSUITABLE SOIL MUST BE REMOVED DOWN TO FIRM NATIVE SUBSOIL. THE BASE SHOULD BE PROOF-ROLLED AND COMPACTED TO A FIRM STABLE STATE WHICH IS TO BE APPROVED BY THE GEOTECHNICAL ENGINEER BEFORE THE START OF FILL PLACEMENT.
- FILL PLACEMENT MUST BE CARRIED OUT IN A CONTROLLED SYSTEMATIC PROGRESSION WHICH ALLOWS FOR HARMONIOUS AND UNIFORM COVERAGE BY THE COMPACTION EQUIPMENT.
- THE MAXIMUM ALLOWABLE LIFT THICKNESS IS 150mm. THE REQUIRED COMPACTION IS MINIMUM 98% STANDARD PROCTOR MAX. DRY DENSITY.

**WATERMAINS**

- WATERMAINS 150MM TO 300MM DIAMETER TO BE P.V.C. CL235 (DR-18) AS PER AWWA C900 (CSA B137.3) WITH GASKETED JOINTS.
- WATER SERVICE CONNECTIONS TO BE AS PER O.P.S.D. 1104.01. AS AMENDED BY REGION OF HALTON PIPE FOR ALL SERVICE CONNECTIONS UP TO 50MM DIA. SHALL BE TYPE "K" SOFT COPPER TUBING MEETING AWWA C800 (LATEST EDITION).
- A MIN. HORIZONTAL SEPARATION OF 2.5M MUST BE MAINTAINED BETWEEN WATERMAINS AND SANITARY OR STORM SEWERS, INCLUDING SERVICE LATERALS.
- A MIN. VERTICAL SEPARATION OF 0.15M BETWEEN WATERMAINS AND SEWERS MUST BE MAINTAINED IF WATERMAIN CROSSES ABOVE SEWER OR 0.50m IF WATERMAIN CROSSES SEWER.
- WATERMAIN BEDDING AND COVER TO BE SUITABLE GRANULAR "A" BEDDING MATERIAL AS PER O.P.S.D. 802.010 AND O.P.S.S. 401.
- ALL HYDRANTS AS PER O.P.S.D. 1105.01 TO HAVE STEAMER CONNECTIONS. HYDRANTS TO BE SUPPLIED WITH:
  - TWO (2) 63.5MM (2 1/2") WITH CSA STANDARD THREAD, 63.5MM I.D., 79.4 O.D., 5 THREADS PER 25MM, 31.75MM SQUARE OPERATING NUT; AND
  - ONE (1) 100MM (4") STORZ PUMPER CONNECTION AS PER CAN/ULC #5-520, 31.75MM SQUARE OPERATING NUT, AND STORZ CAP PAINTED GLOSS BLACK.
  - SECONDARY VALVE AND ANCHOR TEE.
- HYDRANTS SHALL BE INSTALLED SUCH THAT THE ROD STEM LENGTH SHALL NOT EXCEED 1.7M MEASURED FROM THE BREAK-OFF FLANGE. IF HYDRANT BARREL LENGTH EXCEEDS 1.7M THEN A HYDRANT THAT CAN BE RAISED FROM THE BOTTOM WITHOUT INCREASING ROD LENGTH IS TO BE USED.
- ALL METALLIC WATERMAINS, FITTINGS, AND APPURTENANCES SHALL BE INSTALLED WITH A MINIMUM OF ONE ANODE PER LENGTH PER PIPE AND ONE ANODE PER ELECTRONICALLY ISOLATED APPURTENANCE AND INSTALLED IN ACCORDANCE WITH OPSS 442 AND OPSD 1109.010 AND 1109.011. ANODE INSTALLATION IS NOT REQUIRED WITHIN VALVE CHAMBERS, DRAIN CHAMBERS, AIR RELEASE CHAMBERS OR SWAB PORTS.
- ALL SACRIFICIAL ANODES SHALL CONFORM TO A.S.T.M. B-418 TYPE II AND SHALL BE MADE OF HIGH GRADE ELECTROLYTIC ZINC, 99.99% PURE, AS PER HALTON LINEAR DESIGN MANUAL, WATER SERVICE CONNECTIONS - 2.10.4.B.II
- ALL WELD CONNECTIONS TO BE COATED WITH "TC MASTIC" OR APPROVED EQUIVALENT.
- FOR ALL ANODES CONNECTED TO NEW PIPE, FITTINGS OR TO EXISTING METALLIC WATERMAINS, A CADWELDER AND CA-15 OR EQUIVALENT CARTRIDGE SHALL BE USED. ANODE INSTALLATION SHALL BE PERFORMED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS.
- WHERE NEW PIPE IS METALLIC OR OTHERWISE TO BE CONNECTED TO EXISTING DUCTILE IRON OR CAST IRON PIPE A 14.5KG MAGNESIUM ANODE IS TO BE CONNECTED TO THE FIRST LENGTH OF EXISTING PIPE, AS PER OPSS 442 AND OPSD 1109.010 AND 1109.011
- ALL VALVES TO OPEN LEFT (COUNTER-CLOCKWISE), BE OF THE APPROVED TYPE WITH NON-RISING STEM AND SHALL HAVE 50MM SQUARE STANDARD AWWA OPERATING NUT.
- ALL PLUGS, CAPS, TEES, BENDS, AND OTHER APPURTENANCES SHALL BE MECHANICALLY RESTRAINED AS PER MANUFACTURER'S SPECIFICATIONS. MECHANICAL THRUST RESTRAINT DEVICES SHALL HAVE THIRD PARTY TESTING, APPROVALS FROM THE UNDERWRITERS LABORATORY (UL) AND FACTORY MUTUAL (FM), AND BE INCLUDED IN HALTON REGION'S APPROVED MANUFACTURER'S PRODUCT LIST FOR WATER SYSTEMS.

**WATERMAINS Cont'd**

- WHERE WATERMAIN IS PLACED IN FILL OR IN PREVIOUSLY DISTURBED GROUND, ALL JOINTS TO BE MECHANICALLY RESTRAINED.
- MINIMUM DEPTH OF COVER OVER WATERMAIN SHALL BE 1.70M MEASURED FROM THE TOP OF THE PIPE TO THE FINISHED GRADE.
- THE DEPTH OF WATER SERVICES AT PROPERTY LINE SHOULD BE A MINIMUM OF 1.7M AND A MAXIMUM OF 2.0M. THE DISTANCE BETWEEN THE GROUND ELEVATION AND THE TOP OF THE ROD SHOULD BE BETWEEN 0.5M AND 1.0M.
- WATER SERVICES CROSSING THE STORM SEWER TO HAVE MIN. 1.70M OF COVER. WHERE THIS CANNOT BE ACHIEVED, WATER SERVICE IS TO CROSS UNDER SEWER.
- GATE VALVES CONFORMING TO A W.W.A. C509 OR C515 ARE REQUIRED ON WATERMAINS 300MM AND UNDER. LINE GATE VALVES SHALL HAVE SOREW TYPE VALVE BOXES.
- ALL WATERMAIN FITTINGS SHALL HAVE MECHANICAL JOINTS. VALVES IN CHAMBERS TO BE FLANGED.
- PIPE BARREL BENDING/DEFLECTION SHALL NOT BE ALLOWED. PIPE JOINT DEFLECTIONS ARE DISCOURAGED (UTILIZE STANDARD BENDS TO ACHIEVE DESIRED VERTICAL AND HORIZONTAL PIPE ALIGNMENT). HOWEVER, IF ABSOLUTELY NECESSARY THE MAXIMUM ALLOWABLE PIPE JOINT DEFLECTION SHALL BE 50% OF THE MANUFACTURER'S SPECIFICATIONS.
- TRACER WIRE IS TO BE INSTALLED ON ALL NEW INSTALLATIONS OF PVC WATERMAIN PIPE FOR LOCATING PURPOSES. A SOLID 10 GAUGE T.W.U. COPPER WIRE IS TO BE INSTALLED ALONG THE TOP OF THE PIPE, STRAPPED TO THE PIPE AT 6M INTERVALS.
- THE INSPECTOR MAY TEST THE TRACING WIRE FOR CONDUCTIVITY. THE TRACER WIRE SHALL BE INSTALLED BETWEEN EACH VALVE AND/OR THE END OF THE NEW WATERMAIN TO ENSURE A CONTINUOUS SIGNAL FOR LOCATING THE MAIN JOINTS IN THE TRACER WIRE BETWEEN VALVES IS DISCOURAGED, BUT WHEN NECESSARY, MUST BE WATER-PROOFED (REFER TO O.P.S.D. 1109.025) AND DONE IN SUCH A WAY TO ENSURE ELECTRICAL CONDUCTIVITY. AT EACH VALVE, A LOOP OF WIRE IS TO BE BROUGHT UP OUTSIDE THE VALVE BOX AS PER HALTON STANDARD DRAWING RH 406.010. TRACER WIRE FOR HORIZONTAL DIRECTIONAL DRILLING AND PIPE BURSTING INSTALLATION SHALL BE IN ACCORDANCE WITH HALTON REGION'S AMENDMENTS TO O.P.S.S. IF THE TRACING WIRE IS NOT CONTINUOUS FROM VALVE TO VALVE, THE CONTRACTOR SHALL, AT HIS OWN EXPENSE, REPLACE OR REPAIR THE WIRE.
- ALL WATER CUSTOMERS SUPPLIED BY A WATERMAIN TO BE SHUT DOWN SHALL BE NOTIFIED BY THE CONTRACTOR AT LEAST 48 HOURS IN ADVANCE OF THE SHUT DOWN AS PER REGION OF HALTON SPECIFICATIONS. NOTIFICATION SHALL TAKE PLACE UNDER THE ENGINEER'S DIRECTION.
- OPERATING OF EXISTING WATERMAINS SHALL BE BY REGION OF HALTON STAFF ONLY.

**STORM SEWERS**

- ALL STORM SEWERS 450mm DIA. OR SMALLER SHALL BE RIBBED PVC PIPE IN ACCORDANCE WITH CSA B182.4. SDR35 WITH LOCK IN RUBBER SEAL RING BEDDING SHALL BE O.P.S.D. 802.010. BEDDING MATERIAL SHALL BE CRUSHED STONE BASE (HL-6) GRAVEL AGGREGATE) AND A GRANULAR "C" COVER MATERIAL.
- ALL STORM SEWERS LARGER THAN 450mm DIAMETER SHALL BE REINFORCED CONCRETE PIPE (CLASS AS SHOWN) IN ACCORDANCE WITH CSA A257.2. BEDDING SHALL BE O.P.S.D. 802.030. BEDDING MATERIAL SHALL BE CRUSHED STONE BASE (HL-6 GRAVEL AGGREGATE) AND A GRANULAR "C" COVER MATERIAL.
- CONTRACTOR IS RESPONSIBLE FOR SUPPLYING ADDITIONAL BEDDING AND/OR STRONGER PIPE IF ACTUAL TRENCH WIDTHS EXCEED DESIGN WIDTHS.
- MANHOLE SIZES AS SHOWN.
- SURROUND ALL MANHOLES WITH A MINIMUM OF 1.0m COMPACTED GRANULAR "C" BACKFILL. ALL CATCHBASINS TO HAVE COMPLETE, COMPACTED GRANULAR "C" BACKFILL SURROUND.
- CATCHBASIN (CB) PER O.P.S.D. 705.010 C/W 250mm DIA. LEAD. DOUBLE CATCHBASINS (DCB) PER O.P.S.D. 705.020 C/W 300mm DIA. LEAD. CATCHBASINS TO BE FITTED WITH INLET CONTROL DEVICE AS SHOWN. REAR LOT CATCHBASINS TO BE SUMPLESS PER TOWN STD 3-1 C/W BEEHIVE GRATE PER TOWN STD 5-2.
- FOR COMMON TRENCH DETAILS REFER TO REGION STD. RH 302.01.
- DROP STRUCTURES TO BE TOWN OF OAKVILLE STD. 2-2.
- BENCHING IN MANHOLES IS TO EXTEND UP TO THE SPRINGLINE OF THE PIPE.
- DITCH INLETS TO BE AS PER O.P.S.D. 705.030 3:1 GRADE.
- CATCHBASIN FRAME AND GRATES FOR ROADS TO BE AS PER O.P.S.D. 400.11.
- SERVICE CONNECTION AT THE STREET LINE IS TO BE HIGHER THAN THE SANITARY CONNECTION AT THAT POINT.
- ALL ENDS OF SERVICE CONNECTIONS SHALL BE MARKED WITH 100x50 LUMBER MARKERS PLACED FROM THE INVERT OF THE SERVICE TO 1.0m ABOVE GROUND LEVEL AND PAINTED WHITE.
- SAFETY GRATINGS SHALL BE PROVIDED IN ALL MANHOLES WHEN THE DEPTH OF THE MANHOLE EXCEEDS 5.3m. TOWN STD. 2-1 (2003)
- STORM SERVICE LATERALS TO BE 200mm DIA FOR SINGLE FAMILY DWELLINGS. LATERALS TO BE MINIMUM 2.00% GRADE. PVC PIPES TO BE WHITE IN COLOUR AND DR28 SHALL BE USED.

**SANITARY SEWERS**

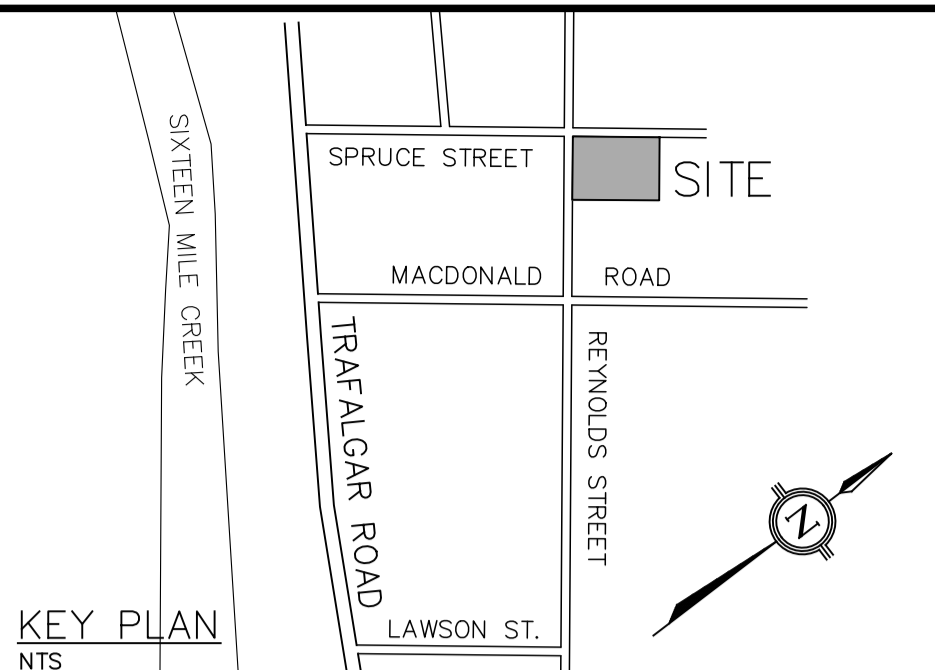
- SANITARY MANHOLES AS PER O.P.S.D. 701.010 WITH FRAMES AND COVERS AS PER O.P.S.D. 401.010 TYPE "A" (AS AMENDED RESPECTIVELY BY THE REGION OF HALTON) UNLESS OTHERWISE NOTED ON THE DRAWINGS.
- BENCHING IN MANHOLES TO BE AS PER O.P.S.D. 701.021 AS AMENDED BY THE REGION OF HALTON. BENCHING IN SANITARY MANHOLES TO BE TO THE OVERT OF THE PIPE.
- SANITARY SEWER PIPE SHALL BE PVC SDR35 (GREEN IN COLOUR) CONFORMING TO CSA B182.2 UNLESS OTHERWISE NOTED.
- SANITARY SERVICE CONNECTIONS TO BE 125mm DIA. FOR SINGLE FAMILY DWELLINGS AND ROWED TOWNHOUSES, COMMERCIAL, INDUSTRIAL, AND INSTITUTIONAL LATERALS SHALL BE A MINIMUM OF 150mm DIAMETER. SANITARY SERVICE CONNECTIONS TO BE MINIMUM 2% GRADE AND SHALL BE NON-WHITE IN COLOUR. FOR PVC LATERAL CONNECTIONS, PIPE SHALL BE GREEN IN COLOUR AND DR28 SHALL BE USED.
- SERVICES TO BE MIN. 2.15M AND MAX. 2.75M DEEP AT PROPERTY LINE. RISERS SHALL BE USED WHERE NOTED AS PER O.P.S.D. 1006.010.
- GRANULAR "A" BEDDING AND COVER ON ALL SEWERS AND CONNECTIONS TO BE AS PER O.P.S.D. 802.010 UNLESS NOTED OTHERWISE, WITH GRANULAR "B" BACKFILL.
- GRANULAR BACKFILL AROUND MANHOLES SHALL BE COMPACTED BY MECHANICAL MEANS TO A MINIMUM OF 95% S.P.D.

**ROADS**

- ALL ROAD BASE AND SUB-BASE MATERIALS SHALL BE CRUSHER RUN LIMESTONE MEETING OPSS TYPE II SPECIFICATIONS.
- ANY AREAS WITHIN R.O.W. WHICH REQUIRE FILL IN EXCESS OF 0.30m ARE SUBJECT TO COMPACTION TESTS AND SUCH TESTS MUST SHOW A MIN. COMPACTION OF 98% S.P.M.D.D. AT ALL DEPTHS. ALL EARTHWORKS MUST COMPLY WITH GEOTECHNICAL INVESTIGATION.
- GRANULAR BASE SHALL BE COMPACTED TO A MIN. OF 100% SPMDI IN LIFTS OF 150mm OR LESS.
- ASPHALT MATERIALS SHALL BE ROLLED AND COMPACTED TO A MIN. OF 97% MARSHALL BULK DENSITY.
- PRIOR TO PLACEMENT OF GRANULAR COURSES, THE SUBGRADE SHALL BE PROOF-ROLLED AND ALL LOOSE, SOFT OR UNSTABLE AREAS REMOVED AS DIRECTED BY THE ENGINEER.
- ALL CURB AND GUTTERS SHALL BE PER OPSD 600.040 UNLESS OTHERWISE NOTED.
- PERFORATED SUBDRAINS C/W FILTER SOCK PER TOWN STD. 7-60, SHALL BE INSTALLED UNDER ALL CURBS.
- SIDEWALK TO BE TOWN STD. 6-3 TYPE 'A'.
- AN EXTRA 150mm THICKNESS GRANULAR "B" SHALL BE ADDED AT ARTERIAL AND INDUSTRIAL ROAD INTERSECTIONS. THIS EXTRA DEPTH SHALL BE EXTENDED FOR A MINIMUM OF 15.0m FROM THE PROPERTY LINE OF THE INTERSECTING STREET.
- TOP COURSE ASPHALTIC CONCRETE SHALL BE PLACED ONLY AFTER ADJACENT BUILDINGS (HOMES, INDUSTRIAL, COMMERCIAL, ETC.) HAVE BEEN CONSTRUCTED AND ONLY WITH THE CONSENT OF THE DIRECTOR OF ENGINEERING AND CONSTRUCTION.
- SIDEWALK RAMPS AT INTERSECTIONS AND MID-BLOCK CROSSINGS SHALL CONFORM TO OPSD 310.030 WITH THE REQUIREMENT THAT THE RAMP GRADIENT SHALL NOT EXCEED 5%.
- PAVEMENT STRUCTURE (TO BE CONFIRMED BY GEOTECHNICAL CONSULTANT):
  - 40mm HL3
  - 50mm HL8
  - 150mm - 19mm CRL
  - 350mm - 50mm CRL

**CONSTRUCTION**

- CONTRACTOR IS RESPONSIBLE FOR ALL TEMPORARY TRAFFIC CONTROLS, PER MTO BOOK 7.
- CONTRACTOR IS RESPONSIBLE FOR ALL CONSTRUCTION LAYOUT, WITH CONTROL BARS PROVIDED BY THE OWNER. PROTECTION OF CONTROL BARS IS THE RESPONSIBILITY OF THE CONTRACTOR.
- CONTRACTOR IS RESPONSIBLE TO VERIFY THE SIZE AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION, INCLUDING VAC TRUCK AND RESTORATION AS REQUIRED.
- CONTRACTOR SHALL PROVIDE THIRD-PARTY DIGITAL AS-BUILTS IN CAD TO INCLUDE ALL NEW SITE SERVICES INCLUDING TOPS AND INVERTS, AND FINISHED GRADES, INCLUDING PAVED AREAS, SWALES, CURBS, SIDEWALKS AND AND RETAINING WALLS, TO THE SATISFACTION OF THE ENGINEER.
- CONTRACTOR SHALL FLUSH AND VIDEO ALL EXISTING SEWERS PRIOR TO AND AFTER CONNECTION, AND NEW AND DISTURBED SEWERS UPON INSTALLATION AND LATER UPON COMPLETION OF TOP WORKS AND LANDSCAPING, PER OPSS 409. VIDEOS TO BE PROVIDED TO THE ENGINEER FOR REVIEW AND APPROVAL.



**LEGEND**

NTS

**BENCHMARK**

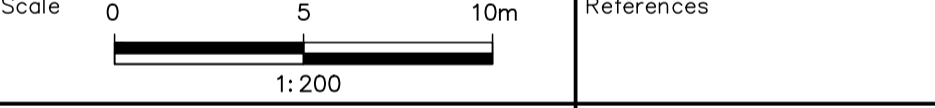
ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

**NOTE**

THE SURVEY WAS COMPLETED ON THE 20TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 23-005 CAD FILE No.23-005TP01


2	29/02/24	MW/GL	ISSUED FOR ZBA/DPS
1	13/02/24	MW/MW	ISSUED FOR COORDINATION

No	DD/MM/YY	By/DRN	REVISIONS		
Design	MW	Chk'd	PC	Cad File	1819N.dwg
Drawn	MW	Chk'd		Plot Date	02/29/24



APPROVALS		Field Notes
Municipal	APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVILLE STANDARDS AND SPECIFICATIONS.	Bell <input type="checkbox"/> Hydro <input type="checkbox"/>
	Date: _____	Gas <input type="checkbox"/> Cable <input type="checkbox"/>
	Manager of Development Services	Traf. <input type="checkbox"/> Water <input type="checkbox"/>

DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

REGIONAL PROFESSIONAL ENGINEER  
P. CIFON  
Feb 29, 2024  
PROVINCE OF ONTARIO

CONSULTANT  
**TRAFALGAR ENGINEERING**  
81-481 MORDEN ROAD, OAKVILLE, ON, L6K 3W6  
www.trafalgareng.com



PROJECT  
**SPRUCE ROSE INC. RESIDENTIAL SUBDIVISION**

DRAWING TITLE  
**STANDARD NOTES**

Municipal No.	24T-XXXX	Regional No.	
Contract No.	-	Consultant No.	1819
		Sheet	N1

## **APPENDIX 'E'**

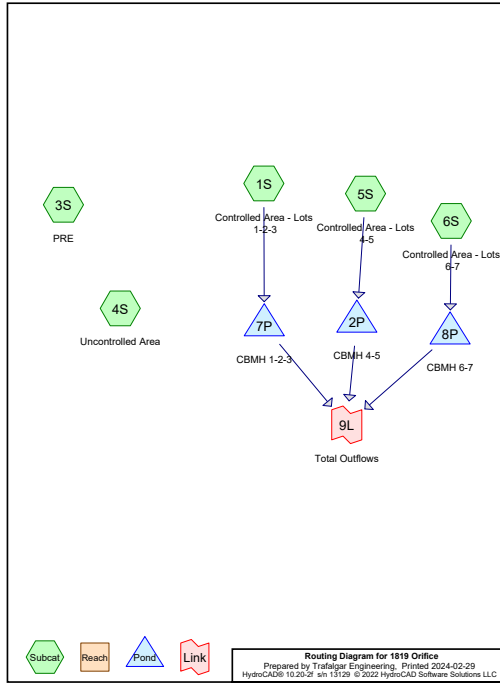
HydroCAD Model Output

**Project Notes**

Copied 6 events from ON Oakville 24hr storm

**Rainfall Events Listing (selected events)**

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (mm)	AMC
1	5-Year	ON Oakville 24hr	5-Year	Default	24.00	1	60	2
2	10-Year	ON Oakville 24hr	10-Year	Default	24.00	1	70	2
3	25-Year	ON Oakville 24hr	25-Year	Default	24.00	1	82	2
4	50-Year	ON Oakville 24hr	50-Year	Default	24.00	1	89	2
5	100-Year	ON Oakville 24hr	100-Year	Default	24.00	1	97	2



**Area Listing (all nodes)**

Area (sq-meters)	CN	Description (subcatchment-numbers)
4,693.0	80	>75% Grass cover, Good, HSG D (1S, 3S, 4S, 5S, 6S)
2,580.0	98	Paved parking, HSG A (1S, 3S, 5S)
393.0	98	Paved parking, HSG D (6S)
507.0	98	Water Surface, HSG A (4S)
<b>8,173.0</b>	<b>88</b>	<b>TOTAL AREA</b>

**Soil Listing (all nodes)**

Area (sq-meters)	Soil Group	Subcatchment Numbers
3,087.0	HSG A	1S, 3S, 4S, 5S
0.0	HSG B	
0.0	HSG C	
5,086.0	HSG D	1S, 3S, 4S, 5S, 6S
0.0	Other	
<b>8,173.0</b>		<b>TOTAL AREA</b>

**Ground Covers (all nodes)**

HSG-A (sq-meters)	HSG-B (sq-meters)	HSG-C (sq-meters)	HSG-D (sq-meters)	Other (sq-meters)	Total (sq-meters)	Ground Cover
0.0	0.0	0.0	4,693.0	0.0	4,693.0	>75% Grass cover, Good
2,580.0	0.0	0.0	393.0	0.0	2,973.0	Paved parking
507.0	0.0	0.0	0.0	0.0	507.0	Water Surface
<b>3,087.0</b>	<b>0.0</b>	<b>0.0</b>	<b>5,086.0</b>	<b>0.0</b>	<b>8,173.0</b>	<b>TOTAL AREA</b>

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

**Subcatchment 1S: Controlled Area -** Runoff Area=1,039.0 m<sup>2</sup> 53.13% Impervious Runoff Depth>35 mm  
 Tc=20.6 min CN=90 Runoff=0.014 m<sup>3</sup>/s 36.1 m<sup>3</sup>

**Subcatchment 3S: PRE** Runoff Area=4,116.0 m<sup>2</sup> 41.81% Impervious Runoff Depth>31 mm  
 Tc=10.0 min CN=88 Runoff=0.075 m<sup>3</sup>/s 128.4 m<sup>3</sup>

**Subcatchment 4S: Uncontrolled Area** Runoff Area=1,114.0 m<sup>2</sup> 45.51% Impervious Runoff Depth>31 mm  
 Tc=10.0 min CN=88 Runoff=0.020 m<sup>3</sup>/s 34.7 m<sup>3</sup>

**Subcatchment 5S: Controlled Area - Lots** Runoff Area=867.0 m<sup>2</sup> 35.41% Impervious Runoff Depth>28 mm  
 Tc=16.0 min CN=86 Runoff=0.011 m<sup>3</sup>/s 24.1 m<sup>3</sup>

**Subcatchment 6S: Controlled Area -** Runoff Area=1,037.0 m<sup>2</sup> 37.90% Impervious Runoff Depth>29 mm  
 Tc=16.0 min CN=87 Runoff=0.014 m<sup>3</sup>/s 30.5 m<sup>3</sup>

**Pond 2P: CBMH 4-5** Peak Elev=95.297 m Storage=2.9 m<sup>3</sup> Inflow=0.011 m<sup>3</sup>/s 24.1 m<sup>3</sup>  
 Outflow=0.008 m<sup>3</sup>/s 24.1 m<sup>3</sup>

**Pond 7P: CBMH 1-2-3** Peak Elev=95.580 m Storage=4.1 m<sup>3</sup> Inflow=0.014 m<sup>3</sup>/s 36.1 m<sup>3</sup>  
 Outflow=0.011 m<sup>3</sup>/s 36.1 m<sup>3</sup>

**Pond 8P: CBMH 6-7** Peak Elev=95.156 m Storage=4.4 m<sup>3</sup> Inflow=0.014 m<sup>3</sup>/s 30.5 m<sup>3</sup>  
 Outflow=0.010 m<sup>3</sup>/s 30.5 m<sup>3</sup>

**Link 9L: Total Outflows** above 10,000 m<sup>3</sup>/s Inflow=0.029 m<sup>3</sup>/s 90.7 m<sup>3</sup>  
 Primary=0.000 m<sup>3</sup>/s 0.0 m<sup>3</sup> Secondary=0.029 m<sup>3</sup>/s 90.7 m<sup>3</sup>

**Total Runoff Area = 8,173.0 m<sup>2</sup> Runoff Volume = 253.9 m<sup>3</sup> Average Runoff Depth = 31 mm**  
**57.42% Pervious = 4,693.0 m<sup>2</sup> 42.58% Impervious = 3,480.0 m<sup>2</sup>**

**Summary for Subcatchment 1S: Controlled Area - Lots 1-2-3**

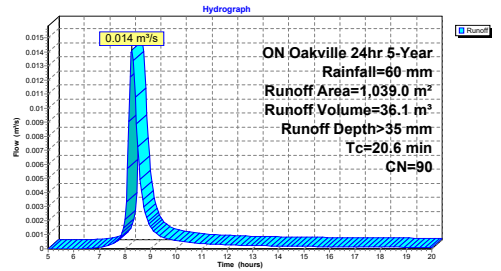
Runoff = 0.014 m<sup>3</sup>/s @ 8.28 hrs, Volume= 36.1 m<sup>3</sup>, Depth> 35 mm  
 Routed to Pond 7P : CBMH 1-2-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 5-Year Rainfall=60 mm

Area (m <sup>2</sup> )	CN	Description
552.0	98	Paved parking, HSG A
487.0	80	>75% Grass cover, Good, HSG D
1,039.0	90	Weighted Average
487.0		46.87% Pervious Area
552.0		53.13% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
20.6					Direct Entry,

**Subcatchment 1S: Controlled Area - Lots 1-2-3**



**Summary for Subcatchment 3S: PRE**

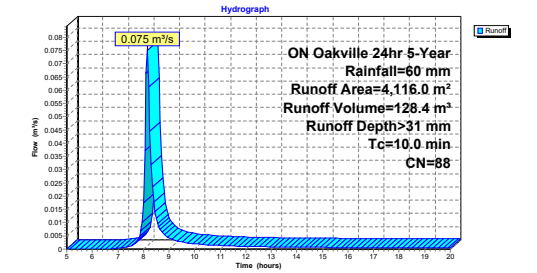
Runoff = 0.075 m<sup>3</sup>/s @ 8.14 hrs, Volume= 128.4 m<sup>3</sup>, Depth> 31 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 5-Year Rainfall=60 mm

Area (m <sup>2</sup> )	CN	Description
1,721.0	98	Paved parking, HSG A
2,395.0	80	>75% Grass cover, Good, HSG D
4,116.0	88	Weighted Average
2,395.0		58.19% Pervious Area
1,721.0		41.81% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

**Subcatchment 3S: PRE**



**Summary for Subcatchment 4S: Uncontrolled Area**

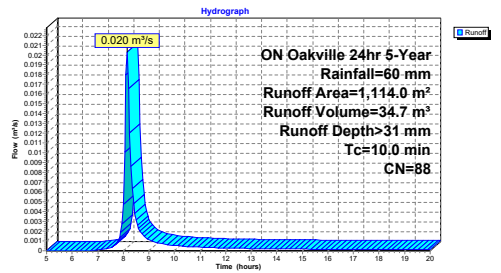
Runoff = 0.020 m<sup>3</sup>/s @ 8.14 hrs, Volume= 34.7 m<sup>3</sup>, Depth> 31 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 5-Year Rainfall=60 mm

Area (m <sup>2</sup> )	CN	Description
507.0	98	Water Surface, HSG A
607.0	80	>75% Grass cover, Good, HSG D
1,114.0	88	Weighted Average
607.0		54.49% Pervious Area
507.0		45.51% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

**Subcatchment 4S: Uncontrolled Area**



**Summary for Subcatchment 5S: Controlled Area - Lots 4-5**

Runoff = 0.011 m<sup>3</sup>/s @ 8.22 hrs, Volume= 24.1 m<sup>3</sup>, Depth> 28 mm

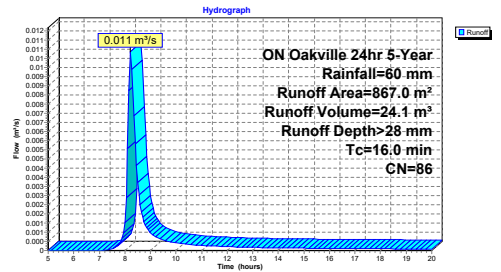
Routed to Pond 2P : CBMH 4-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 5-Year Rainfall=60 mm

Area (m <sup>2</sup> )	CN	Description
307.0	98	Paved parking, HSG A
560.0	80	>75% Grass cover, Good, HSG D
867.0	86	Weighted Average
560.0		64.59% Pervious Area
307.0		35.41% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
16.0					Direct Entry,

**Subcatchment 5S: Controlled Area - Lots 4-5**



**Summary for Subcatchment 6S: Controlled Area - Lots 6-7**

Runoff = 0.014 m<sup>3</sup>/s @ 8.22 hrs, Volume= 30.5 m<sup>3</sup>, Depth> 29 mm

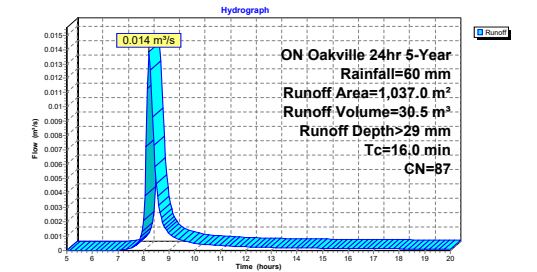
Routed to Pond 8P : CBMH 6-7

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 5-Year Rainfall=60 mm

Area (m <sup>2</sup> )	CN	Description
393.0	98	Paved parking, HSG D
644.0	80	>75% Grass cover, Good, HSG D
1,037.0	87	Weighted Average
644.0		62.10% Pervious Area
393.0		37.90% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
16.0					Direct Entry,

**Subcatchment 6S: Controlled Area - Lots 6-7**





Summary for Pond 2P: CBMH 4-5

Inflow Area = 867.0 m<sup>2</sup>, 35.41% Impervious, Inflow Depth > 28 mm for 5-Year event  
 Inflow = 0.011 m<sup>3</sup>/s @ 8.22 hrs, Volume= 24.1 m<sup>3</sup>  
 Outflow = 0.008 m<sup>3</sup>/s @ 8.32 hrs, Volume= 24.1 m<sup>3</sup>, Atten= 23%, Lag= 6.0 min  
 Primary = 0.008 m<sup>3</sup>/s @ 8.32 hrs, Volume= 24.1 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.297 m @ 8.32 hrs Storage= 2.9 m<sup>3</sup>

Plug-Flow detention time= 4.9 min calculated for 24.0 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 4.2 min ( 584.5 - 580.3 )

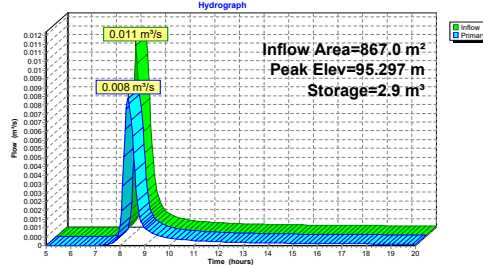
Volume	Invert	Avail. Storage	Storage Description
#1	94.810 m	19.5 m <sup>3</sup>	Custom Stage Data Listed below

Elevation (meters)	Cum. Store (cubic-meters)
94.810	0.0
97.110	13.5
97.260	19.5

Device	Routing	Invert	Outlet Devices
#1	Primary	94.810 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.008 m<sup>3</sup>/s @ 8.32 hrs HW=95.290 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.008 m<sup>3</sup>/s @ 1.89 m/s)

Pond 2P: CBMH 4-5



Summary for Pond 7P: CBMH 1-2-3

Inflow Area = 1,039.0 m<sup>2</sup>, 53.13% Impervious, Inflow Depth > 35 mm for 5-Year event  
 Inflow = 0.014 m<sup>3</sup>/s @ 8.28 hrs, Volume= 36.1 m<sup>3</sup>  
 Outflow = 0.011 m<sup>3</sup>/s @ 8.39 hrs, Volume= 36.1 m<sup>3</sup>, Atten= 21%, Lag= 6.9 min  
 Primary = 0.011 m<sup>3</sup>/s @ 8.39 hrs, Volume= 36.1 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.580 m @ 8.39 hrs Storage= 4.1 m<sup>3</sup>

Plug-Flow detention time= 4.6 min calculated for 35.9 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 4.1 min ( 577.2 - 573.2 )

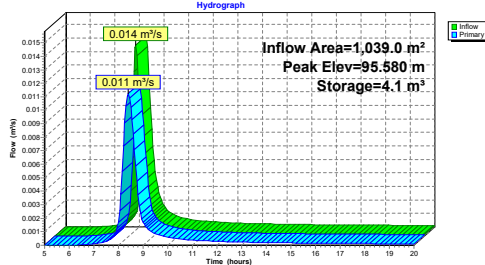
Volume	Invert	Avail. Storage	Storage Description
#1	94.740 m	15.1 m <sup>3</sup>	Custom Stage Data Listed below

Elevation (meters)	Cum. Store (cubic-meters)
94.740	0.0
96.970	11.0
97.260	15.1

Device	Routing	Invert	Outlet Devices
#1	Primary	94.740 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.011 m<sup>3</sup>/s @ 8.39 hrs HW=95.575 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.011 m<sup>3</sup>/s @ 2.53 m/s)

Pond 7P: CBMH 1-2-3



Summary for Pond 8P: CBMH 6-7

Inflow Area = 1,037.0 m<sup>2</sup>, 37.90% Impervious, Inflow Depth > 29 mm for 5-Year event  
 Inflow = 0.014 m<sup>3</sup>/s @ 8.22 hrs, Volume= 30.5 m<sup>3</sup>  
 Outflow = 0.010 m<sup>3</sup>/s @ 8.34 hrs, Volume= 30.5 m<sup>3</sup>, Atten= 29%, Lag= 7.1 min  
 Primary = 0.010 m<sup>3</sup>/s @ 8.34 hrs, Volume= 30.5 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.156 m @ 8.34 hrs Storage= 4.4 m<sup>3</sup>

Plug-Flow detention time= 6.1 min calculated for 30.5 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 5.2 min ( 582.8 - 577.6 )

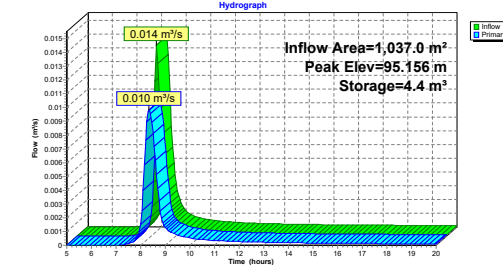
Volume	Invert	Avail. Storage	Storage Description
#1	94.500 m	14.7 m <sup>3</sup>	Custom Stage Data Listed below

Elevation (meters)	Cum. Store (cubic-meters)
94.500	0.0
96.520	13.5
96.670	14.7

Device	Routing	Invert	Outlet Devices
#1	Primary	94.500 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

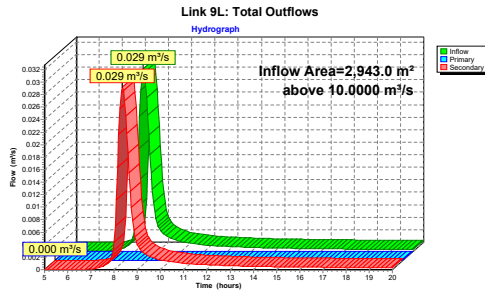
Primary OutFlow Max=0.010 m<sup>3</sup>/s @ 8.34 hrs HW=95.152 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.010 m<sup>3</sup>/s @ 2.22 m/s)

Pond 8P: CBMH 6-7



Summary for Link 9L: Total Outflows

Inflow Area = 2,943.0 m<sup>2</sup>, 42.54% Impervious, Inflow Depth > 31 mm for 5-Year event  
 Inflow = 0.029 m<sup>3</sup>/s @ 8.35 hrs, Volume= 90.7 m<sup>3</sup>  
 Primary = 0.000 m<sup>3</sup>/s @ 5.00 hrs, Volume= 0.0 m<sup>3</sup>, Atten= 100%, Lag= 0.0 min  
 Secondary = 0.029 m<sup>3</sup>/s @ 8.35 hrs, Volume= 90.7 m<sup>3</sup>  
 Primary outflow = Inflow above 10.0000 m<sup>3</sup>/s, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

- Subcatchment 1S: Controlled Area -** Runoff Area=1,039.0 m<sup>2</sup> 53.13% Impervious Runoff Depth>43 mm  
 Tc=20.6 min CN=90 Runoff=0.018 m<sup>3</sup>/s 44.6 m<sup>3</sup>
  - Subcatchment 3S: PRE** Runoff Area=4,116.0 m<sup>2</sup> 41.81% Impervious Runoff Depth>39 mm  
 Tc=10.0 min CN=88 Runoff=0.096 m<sup>3</sup>/s 160.5 m<sup>3</sup>
  - Subcatchment 4S: Uncontrolled Area** Runoff Area=1,114.0 m<sup>2</sup> 45.51% Impervious Runoff Depth>39 mm  
 Tc=10.0 min CN=88 Runoff=0.026 m<sup>3</sup>/s 43.4 m<sup>3</sup>
  - Subcatchment 5S: Controlled Area - Lots** Runoff Area=867.0 m<sup>2</sup> 35.41% Impervious Runoff Depth>35 mm  
 Tc=16.0 min CN=86 Runoff=0.014 m<sup>3</sup>/s 30.6 m<sup>3</sup>
  - Subcatchment 6S: Controlled Area -** Runoff Area=1,037.0 m<sup>2</sup> 37.90% Impervious Runoff Depth>37 mm  
 Tc=16.0 min CN=87 Runoff=0.018 m<sup>3</sup>/s 38.5 m<sup>3</sup>
  - Pond 2P: CBMH 4-5** Peak Elev=95.528 m Storage=4.2 m<sup>3</sup> Inflow=0.014 m<sup>3</sup>/s 30.6 m<sup>3</sup>  
 Outflow=0.010 m<sup>3</sup>/s 30.6 m<sup>3</sup>
  - Pond 7P: CBMH 1-2-3** Peak Elev=95.936 m Storage=5.9 m<sup>3</sup> Inflow=0.018 m<sup>3</sup>/s 44.6 m<sup>3</sup>  
 Outflow=0.013 m<sup>3</sup>/s 44.5 m<sup>3</sup>
  - Pond 8P: CBMH 6-7** Peak Elev=95.450 m Storage=6.3 m<sup>3</sup> Inflow=0.018 m<sup>3</sup>/s 38.5 m<sup>3</sup>  
 Outflow=0.012 m<sup>3</sup>/s 38.4 m<sup>3</sup>
  - Link 9L: Total Outflows** above 10.0000 m<sup>3</sup>/s Inflow=0.036 m<sup>3</sup>/s 113.5 m<sup>3</sup>  
 Primary=0.000 m<sup>3</sup>/s 0.0 m<sup>3</sup> Secondary=0.036 m<sup>3</sup>/s 113.5 m<sup>3</sup>
- Total Runoff Area = 8,173.0 m<sup>2</sup> Runoff Volume = 317.5 m<sup>3</sup> Average Runoff Depth = 39 mm**  
**57.42% Pervious = 4,693.0 m<sup>2</sup> 42.58% Impervious = 3,480.0 m<sup>2</sup>**

Summary for Subcatchment 1S: Controlled Area - Lots 1-2-3

Runoff = 0.018 m<sup>3</sup>/s @ 8.27 hrs, Volume= 44.6 m<sup>3</sup>, Depth> 43 mm  
 Routed to Pond 7P : CBMH 1-2-3

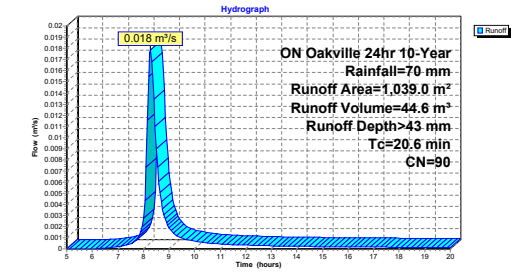
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 10-Year Rainfall=70 mm

Area (m <sup>2</sup> )	CN	Description
552.0	98	Paved parking, HSG A
487.0	80	>75% Grass cover, Good, HSG D
1,039.0	90	Weighted Average
487.0		46.87% Pervious Area
552.0		53.13% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
20.6					Direct Entry,

Subcatchment 1S: Controlled Area - Lots 1-2-3



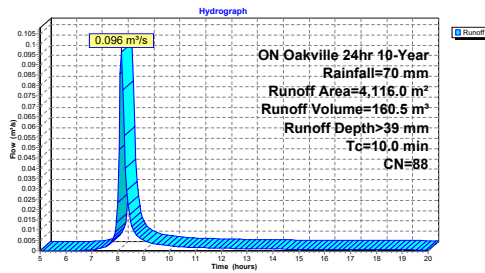
Summary for Subcatchment 3S: PRE

Runoff = 0.096 m<sup>3</sup>/s @ 8.14 hrs, Volume= 160.5 m<sup>3</sup>, Depth> 39 mm  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 10-Year Rainfall=70 mm

Area (m <sup>2</sup> )	CN	Description
1,721.0	98	Paved parking, HSG A
2,395.0	80	>75% Grass cover, Good, HSG D
4,116.0	88	Weighted Average
2,395.0		58.19% Pervious Area
1,721.0		41.81% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

Subcatchment 3S: PRE



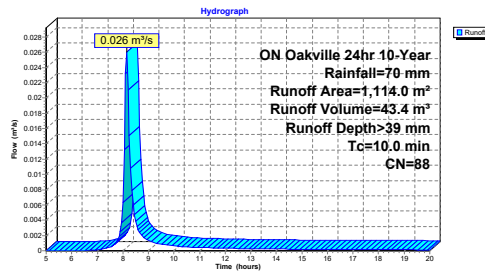
Summary for Subcatchment 4S: Uncontrolled Area

Runoff = 0.026 m<sup>3</sup>/s @ 8.14 hrs, Volume= 43.4 m<sup>3</sup>, Depth> 39 mm  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 10-Year Rainfall=70 mm

Area (m <sup>2</sup> )	CN	Description
507.0	98	Water Surface, HSG A
607.0	80	>75% Grass cover, Good, HSG D
1,114.0	88	Weighted Average
607.0		54.49% Pervious Area
507.0		45.51% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

Subcatchment 4S: Uncontrolled Area



Summary for Subcatchment 5S: Controlled Area - Lots 4-5

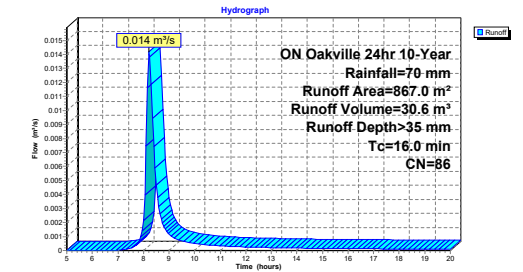
Runoff = 0.014 m<sup>3</sup>/s @ 8.22 hrs, Volume= 30.6 m<sup>3</sup>, Depth> 35 mm  
 Routed to Pond 2P : CBMH 4-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 10-Year Rainfall=70 mm

Area (m <sup>2</sup> )	CN	Description
307.0	98	Paved parking, HSG A
560.0	80	>75% Grass cover, Good, HSG D
867.0	86	Weighted Average
560.0		64.59% Pervious Area
307.0		35.41% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
16.0					Direct Entry,

Subcatchment 5S: Controlled Area - Lots 4-5



Summary for Subcatchment 6S: Controlled Area - Lots 6-7

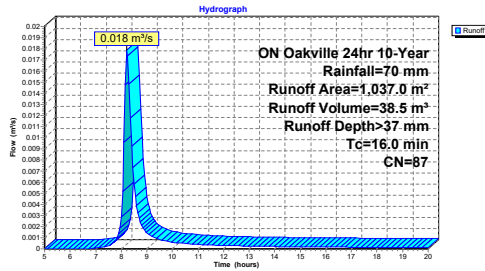
Runoff = 0.018 m³/s @ 8.22 hrs, Volume= 38.5 m³, Depth> 37 mm  
 Routed to Pond 8P : CBMH 6-7

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 10-Year Rainfall=70 mm

Area (m²)	CN	Description
393.0	98	Paved parking, HSG D
644.0	80	>75% Grass cover, Good, HSG D
1,037.0	87	Weighted Average
644.0	62	10% Pervious Area
393.0	37	90% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 6S: Controlled Area - Lots 6-7



Summary for Pond 2P: CBMH 4-5

Inflow Area = 867.0 m², 35.41% Impervious, Inflow Depth > 35 mm for 10-Year event  
 Inflow = 0.014 m³/s @ 8.22 hrs, Volume= 30.6 m³  
 Outflow = 0.010 m³/s @ 8.33 hrs, Volume= 30.6 m³, Atten= 27%, Lag= 6.7 min  
 Primary = 0.010 m³/s @ 8.33 hrs, Volume= 30.6 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.528 m @ 8.33 hrs Storage= 4.2 m³

Plug-Flow detention time= 5.3 min calculated for 30.5 m³ (100% of inflow)  
 Center-of-Mass det. time= 4.7 min ( 578.6 - 573.9 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.810 m	19.5 m³	Custom Stage Data Listed below

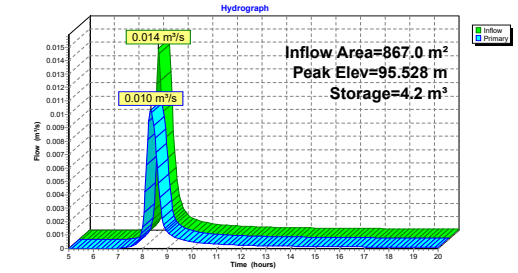
  

Elevation (meters)	Cum. Store (cubic-meters)
94.810	0.0
97.110	13.5
97.260	19.5

Device	Routing	Invert	Outlet Devices
#1	Primary	94.810 m	75 mm Vert. Orifice/Gate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.010 m³/s @ 8.33 hrs HW=95.521 m (Free Discharge)  
 1=Orifice/Gate (Orifice Controls 0.010 m³/s @ 2.33 m/s)

Pond 2P: CBMH 4-5



Summary for Pond 7P: CBMH 1-2-3

Inflow Area = 1,039.0 m², 53.13% Impervious, Inflow Depth > 43 mm for 10-Year event  
 Inflow = 0.018 m³/s @ 8.27 hrs, Volume= 44.6 m³  
 Outflow = 0.013 m³/s @ 8.40 hrs, Volume= 44.5 m³, Atten= 25%, Lag= 7.7 min  
 Primary = 0.013 m³/s @ 8.40 hrs, Volume= 44.5 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.936 m @ 8.40 hrs Storage= 5.9 m³

Plug-Flow detention time= 5.1 min calculated for 44.4 m³ (100% of inflow)  
 Center-of-Mass det. time= 4.6 min ( 572.5 - 567.9 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.740 m	15.1 m³	Custom Stage Data Listed below

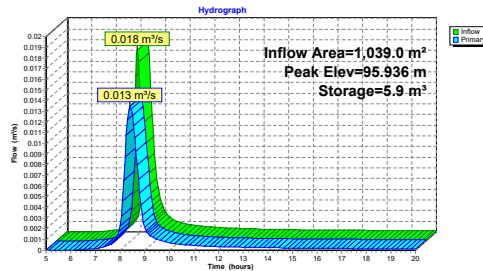
  

Elevation (meters)	Cum. Store (cubic-meters)
94.740	0.0
96.970	11.0
97.260	15.1

Device	Routing	Invert	Outlet Devices
#1	Primary	94.740 m	75 mm Vert. Orifice/Gate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.013 m³/s @ 8.40 hrs HW=95.934 m (Free Discharge)  
 1=Orifice/Gate (Orifice Controls 0.013 m³/s @ 3.05 m/s)

Pond 7P: CBMH 1-2-3



Summary for Pond 8P: CBMH 6-7

Inflow Area = 1,037.0 m², 37.90% Impervious, Inflow Depth > 37 mm for 10-Year event  
 Inflow = 0.018 m³/s @ 8.22 hrs, Volume= 38.5 m³  
 Outflow = 0.012 m³/s @ 8.35 hrs, Volume= 38.4 m³, Atten= 33%, Lag= 7.9 min  
 Primary = 0.012 m³/s @ 8.35 hrs, Volume= 38.4 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.450 m @ 8.35 hrs Storage= 6.3 m³

Plug-Flow detention time= 6.7 min calculated for 38.3 m³ (100% of inflow)  
 Center-of-Mass det. time= 5.8 min ( 577.4 - 571.6 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.500 m	14.7 m³	Custom Stage Data Listed below

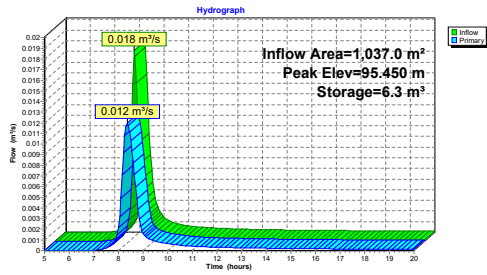
  

Elevation (meters)	Cum. Store (cubic-meters)
94.500	0.0
96.520	13.5
96.670	14.7

Device	Routing	Invert	Outlet Devices
#1	Primary	94.500 m	75 mm Vert. Orifice/Gate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.012 m³/s @ 8.35 hrs HW=95.449 m (Free Discharge)  
 1=Orifice/Gate (Orifice Controls 0.012 m³/s @ 2.71 m/s)

Pond 8P: CBMH 6-7

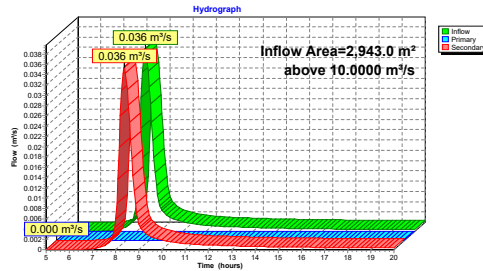


Summary for Link 9L: Total Outflows

Inflow Area = 2,943.0 m<sup>2</sup>, 42.54% Impervious, Inflow Depth > 39 mm for 10-Year event  
 Inflow = 0.036 m<sup>3</sup>/s @ 8.36 hrs, Volume= 113.5 m<sup>3</sup>  
 Primary = 0.000 m<sup>3</sup>/s @ 5.00 hrs, Volume= 0.0 m<sup>3</sup>; Atten= 100%, Lag= 0.0 min  
 Secondary = 0.036 m<sup>3</sup>/s @ 8.36 hrs, Volume= 113.5 m<sup>3</sup>

Primary outflow = Inflow above 10.0000 m<sup>3</sup>/s, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 9L: Total Outflows



Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

- Subcatchment 1S: Controlled Area -** Runoff Area=1,039.0 m<sup>2</sup> 53.13% Impervious Runoff Depth=54 mm  
 Tc=20.6 min CN=90 Runoff=0.023 m<sup>3</sup>/s 55.8 m<sup>3</sup>
  - Subcatchment 3S: PRE** Runoff Area=4,116.0 m<sup>2</sup> 41.81% Impervious Runoff Depth>50 mm  
 Tc=10.0 min CN=88 Runoff=0.125 m<sup>3</sup>/s 203.8 m<sup>3</sup>
  - Subcatchment 4S: Uncontrolled Area** Runoff Area=1,114.0 m<sup>2</sup> 45.51% Impervious Runoff Depth>50 mm  
 Tc=10.0 min CN=88 Runoff=0.034 m<sup>3</sup>/s 55.2 m<sup>3</sup>
  - Subcatchment 5S: Controlled Area - Lots** Runoff Area=867.0 m<sup>2</sup> 35.41% Impervious Runoff Depth=45 mm  
 Tc=16.0 min CN=86 Runoff=0.019 m<sup>3</sup>/s 39.4 m<sup>3</sup>
  - Subcatchment 6S: Controlled Area -** Runoff Area=1,037.0 m<sup>2</sup> 37.90% Impervious Runoff Depth=47 mm  
 Tc=16.0 min CN=87 Runoff=0.023 m<sup>3</sup>/s 49.2 m<sup>3</sup>
  - Pond 2P: CBMH 4-5** Peak Elev=95.886 m Storage=6.3 m<sup>3</sup> Inflow=0.019 m<sup>3</sup>/s 39.4 m<sup>3</sup>  
 Outflow=0.013 m<sup>3</sup>/s 39.3 m<sup>3</sup>
  - Pond 7P: CBMH 1-2-3** Peak Elev=96.465 m Storage=8.5 m<sup>3</sup> Inflow=0.023 m<sup>3</sup>/s 55.8 m<sup>3</sup>  
 Outflow=0.016 m<sup>3</sup>/s 55.8 m<sup>3</sup>
  - Pond 8P: CBMH 6-7** Peak Elev=95.891 m Storage=9.3 m<sup>3</sup> Inflow=0.023 m<sup>3</sup>/s 49.2 m<sup>3</sup>  
 Outflow=0.015 m<sup>3</sup>/s 49.1 m<sup>3</sup>
  - Link 9L: Total Outflows** above 10.0000 m<sup>3</sup>/s Inflow=0.043 m<sup>3</sup>/s 144.2 m<sup>3</sup>  
 Primary=0.000 m<sup>3</sup>/s 0.0 m<sup>3</sup> Secondary=0.043 m<sup>3</sup>/s 144.2 m<sup>3</sup>
- Total Runoff Area = 8,173.0 m<sup>2</sup> Runoff Volume = 403.3 m<sup>3</sup> Average Runoff Depth = 49 mm**  
**57.42% Pervious = 4,693.0 m<sup>2</sup> 42.58% Impervious = 3,480.0 m<sup>2</sup>**

Summary for Subcatchment 1S: Controlled Area - Lots 1-2-3

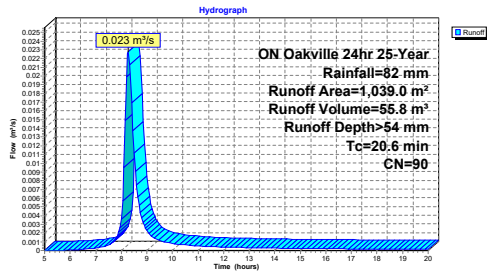
Runoff = 0.023 m<sup>3</sup>/s @ 8.27 hrs, Volume= 55.8 m<sup>3</sup>, Depth> 54 mm  
 Routed to Pond 7P : CBMH 1-2-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 25-Year Rainfall=82 mm

Area (m <sup>2</sup> )	CN	Description
552.0	98	Paved parking, HSG A
487.0	80	>75% Grass cover, Good, HSG D
1,039.0	90	Weighted Average
487.0		46.87% Pervious Area
552.0		53.13% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
20.6					Direct Entry,

Subcatchment 1S: Controlled Area - Lots 1-2-3



Summary for Subcatchment 3S: PRE

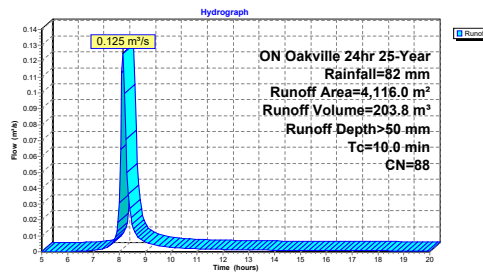
Runoff = 0.125 m<sup>3</sup>/s @ 8.14 hrs, Volume= 203.8 m<sup>3</sup>, Depth> 50 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 25-Year Rainfall=82 mm

Area (m <sup>2</sup> )	CN	Description
1,721.0	98	Paved parking, HSG A
2,395.0	80	>75% Grass cover, Good, HSG D
4,116.0	88	Weighted Average
2,395.0		58.19% Pervious Area
1,721.0		41.81% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

Subcatchment 3S: PRE



Summary for Subcatchment 4S: Uncontrolled Area

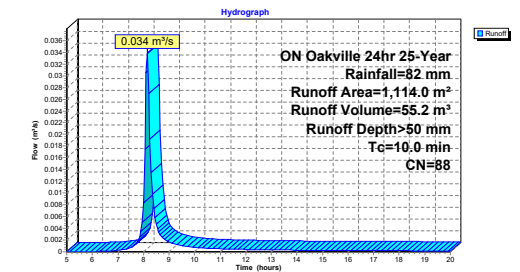
Runoff = 0.034 m<sup>3</sup>/s @ 8.14 hrs, Volume= 55.2 m<sup>3</sup>, Depth> 50 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 25-Year Rainfall=82 mm

Area (m <sup>2</sup> )	CN	Description
507.0	98	Water Surface, HSG A
607.0	80	>75% Grass cover, Good, HSG D
1,114.0	88	Weighted Average
607.0		54.49% Pervious Area
507.0		45.51% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

Subcatchment 4S: Uncontrolled Area



Summary for Subcatchment 5S: Controlled Area - Lots 4-5

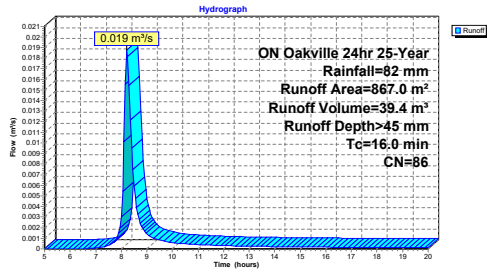
Runoff = 0.019 m³/s @ 8.22 hrs, Volume= 39.4 m³, Depth> 45 mm  
 Routed to Pond 2P : CBMH 4-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 25-Year Rainfall=82 mm

Area (m²)	CN	Description
307.0	98	Paved parking, HSG A
560.0	80	>75% Grass cover, Good, HSG D
867.0	86	Weighted Average
560.0		64.59% Pervious Area
307.0		35.41% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 5S: Controlled Area - Lots 4-5



Summary for Subcatchment 6S: Controlled Area - Lots 6-7

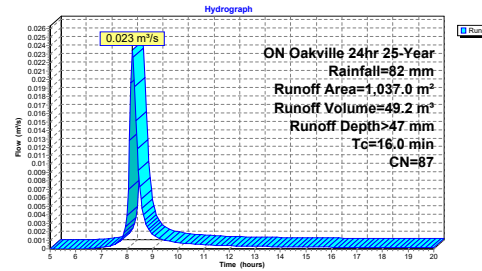
Runoff = 0.023 m³/s @ 8.22 hrs, Volume= 49.2 m³, Depth> 47 mm  
 Routed to Pond 8P : CBMH 6-7

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 25-Year Rainfall=82 mm

Area (m²)	CN	Description
393.0	98	Paved parking, HSG D
644.0	80	>75% Grass cover, Good, HSG D
1,037.0	87	Weighted Average
644.0		62.10% Pervious Area
393.0		37.90% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 6S: Controlled Area - Lots 6-7



Summary for Pond 2P: CBMH 4-5

Inflow Area = 867.0 m², 35.41% Impervious, Inflow Depth > 45 mm for 25-Year event  
 Inflow = 0.019 m³/s @ 8.22 hrs, Volume= 39.4 m³  
 Outflow = 0.013 m³/s @ 8.34 hrs, Volume= 39.3 m³, Atten= 32%, Lag= 7.5 min  
 Primary = 0.013 m³/s @ 8.34 hrs, Volume= 39.3 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.886 m @ 8.34 hrs Storage= 6.3 m³

Plug-Flow detention time= 6.0 min calculated for 39.3 m³ (100% of inflow)  
 Center-of-Mass det. time= 5.3 min ( 573.6 - 568.3 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.810 m	19.5 m³	Custom Stage Data Listed below

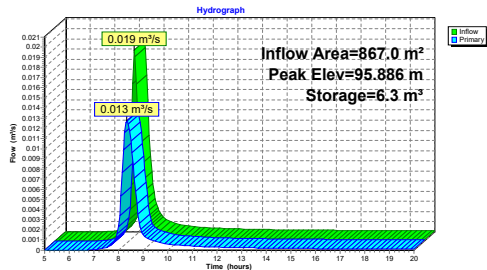
  

Elevation (meters)	Cum. Store (cubic-meters)
94.810	0.0
97.110	13.5
97.260	19.5

Device	Routing	Invert	Outlet Devices
#1	Primary	94.810 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.013 m³/s @ 8.34 hrs HW=95.882 m (Free Discharge)  
 Orifice/Grate (Orifice Controls 0.013 m³/s @ 2.88 m/s)

Pond 2P: CBMH 4-5



Summary for Pond 7P: CBMH 1-2-3

Inflow Area = 1,039.0 m², 53.13% Impervious, Inflow Depth > 54 mm for 25-Year event  
 Inflow = 0.023 m³/s @ 8.27 hrs, Volume= 55.8 m³  
 Outflow = 0.016 m³/s @ 8.41 hrs, Volume= 55.9 m³, Atten= 29%, Lag= 8.4 min  
 Primary = 0.016 m³/s @ 8.41 hrs, Volume= 55.8 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.465 m @ 8.41 hrs Storage= 8.5 m³

Plug-Flow detention time= 5.8 min calculated for 55.6 m³ (100% of inflow)  
 Center-of-Mass det. time= 5.3 min ( 568.4 - 563.1 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.740 m	15.1 m³	Custom Stage Data Listed below

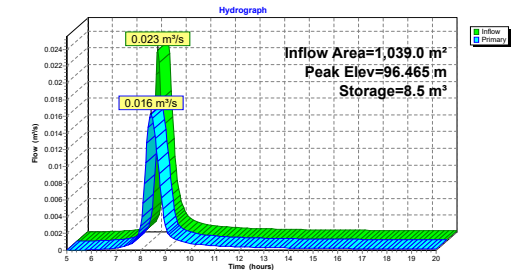
  

Elevation (meters)	Cum. Store (cubic-meters)
94.740	0.0
96.970	11.0
97.260	15.1

Device	Routing	Invert	Outlet Devices
#1	Primary	94.740 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.016 m³/s @ 8.41 hrs HW=96.453 m (Free Discharge)  
 Orifice/Grate (Orifice Controls 0.016 m³/s @ 3.67 m/s)

Pond 7P: CBMH 1-2-3



Summary for Pond 8P: CBMH 6-7

Inflow Area = 1,037.0 m<sup>2</sup>, 37.90% Impervious, Inflow Depth > 47 mm for 25-Year event  
 Inflow = 0.023 m<sup>3</sup>/s @ 8.22 hrs, Volume= 49.2 m<sup>3</sup>  
 Outflow = 0.015 m<sup>3</sup>/s @ 8.36 hrs, Volume= 49.1 m<sup>3</sup>, Atten= 38%, Lag= 8.6 min  
 Primary = 0.015 m<sup>3</sup>/s @ 8.36 hrs, Volume= 49.1 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 95.891 m @ 8.36 hrs Storage= 9.3 m<sup>3</sup>

Plug-Flow detention time= 7.4 min calculated for 48.9 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 6.6 min ( 572.8 - 566.2 )

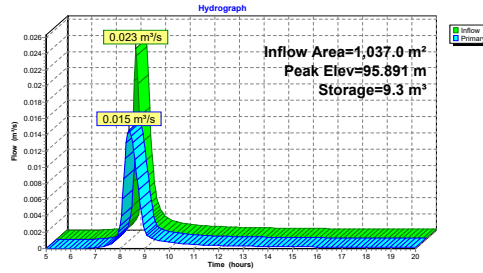
Volume Invert Avail.Storage Storage Description  
 #1 94.500 m 14.7 m<sup>3</sup> Custom Stage Data Listed below

Elevation (meters)	Cum.Store (cubic-meters)
94.500	0.0
95.520	13.5
96.670	14.7

Device	Routing	Invert	Outlet Devices
#1	Primary	94.500 m	75 mm Vert. Orifice/Grate C=0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.015 m<sup>3</sup>/s @ 8.36 hrs HW=95.882 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.015 m<sup>3</sup>/s @ 3.29 m/s)

Pond 8P: CBMH 6-7

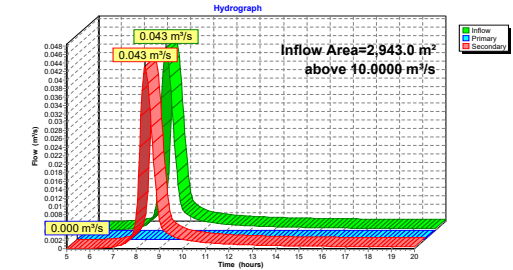


Summary for Link 9L: Total Outflows

Inflow Area = 2,943.0 m<sup>2</sup>, 42.54% Impervious, Inflow Depth > 49 mm for 25-Year event  
 Inflow = 0.043 m<sup>3</sup>/s @ 8.37 hrs, Volume= 144.2 m<sup>3</sup>  
 Primary = 0.000 m<sup>3</sup>/s @ 5.00 hrs, Volume= 0.0 m<sup>3</sup>, Atten= 100%, Lag= 0.0 min  
 Secondary = 0.043 m<sup>3</sup>/s @ 8.37 hrs, Volume= 144.2 m<sup>3</sup>

Primary outflow = Inflow above 10.0000 m<sup>3</sup>/s, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 9L: Total Outflows



Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Controlled Area - Runoff Area=1,039.0 m<sup>2</sup> 53.13% Impervious Runoff Depth=60 mm  
 Tc=20.6 min CN=90 Runoff=0.026 m<sup>3</sup>/s 62.5 m<sup>3</sup>

Subcatchment 3S: PRE Runoff Area=4,116.0 m<sup>2</sup> 41.81% Impervious Runoff Depth=56 mm  
 Tc=10.0 min CN=88 Runoff=0.146 m<sup>3</sup>/s 229.6 m<sup>3</sup>

Subcatchment 4S: Uncontrolled Area Runoff Area=1,114.0 m<sup>2</sup> 45.51% Impervious Runoff Depth=56 mm  
 Tc=10.0 min CN=88 Runoff=0.039 m<sup>3</sup>/s 62.1 m<sup>3</sup>

Subcatchment 5S: Controlled Area - Lots Runoff Area=867.0 m<sup>2</sup> 35.41% Impervious Runoff Depth=51 mm  
 Tc=16.0 min CN=86 Runoff=0.022 m<sup>3</sup>/s 44.6 m<sup>3</sup>

Subcatchment 6S: Controlled Area - Runoff Area=1,037.0 m<sup>2</sup> 37.90% Impervious Runoff Depth=54 mm  
 Tc=16.0 min CN=87 Runoff=0.027 m<sup>3</sup>/s 55.5 m<sup>3</sup>

Pond 2P: CBMH 4-5 Peak Elev=96.161 m Storage=7.9 m<sup>3</sup> Inflow=0.022 m<sup>3</sup>/s 44.6 m<sup>3</sup>  
 Outflow=0.014 m<sup>3</sup>/s 44.6 m<sup>3</sup>

Pond 7P: CBMH 1-2-3 Peak Elev=96.869 m Storage=10.5 m<sup>3</sup> Inflow=0.026 m<sup>3</sup>/s 62.5 m<sup>3</sup>  
 Outflow=0.018 m<sup>3</sup>/s 62.5 m<sup>3</sup>

Pond 8P: CBMH 6-7 Peak Elev=96.225 m Storage=11.5 m<sup>3</sup> Inflow=0.027 m<sup>3</sup>/s 55.5 m<sup>3</sup>  
 Outflow=0.016 m<sup>3</sup>/s 55.5 m<sup>3</sup>

Link 9L: Total Outflows above 10.0000 m<sup>3</sup>/s Inflow=0.048 m<sup>3</sup>/s 162.5 m<sup>3</sup>  
 Primary=0.000 m<sup>3</sup>/s 0.0 m<sup>3</sup> Secondary=0.048 m<sup>3</sup>/s 162.5 m<sup>3</sup>

Total Runoff Area = 8,173.0 m<sup>2</sup> Runoff Volume = 454.4 m<sup>3</sup> Average Runoff Depth = 56 mm  
 57.42% Pervious = 4,693.0 m<sup>2</sup> 42.58% Impervious = 3,480.0 m<sup>2</sup>

Summary for Subcatchment 1S: Controlled Area - Lots 1-2-3

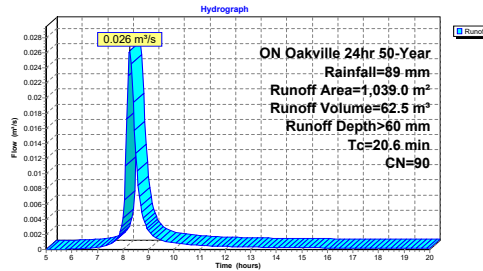
Runoff = 0.026 m<sup>3</sup>/s @ 8.27 hrs, Volume= 62.5 m<sup>3</sup>, Depth> 60 mm  
 Routed to Pond 7P : CBMH 1-2-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 50-Year Rainfall=89 mm

Area (m <sup>2</sup> )	CN	Description
552.0	98	Paved parking, HSG A
487.0	80	>75% Grass cover, Good, HSG D
1,039.0	90	Weighted Average
487.0		46.87% Pervious Area
552.0		53.13% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
20.6					Direct Entry,

Subcatchment 1S: Controlled Area - Lots 1-2-3



Summary for Subcatchment 3S: PRE

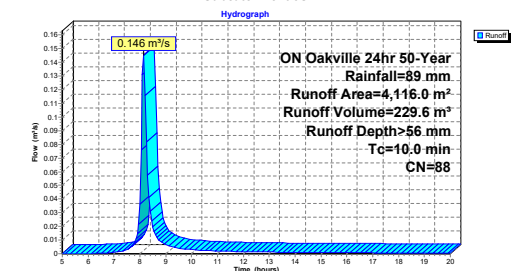
Runoff = 0.146 m<sup>3</sup>/s @ 8.14 hrs, Volume= 229.6 m<sup>3</sup>, Depth> 56 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 50-Year Rainfall=89 mm

Area (m <sup>2</sup> )	CN	Description
1,721.0	98	Paved parking, HSG A
2,395.0	80	>75% Grass cover, Good, HSG D
4,116.0	88	Weighted Average
2,395.0		58.19% Pervious Area
1,721.0		41.81% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
10.0					Direct Entry,

Subcatchment 3S: PRE



Summary for Subcatchment 4S: Uncontrolled Area

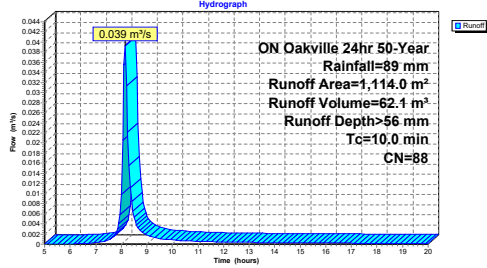
Runoff = 0.039 m³/s @ 8.14 hrs, Volume= 62.1 m³, Depth> 56 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 50-Year Rainfall=89 mm

Area (m²)	CN	Description
507.0	98	Water Surface, HSG A
607.0	80	>75% Grass cover, Good, HSG D
1,114.0	88	Weighted Average
607.0	88	54.49% Pervious Area
507.0	88	45.51% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
10.0					Direct Entry,

Subcatchment 4S: Uncontrolled Area



Summary for Subcatchment 5S: Controlled Area - Lots 4-5

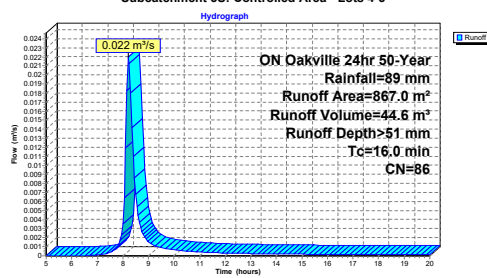
Runoff = 0.022 m³/s @ 8.22 hrs, Volume= 44.6 m³, Depth> 51 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 50-Year Rainfall=89 mm

Area (m²)	CN	Description
307.0	98	Paved parking, HSG A
560.0	80	>75% Grass cover, Good, HSG D
867.0	86	Weighted Average
560.0	86	64.59% Pervious Area
307.0	86	35.41% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 5S: Controlled Area - Lots 4-5



Summary for Subcatchment 6S: Controlled Area - Lots 6-7

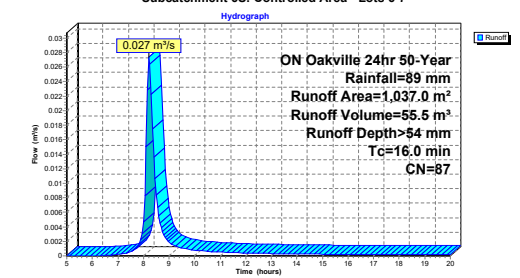
Runoff = 0.027 m³/s @ 8.22 hrs, Volume= 55.5 m³, Depth> 54 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 50-Year Rainfall=89 mm

Area (m²)	CN	Description
393.0	98	Paved parking, HSG D
644.0	80	>75% Grass cover, Good, HSG D
1,037.0	87	Weighted Average
644.0	87	62.10% Pervious Area
393.0	87	37.90% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 6S: Controlled Area - Lots 6-7



Summary for Pond 2P: CBMH 4-5

Inflow Area = 867.0 m², 35.41% Impervious, Inflow Depth > 51 mm for 50-Year event  
 Inflow = 0.022 m³/s @ 8.22 hrs, Volume= 44.6 m³  
 Outflow = 0.014 m³/s @ 8.35 hrs, Volume= 44.6 m³, Atten= 35%, Lag= 8.0 min  
 Primary = 0.014 m³/s @ 8.35 hrs, Volume= 44.6 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.161 m @ 8.35 hrs Storage= 7.9 m³

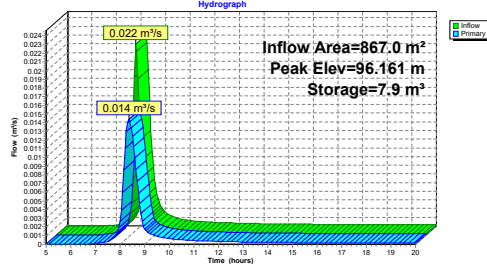
Plug-Flow detention time= 6.4 min calculated for 44.6 m³ (100% of inflow)  
 Center-of-Mass det. time= 5.8 min ( 568.5 - 562.7 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.810 m	19.5 m³	Custom Stage Data Listed below
	Elevation (meters)	Cum. Store (cubic-meters)	
	94.810	0.0	
	97.110	13.5	
	97.260	19.5	

Device	Routing	Invert	Outlet Devices
#1	Primary	94.810 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.014 m³/s @ 8.35 hrs HW=96.160 m (Free Discharge)  
 T=1=Orifice/Grate (Orifice Controls 0.014 m³/s @ 3.25 m/s)

Pond 2P: CBMH 4-5



Summary for Pond 7P: CBMH 1-2-3

Inflow Area = 1,039.0 m², 53.13% Impervious, Inflow Depth > 60 mm for 50-Year event  
 Inflow = 0.026 m³/s @ 8.27 hrs, Volume= 62.5 m³  
 Outflow = 0.018 m³/s @ 8.42 hrs, Volume= 62.5 m³, Atten= 31%, Lag= 8.8 min  
 Primary = 0.018 m³/s @ 8.42 hrs, Volume= 62.5 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.869 m @ 8.42 hrs Storage= 10.5 m³

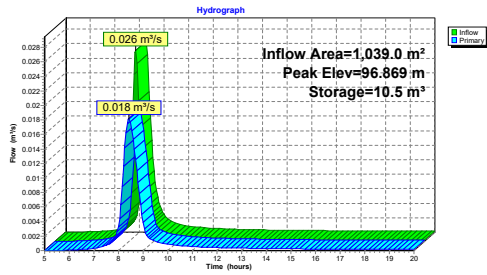
Plug-Flow detention time= 6.3 min calculated for 62.3 m³ (100% of inflow)  
 Center-of-Mass det. time= 5.9 min ( 564.2 - 558.3 )

Volume	Invert	Avail. Storage	Storage Description
#1	94.740 m	15.1 m³	Custom Stage Data Listed below
	Elevation (meters)	Cum. Store (cubic-meters)	
	94.740	0.0	
	96.970	11.0	
	97.260	15.1	

Device	Routing	Invert	Outlet Devices
#1	Primary	94.740 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.018 m³/s @ 8.42 hrs HW=96.852 m (Free Discharge)  
 T=1=Orifice/Grate (Orifice Controls 0.018 m³/s @ 4.08 m/s)

Pond 7P: CBMH 1-2-3



Summary for Pond 8P: CBMH 6-7

Inflow Area = 1,037.0 m<sup>2</sup>, 37.90% Impervious, Inflow Depth > 54 mm for 50-Year event  
 Inflow = 0.027 m<sup>3</sup>/s @ 8.22 hrs, Volume= 55.5 m<sup>3</sup>  
 Outflow = 0.016 m<sup>3</sup>/s @ 8.37 hrs, Volume= 55.5 m<sup>3</sup>, Atten= 41%, Lag= 9.0 min  
 Primary = 0.016 m<sup>3</sup>/s @ 8.37 hrs, Volume= 55.5 m<sup>3</sup>  
 Routed to Link 9L: Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.225 m @ 8.37 hrs Storage= 11.5 m<sup>3</sup>

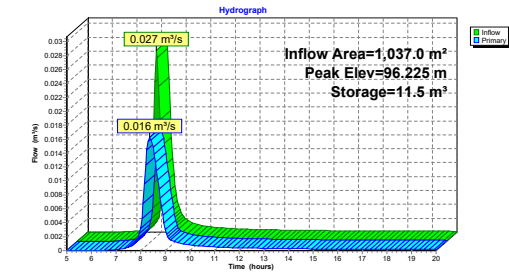
Plug-Flow detention time= 8.0 min calculated for 55.5 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 7.3 min (568.0 - 560.7)

Volume	Invert	Avail. Storage	Storage Description
#1	94.500 m	14.7 m <sup>3</sup>	Custom Stage Data Listed below
Elevation (meters)	Cum. Store (cubic-meters)		
94.500	0.0		
96.520	13.5		
96.670	14.7		

Device	Routing	Invert	Outlet Devices
#1	Primary	94.500 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary Outflow Max=0.016 m<sup>3</sup>/s @ 8.37 hrs HW=96.211 m (Free Discharge)  
 Orifice/Grate (Orifice Controls 0.016 m<sup>3</sup>/s @ 3.67 m/s)

Pond 8P: CBMH 6-7

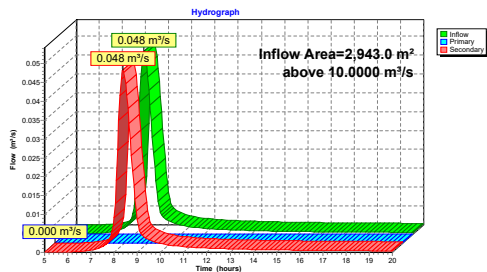


Summary for Link 9L: Total Outflows

Inflow Area = 2,943.0 m<sup>2</sup>, 42.54% Impervious, Inflow Depth > 55 mm for 50-Year event  
 Inflow = 0.048 m<sup>3</sup>/s @ 8.38 hrs, Volume= 162.5 m<sup>3</sup>  
 Primary = 0.000 m<sup>3</sup>/s @ 5.00 hrs, Volume= 0.0 m<sup>3</sup>, Atten= 100%, Lag= 0.0 min  
 Secondary = 0.048 m<sup>3</sup>/s @ 8.38 hrs, Volume= 162.5 m<sup>3</sup>

Primary outflow = Inflow above 10.0000 m<sup>3</sup>/s, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 9L: Total Outflows



Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points  
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN  
 Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1S: Controlled Area - Runoff Area=1,039.0 m<sup>2</sup> 53.13% Impervious Runoff Depth>68 mm  
 Tc=20.6 min CN=90 Runoff=0.030 m<sup>3</sup>/s 70.7 m<sup>3</sup>

Subcatchment 3S: PRE Runoff Area=4,116.0 m<sup>2</sup> 41.81% Impervious Runoff Depth>63 mm  
 Tc=10.0 min CN=88 Runoff=0.166 m<sup>3</sup>/s 261.3 m<sup>3</sup>

Subcatchment 4S: Uncontrolled Area Runoff Area=1,114.0 m<sup>2</sup> 45.51% Impervious Runoff Depth>63 mm  
 Tc=10.0 min CN=87 Runoff=0.045 m<sup>3</sup>/s 70.7 m<sup>3</sup>

Subcatchment 5S: Controlled Area - Lots Runoff Area=867.0 m<sup>2</sup> 35.41% Impervious Runoff Depth>59 mm  
 Tc=16.0 min CN=86 Runoff=0.025 m<sup>3</sup>/s 51.1 m<sup>3</sup>

Subcatchment 6S: Controlled Area - Runoff Area=1,037.0 m<sup>2</sup> 37.90% Impervious Runoff Depth>61 mm  
 Tc=16.0 min CN=87 Runoff=0.031 m<sup>3</sup>/s 63.4 m<sup>3</sup>

Pond 2P: CBMH 4-5 Peak Elev=96.462 m Storage=9.7 m<sup>3</sup> Inflow=0.025 m<sup>3</sup>/s 51.1 m<sup>3</sup>  
 Outflow=0.016 m<sup>3</sup>/s 51.1 m<sup>3</sup>

Pond 7P: CBMH 1-2-3 Peak Elev=97.098 m Storage=12.8 m<sup>3</sup> Inflow=0.030 m<sup>3</sup>/s 70.7 m<sup>3</sup>  
 Outflow=0.019 m<sup>3</sup>/s 70.7 m<sup>3</sup>

Pond 8P: CBMH 6-7 Peak Elev=96.577 m Storage=14.0 m<sup>3</sup> Inflow=0.031 m<sup>3</sup>/s 63.4 m<sup>3</sup>  
 Outflow=0.018 m<sup>3</sup>/s 63.4 m<sup>3</sup>

Link 9L: Total Outflows above 10.0000 m<sup>3</sup>/s Inflow=0.053 m<sup>3</sup>/s 185.1 m<sup>3</sup>  
 Primary=0.000 m<sup>3</sup>/s 0.0 m<sup>3</sup> Secondary=0.053 m<sup>3</sup>/s 185.1 m<sup>3</sup>

Total Runoff Area = 8,173.0 m<sup>2</sup> Runoff Volume = 517.3 m<sup>3</sup> Average Runoff Depth = 63 mm  
 57.42% Pervious = 4,693.0 m<sup>2</sup> 42.58% Impervious = 3,480.0 m<sup>2</sup>

Summary for Subcatchment 1S: Controlled Area - Lots 1-2-3

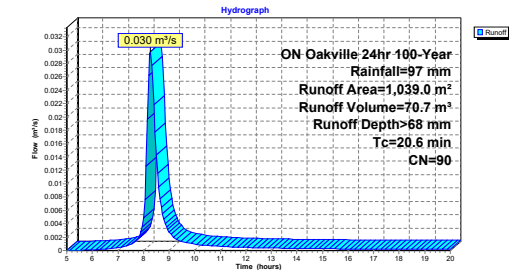
Runoff = 0.030 m<sup>3</sup>/s @ 8.27 hrs, Volume= 70.7 m<sup>3</sup>, Depth> 68 mm  
 Routed to Pond 7P: CBMH 1-2-3

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 100-Year Rainfall=97 mm

Area (m <sup>2</sup> )	CN	Description
552.0	98	Paved parking, HSG A
487.0	80	>75% Grass cover, Good, HSG D
1,039.0	90	Weighted Average
487.0		46.87% Pervious Area
552.0		53.13% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m <sup>3</sup> /s)	Description
20.6					Direct Entry,

Subcatchment 1S: Controlled Area - Lots 1-2-3





Summary for Subcatchment 3S: PRE

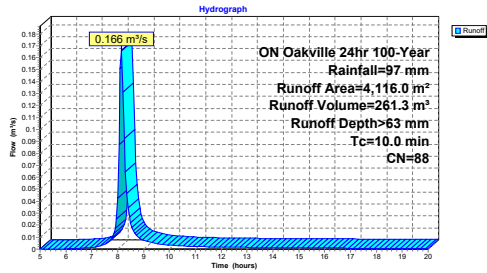
Runoff = 0.166 m³/s @ 8.14 hrs, Volume= 261.3 m³, Depth> 63 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 100-Year Rainfall=97 mm

Area (m²)	CN	Description
1,721.0	98	Paved parking, HSG A
2,395.0	80	>75% Grass cover, Good, HSG D
4,116.0	88	Weighted Average
2,395.0		58.19% Pervious Area
1,721.0		41.81% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
10.0					Direct Entry,

Subcatchment 3S: PRE



Summary for Subcatchment 4S: Uncontrolled Area

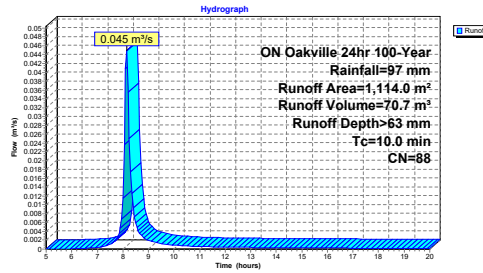
Runoff = 0.045 m³/s @ 8.14 hrs, Volume= 70.7 m³, Depth> 63 mm

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 100-Year Rainfall=97 mm

Area (m²)	CN	Description
507.0	98	Water Surface, HSG A
607.0	80	>75% Grass cover, Good, HSG D
1,114.0	88	Weighted Average
607.0		54.49% Pervious Area
507.0		45.51% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
10.0					Direct Entry,

Subcatchment 4S: Uncontrolled Area



Summary for Subcatchment 5S: Controlled Area - Lots 4-5

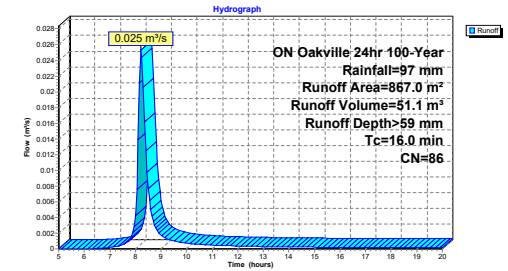
Runoff = 0.025 m³/s @ 8.22 hrs, Volume= 51.1 m³, Depth> 59 mm  
 Routed to Pond 2P : CBMH 4-5

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 100-Year Rainfall=97 mm

Area (m²)	CN	Description
307.0	98	Paved parking, HSG A
560.0	80	>75% Grass cover, Good, HSG D
867.0	86	Weighted Average
560.0		64.58% Pervious Area
307.0		35.41% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 5S: Controlled Area - Lots 4-5



Summary for Subcatchment 6S: Controlled Area - Lots 6-7

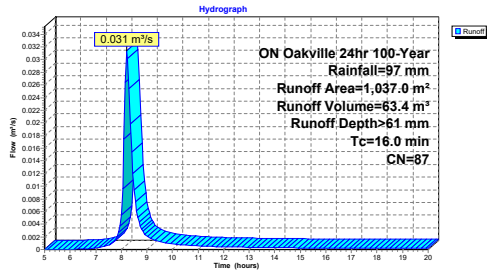
Runoff = 0.031 m³/s @ 8.22 hrs, Volume= 63.4 m³, Depth> 61 mm  
 Routed to Pond 8P : CBMH 6-7

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 ON Oakville 24hr 100-Year Rainfall=97 mm

Area (m²)	CN	Description
393.0	98	Paved parking, HSG D
644.0	80	>75% Grass cover, Good, HSG D
1,037.0	87	Weighted Average
644.0		62.10% Pervious Area
393.0		37.90% Impervious Area

Tc (min)	Length (meters)	Slope (m/m)	Velocity (m/sec)	Capacity (m³/s)	Description
16.0					Direct Entry,

Subcatchment 6S: Controlled Area - Lots 6-7



Summary for Pond 2P: CBMH 4-5

Inflow Area = 867.0 m², 35.41% Impervious, Inflow Depth > 59 mm for 100-Year event  
 Inflow = 0.025 m³/s @ 8.22 hrs, Volume= 51.1 m³  
 Outflow = 0.016 m³/s @ 8.36 hrs, Volume= 51.1 m³, Atten= 37%, Lag= 8.4 min  
 Primary = 0.016 m³/s @ 8.36 hrs, Volume= 51.1 m³  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.462 m @ 8.36 hrs Storage= 9.7 m³

Plug-Flow detention time= 6.9 min calculated for 51.1 m³ (100% of inflow)  
 Center-of-Mass det. time= 6.3 min ( 566.8 - 560.5 )

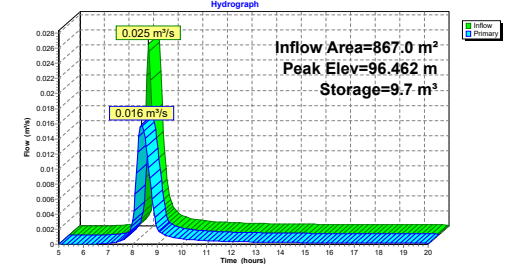
Volume	Invert	Avail Storage	Storage Description
#1	94.810 m	19.5 m³	Custom Stage Data Listed below

Elevation (meters)	Cum.Store (cubic-meters)
94.810	0.0
97.110	13.5
97.260	19.5

Device	Routing	Invert	Outlet Devices
#1	Primary	94.810 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary OutFlow Max=0.016 m³/s @ 8.36 hrs HW=96.455 m (Free Discharge)  
 ←1-Orifice/Grate (Orifice Controls 0.016 m³/s @ 3.59 m/s)

Pond 2P: CBMH 4-5



Summary for Pond 7P: CBMH 1-2-3

Inflow Area = 1,039.0 m<sup>2</sup>, 53.13% Impervious, Inflow Depth > 68 mm for 100-Year event  
 Inflow = 0.030 m<sup>3</sup>/s @ 8.27 hrs, Volume= 70.7 m<sup>3</sup>  
 Outflow = 0.019 m<sup>3</sup>/s @ 8.43 hrs, Volume= 70.7 m<sup>3</sup>, Atten= 36%, Lag= 9.8 min  
 Primary = 0.019 m<sup>3</sup>/s @ 8.43 hrs, Volume= 70.7 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 97.098 m @ 8.43 hrs Storage= 12.8 m<sup>3</sup>

Plug-Flow detention time= 6.9 min calculated for 70.5 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 6.4 min ( 562.9 - 556.5 )

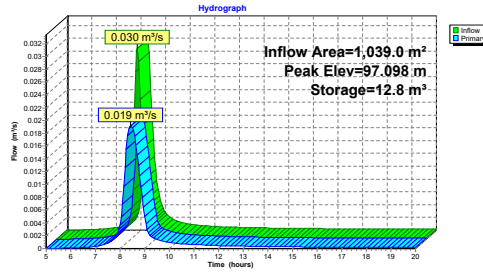
Volume	Invert	Avail. Storage	Storage Description
#1	94.740 m	15.1 m <sup>3</sup>	Custom Stage Data Listed below

Elevation (meters)	Cum. Store (cubic-meters)
94.740	0.0
96.970	11.0
97.260	15.1

Device	Routing	Invert	Outlet Devices
#1	Primary	94.740 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary Outflow Max=0.019 m<sup>3</sup>/s @ 8.43 hrs HW=97.093 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.019 m<sup>3</sup>/s @ 4.31 m/s)

Pond 7P: CBMH 1-2-3



Summary for Pond 8P: CBMH 6-7

Inflow Area = 1,037.0 m<sup>2</sup>, 37.90% Impervious, Inflow Depth > 61 mm for 100-Year event  
 Inflow = 0.031 m<sup>3</sup>/s @ 8.22 hrs, Volume= 63.4 m<sup>3</sup>  
 Outflow = 0.018 m<sup>3</sup>/s @ 8.37 hrs, Volume= 63.4 m<sup>3</sup>, Atten= 43%, Lag= 9.4 min  
 Primary = 0.018 m<sup>3</sup>/s @ 8.37 hrs, Volume= 63.4 m<sup>3</sup>  
 Routed to Link 9L : Total Outflows

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs  
 Peak Elev= 96.577 m @ 8.37 hrs Storage= 14.0 m<sup>3</sup>

Plug-Flow detention time= 8.6 min calculated for 63.4 m<sup>3</sup> (100% of inflow)  
 Center-of-Mass det. time= 7.9 min ( 566.5 - 558.6 )

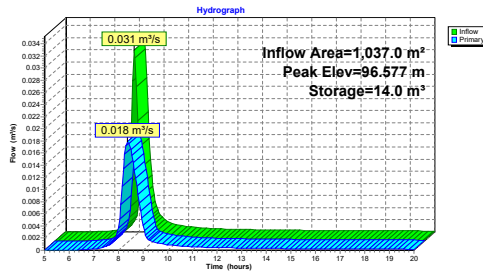
Volume	Invert	Avail. Storage	Storage Description
#1	94.500 m	14.7 m <sup>3</sup>	Custom Stage Data Listed below

Elevation (meters)	Cum. Store (cubic-meters)
94.500	0.0
96.520	13.5
96.670	14.7

Device	Routing	Invert	Outlet Devices
#1	Primary	94.500 m	75 mm Vert. Orifice/Grate C= 0.640 Limited to weir flow at low heads

Primary Outflow Max=0.018 m<sup>3</sup>/s @ 8.37 hrs HW=96.560 m (Free Discharge)  
 1=Orifice/Grate (Orifice Controls 0.018 m<sup>3</sup>/s @ 4.03 m/s)

Pond 8P: CBMH 6-7



Summary for Link 9L: Total Outflows

Inflow Area = 2,943.0 m<sup>2</sup>, 42.54% Impervious, Inflow Depth > 63 mm for 100-Year event  
 Inflow = 0.053 m<sup>3</sup>/s @ 8.38 hrs, Volume= 185.1 m<sup>3</sup>  
 Primary = 0.000 m<sup>3</sup>/s @ 5.00 hrs, Volume= 0.0 m<sup>3</sup>, Atten= 100%, Lag= 0.0 min  
 Secondary = 0.053 m<sup>3</sup>/s @ 8.38 hrs, Volume= 185.1 m<sup>3</sup>

Primary outflow = Inflow above 10.0000 m<sup>3</sup>/s, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Link 9L: Total Outflows

