

1258 Rebecca Street, Oakville

Functional Servicing Report

April 2022



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Project Number: 2480

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SUBMISSION HISTORY

Submission Date		In Support Of	Distributed To		
1 st	April 2022	Zoning By-law Amendment Application	Town of Oakville, Conservation Halton		

1.0 INTRODUCTION

SCS Consulting Group Ltd. has been retained by Halton Region to prepare a Functional Servicing Report for a proposed assisted living development located at Rebecca Street and Warminster Drive in the Town of Oakville.

1.1 Purpose of the Report

The Functional Servicing and Stormwater Management (SWM) Report has been prepared in support of a Zoning By-law Amendment (ZBA) application for the proposed development. The Site Plan is provided in **Appendix A**.

The purpose of this report is to demonstrate that the proposed development can be graded and serviced in accordance with the Town of Oakville, Halton Region, Conservation Halton, Ontario Building Code (OBC), and the Ministry of Environment, Conservation and Parks (MECP) design criteria.

1.2 Study Area

The existing site is comprised of vacant open space located within the Fourteen Mile Creek watershed in the Town of Oakville. As shown on **Figure 1.1**, the study area is bound by:

- Rebecca Street to the north;
- Patricia-Picknell Elementary School to the south;
- Single-family residential area to the east; and
- Oakville Public Library and Paramedic Services Station to the west.



Figure 1.1: Site Location Plan

The proposed development is approximately 0.66 ha in size and consists of three single detached lots fronting onto Rebecca Street and fourteen single storey semi-detached units. The semi-detached units will serve as an affordable independent living community for seniors.

Each of the proposed single detached lots will have independent access onto Rebecca Street. These lots are intended to be sold as serviced lots and will be developed by others.

The independent living community is proposed to include a private laneway with access from Rebecca Street. Pedestrian connections to the neighbouring library will also be provided. The semi-detached units will be constructed as slab-on-grade and will not have basements.

Please refer to the Site Plan in **Appendix A** to view the proposed site layout.

1.3 Background Servicing Information

In preparation of the preliminary servicing and SWM strategies, the following design guidelines and standards were used:

- Town of Oakville, Development Engineering Procedures and Guidelines Manual;
- Development Engineering Procedures and Guidelines Manual Addendum #1 (January 2017);
- North Oakville Sustainable Development Checklist & User Guide Subdivision and Site Level Design, prepared by the Town of Oakville (May 2008);
- Conservation Halton Policies and Guidelines for the Administration of Ontario Regulation 162/06 (November 2020);
- Conservation Halton Guidelines for Stormwater Management Engineering Submissions (May 2021);
- Halton Region, Water and Wastewater Linear Design Manual, version 4.0 (April 2019);
- Ministry of Environment, Conservation and Parks (MECP) Stormwater Management Planning and Design Manual (March 2003); and
- Ministry of Transportation (MTO) Drainage Management Manual (1997).

The preliminary site servicing and SWM strategies in this report are based on the following reports:

- Preliminary Geotechnical Investigation, prepared by WSP (February 2021); and
- Proposed Halton Region Paramedic Services Station No. 15 Stormwater Management Report, prepared by MGM Consulting Inc. (August 2017).

The preliminary site servicing and SWM strategies are also based on the following approved Engineering Drawings:

 Woodside Drive – Storm Drainage Area Plan No. R-358-00-03, prepared by Trafalgar Engineering Ltd., dated March 2001;

- Woodside Drive Rebecca to Sta. 0+320 No. 946P1, prepared by Trafalgar Engineering Ltd., dated March 2001;
- Rebecca Street Watermain Replacement Drawing No. PR-1452, prepared by Marshall Macklin Monaghan Ltd., dated July 1993;
- Rebecca Street –Plan & Profile Showing Proposed Storm Sewer from Third Line Road to Fourteen Mile Creek Drawing No. 2, prepared by Franklin McArthur Associates Ltd., dated February 1958; and
- Utility Investigation, prepared by R&B Locating, dated December 2020.

The above listed drawings have been included in Appendix B.

2.0 STORM SERVICING

2.1 Existing Storm Sewer System

As indicated in the utility investigation prepared by R&B Locating and the record drawings (**Appendix B**), the sizes and locations of the existing municipal storm sewers surrounding the site are:

- An 1800 mm diameter concrete storm sewer on Rebecca Street flowing northeast; and
- A 375 mm diameter PVC storm sewer on Woodside Drive flowing southeast.

The existing lands drain southwest via overland flow to the neighbouring Patricia-Picknell Elementary School grounds, where the flows are captured by a ditch inlet catchbasin and conveyed to the existing 375 mm diameter storm sewer on Woodside Drive. Please refer to **Section 3.2** for further discussion of the existing drainage.

As presented in the Town of Oakville Stormwater Management Master Plan, the existing 1800 mm diameter sewer on Rebecca Street is surcharged in the 5 year storm event to an elevation above the pipe obvert but below the manhole rim elevation. A figure showing the results of the Town's capacity assessment is included in **Appendix D**. Based on the Town's Construction Projects web page, there are no works planned in the near future to upgrade the existing storm sewer system.

The Town's SWM Master Plan identifies the existing 375 mm diameter sewer on Woodside Drive as not surcharged in the 5 year storm. This is likely based on the drainage plan prepared by Trafalgar Engineering Ltd (**Appendix B**), which accounted for 0.33 ha of drainage from 1258 Rebecca Street. However, based on the site survey, the entire site area of 0.66 ha plus 0.04 ha of external area currently drains to the Woodside Drive sewer. The Existing Woodside Drive Design Sheet is included in **Appendix D**. The analysis shows that the 375 mm diameter sewer is surcharged at 103% of the pipe capacity during the 5 year storm event under existing conditions.

2.2 Proposed Storm Sewer System

The storm sewer system (minor system) for the proposed development will be designed for the 5 year return storm per the Town of Oakville standards. The storm sewer system will be designed in accordance with the Town of Oakville, Ontario Building Code and MECP guidelines, including the following:

- Minor System Conveyance: 5 Year
- Major System Conveyance: 100 Year
- Time of Concentration: 10 minutes
- Minimum Pipe Size: 300 mm diameter
- Minimum Slope: 0.30%
- Minimum / Maximum Velocity: 0.75 m/s 4.0 m/s

Minimum Pipe Cover: 1.20 m (frost cover)

The rainfall intensity will be determined using the values from Table 3.1 of the Town of Oakville Development Engineering Procedures and Guidelines Manual dated January 2011 as shown in **Table 2.2**:

Return Period Storm	А	В	С
2 Year	725	4.8	0.808
5 Year	1170	5.8	0.843
10 Year	1400	5.8	0.848
25 Year	1680	5.6	0.851
50 Year	1960	5.8	0.861
100 Year	2150	5.7	0.861

Table 2.2 – Rainfall Intensity Parameters

The preliminary storm sewer layout is shown on **Figure 2.1**. Flows captured from the independent living community are proposed to be conveyed to the existing 375 mm diameter Woodside Drive storm sewer. The proposed storm service connection for the independent living community will be routed through the neighbouring Paramedic Services Station property, which is owned by Halton Region. The requirement for an easement through the neighbouring property will be determined at the detailed design stage. The proposed service connection will have sufficient depth to service the subject site.

Stormwater from the front yards of the three single family lots is proposed to drain via overland flow to the Rebecca Street right-of-way. Stormwater from the remaining area of the single family lots is proposed to drain via overland flow to the private storm sewer system within the independent living community and ultimately outlet to Woodside Drive. The proposed storm drainage is shown on **Figure 3.2**.

The allowable release rate to the Woodside Drive storm sewer will be 81.4 L/s based on the existing drainage conditions. As shown in the Proposed Woodside Drive Design Sheet (**Appendix D**), the proposed development will not worsen the existing surcharge conditions in the downstream sewer system. Please refer to **Section 3.3** for further discussion of the allowable release rate.

The front yards of the single-family lots will drain uncontrolled to the Rebecca Street right-ofway at a rate of 16.7 L/s in the 100 year storm. This flow corresponds to 0.3% of the existing 1800 mm diameter sewer capacity, and is only a marginal increase in flow. Therefore, the impact on the existing surcharged condition will be minimal. Please refer to the Proposed Rebecca Street Design Sheet in **Appendix D** for further details.

3.0 STORMWATER MANAGEMENT

3.1 Stormwater Runoff Control Criteria

The following stormwater runoff control criteria have been established based on the greatest requirements of each of the design guidelines and standards listed in **Section 1.3**. The stormwater runoff criteria are summarized below in **Table 3.1**.

Criteria	Control Measure		
Quantity Control	Control proposed peak flows to existing peak flows for the 2 through 100 year storm events. Where runoff is conveyed to an existing storm sewer, limit the maximum peak flow to the existing 5 year storm event peak flow (Conservation Halton).		
Quality Control	MECP Enhanced Level Protection (80% TSS Removal).		
Erosion Control	Detention/retention of the 25 mm rainfall runoff for a minimum of 24 hours. For smaller site, demonstrate that the use of pipe storage, infiltration, evapotranspiration, and on-site re-use of runoff has been applied to the extent feasible to reduce erosion potential (Conservation Halton).		
Water Budget	Replicate/maintain as closely as possible existing hydrologic conditions by maintaining a balance between infiltration, runoff and evapotranspiration and minimize negative impacts to groundwater (Conservation Halton).		

Table 3.1: Stormwater Run	off Control Criteria
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3.2 Existing Drainage

The existing lands (0.70 ha) drain southwest via overland flow to an existing ditch at the southwest corner of the site via an existing ditch system (Catchment 102 and External Catchment EXT-1 on **Figure 3.1**). Flow in the existing ditch is captured via an existing ditch inlet catchbasin (DICB) which is connected to the existing 375 mm diameter storm sewer on Woodside Drive and outlets to the Sedgewick Forest and ultimately to Lake Ontario.

3.3 Allowable Release Rate

The allowable release rate for the proposed development has been established based on controlling the proposed peak flows to existing peak flows for the 2 through 100 year storm events however, where runoff is conveyed to an existing storm sewer, the maximum peak flow is limited to the existing 5 year storm event peak flow.

As mentioned in **Section 3.2**, existing drainage from the development and external drainage area, (0.66 ha and 0.04 ha, respectively) **Figure 3.1**, drains to the existing storm sewer on



Woodside Drive. The 5 year flow from the proposed development (and external area) is 81.4 L/s.

As mention in **Section 2.2**, the Woodside Drive storm sewer system design accounted for 0.33 ha of drainage from the site, per the Woodside Drive Storm Drainage Area Plan previously completed by Trafalgar Engineering Ltd (March 2001) (refer to the excerpt in **Appendix B**). A downstream storm sewer analysis of the Woodside Drive storm sewer was completed and results in a surcharged condition.

The downstream storm sewer analysis was updated to include the existing drainage of 0.70 ha which enters the Woodside Drive storm sewer to determine the impacts. The analysis determined that the existing development will not worsen the surcharge condition within the existing Woodside Drive storm sewer as outlined within **Section 2.2**. As such, the allowable release rate is to control proposed peak flows to the existing 5 year peak flow of 81.4 L/s.

The rational method was used to determine the target release rate from the site based on Intensity-Duration-Frequency (IDF) rainfall curves from the Town of Oakville Design Standards. Supporting calculations are provided in **Appendix E**.

3.4 Stormwater Best Management Practices Selection

In accordance with the Ministry of Environment Stormwater Management Planning and Design Manual (2003), a review of stormwater management best practices was completed using a treatment train approach, which evaluated lot level, conveyance system and end-of-pipe alternatives. The potential best management practices were evaluated based on the stormwater management objectives listed in **Table 3.1**.

The following study area characteristics were taken into consideration:

- The existing site is mostly undeveloped open space with some existing paved areas;
- Based on the Geotechnical investigation, study area soils consist of 50 130 mm layers of topsoil over fill materials extending to depths of 0.8 m to 1.5m. The fill materials are overlain by native silty clay till extending to depths ranging from 1.9m to 2.6 m., which is underlain by shale bedrock;
- Within the installed site wells, groundwater was observed at depths ranging between 1.82 m to 2.77 m below existing grade; and
- The proposed site plan development is approximately 0.66 ha and consists of three single detached lots fronting onto Rebecca Street, fourteen single storey semi-detached units and a proposed laneway.

The following are examples of lot-level, conveyance and end-of-pipe controls that will be evaluated for use in the proposed development. While evaluating the following controls, cost, feasibility, groundwater and grading constraints will be taken into consideration.



Lot-Level Controls

Lot-level controls are at-source measures that reduce runoff prior to stormwater entering the conveyance system, such as:

- Increased topsoil depth;
- Roof leaders to grassed areas;
- At-source storage (i.e. rooftop or parking lot storage);
- Pervious pavements;
- Infiltration trenches/soak-away pits.

Conveyance Controls

Conveyance controls provide treatment of stormwater during the transport of runoff from individual lots to the receiving watercourse or end-of-pipe facility. Examples of conveyance controls include:

- ➡ Grassed Swales;
- Pervious pipe system.

End-of-Pipe Controls

End-of-pipe stormwater management facilities receive stormwater flows from a conveyance system (i.e., storm sewers or ditches) and provide treatment of stormwater prior to discharging flows to the receiving watercourse. Typical end-of-pipe controls include:

- ➡ Wet ponds;
- ➡ Wetlands;
- Dry ponds;
- Infiltration basins; and
- Underground storage.

A comprehensive assessment of LID practices will be provided in support of the Site Plan Application. The development consists of a private road, three single detached lots and fourteen single storey semi-detached units. It is noted that the site has high groundwater levels and the opportunity for infiltration based LIDs are limited. However, a large portion of the private road consists of permeable pavers, therefore infiltration opportunities within the permeable pavers will be explored at the Site Plan Application stage in addition to grassed swales within the single detached lots and increased topsoil depth.

At the detailed design stage, a water balance evaluation will be incorporated into the detailed stormwater management report that discusses the selection of LIDs in accordance with the Town of Oakville Engineering Design Criteria and Conservation Halton guidelines, and quantifies the proposed rainwater retention volume.



3.5 Proposed Storm Drainage

The proposed major and minor system flow patterns and drainage areas are shown on **Figure 3.2**. As illustrated, runoff from the proposed development will be conveyed to the existing Woodside Drive storm sewer. Major and minor system flows from the front portion of the proposed lots on Rebecca Street (Catchment 203, **Figure 3.2**) will drain uncontrolled to Rebecca Street. Major and minor system flows from the rear portion of the proposed lots on Rebecca Street (Catchment 202, **Figure 3.2**) will drain uncontrolled to the private road storm sewer system. Drainage from the remainder of the proposed development (Catchment 201, **Figure 3.2**) will be captured via a proposed internal storm sewer system which will connect to the existing Woodside Drive sewer system.

3.5.1 Quantity Control

Quantity control for the proposed development will be required to control proposed runoff back to the allowable release rates to the Woodside Drive storm sewer. The allowable release rate for the proposed development, as identified in **Section 3.3**, is to be achieved by utilizing an orifice plate and providing on-site storage of stormwater. Preliminary calculations have been completed and require approximately 176 m³ of storage, refer to calculations in **Appendix E**. This can be achieved through underground storage in the form of an oversized super pipe, 1.5 m x 1.2 m box culvert. Details will be provided at the Site Plan application stage.

3.5.2 Quality Control

Quality control for the proposed development will be required to be provided on-site. This will be achieved through a combination of on-site LID's and a manufactured treatment device.

Quality control for runoff from the proposed development, Catchments 201 and 202 (**Figure 3.2**) will be provided by a treatment train of Best Management (BMP) techniques which could include additional topsoil depth on all grassed areas, permeable pavers, and grassed swale with an end-of-pipe manufactured treatment device, i.e. Jellyfish Unit JF4-2-1 model or approved equivalent. The manufactured treatment device has been sized to achieve Enhanced level quality control (80% TSS removal) as requested by the Town of Oakville (correspondence provided in **Appendix B**).

3.5.3 Erosion Control

As mentioned within **Section 3.1**, detention/retention of the 25 mm rainfall runoff for a minimum of 24 hours is required. However, for smaller sites, demonstrate that the use of pipe storage, infiltration, and evapotranspiration, and on-site re-use of runoff has been applied to the extent feasible to reduce erosion potential. As the proposed site is 0.66 ha, detention/retention of the 25 mm storm event would be challenging. Every extent possible to detain/retain the 25 mm storm event will be investigated and detailed at the site plan application stage via on-site storage within the proposed superpipe and infiltration within the permeable pavers.



3.5.4 Water Balance

Where feasible, measures to minimize impacts on the water budget will be incorporated into the proposed development design.

As noted in **Section 2.1**, the minimum criteria is to maintain existing hydrology function. Proposed BMP's will be fully explored at site plan application stage and a water balance will be completed to determine the existing, proposed and proposed with mitigation infiltration values. As mentioned within **Section 3.4**, potential preliminary BMP's include infiltration within the permeable pavers, increased topsoil depth and grassed swales.

4.0 SANITARY SERVICING

4.1 Existing Sanitary Sewer System

As indicated in the utility investigation prepared by R&B Locating (**Appendix B**), the sizes and locations of the existing sanitary sewers surrounding the site are:

- A 525 mm diameter vitrified clay sanitary sewer on Rebecca Street flowing northeast;
- A 1350 mm diameter concrete sanitary sewer on Woodside Drive flowing south; and
- A 200 mm diameter PVC sanitary sewer on Woodside Drive flowing south.

The subject site previously had a church building which has now been demolished, but was serviced from the existing 525 mm diameter sewer on Rebecca Street, as shown in the record drawings. Based on the Town of Oakville design criteria, the church would have generated a peak flow of approximately 0.48 L/s. The sanitary flow calculations are included in **Appendix F**.

4.2 Proposed Sanitary Sewer System

The proposed sanitary sewer system for the subject development is illustrated on **Figure 2.1**. The independent living community is proposed to be serviced from the existing 525 mm sanitary sewer on Rebecca Street via a new control manhole at the property line. The three single family lots will also be provided with individual service connections to the 525 mm sanitary sewer per Halton Region standards. The proposed service connections will have approximately 2.5 m of cover at the property line, which is sufficient to service the development.

The sanitary sewers within the site will have slopes ranging between 0.5% and 2% (typically) and will be provided at 2.5 m to 1.5 m deep. The sanitary sewer system will be designed in accordance with the Halton Region and MECP criteria, including but not limited to:

- Residential Sanitary Generation Rate: 275 L/cap/day
- Residential Population Density:
 - 55 persons/ha (Single-family)
 - 100 persons/ha (Semi-detached)
- Peaking Factor: Modified Harmon's Equation (Min = 2.0)
- Infiltration Rate: 0.286 L/s/ha
- Minimum Pipe Size: 200 mm diameter
- Minimum Velocity: 0.6 m/s
- Maximum Velocity: 3.0 m/s

Based on the design criteria, the proposed site is expected to generate a flow of 0.96 L/s. The net increase in sanitary flow from the development is 0.47 L/s. This increase in flow corresponds to 0.2% of the existing 525 mm sewer capacity. The proposed flow rate is only marginally higher than the existing condition, and therefore the impact on the existing downstream system will be minimal.

Please refer to the sanitary flow calculations in **Appendix F** for further details.

5.0 WATER SUPPLY AND DISTRIBUTION

5.1 Existing Water Distribution

As indicated in the record drawings (**Appendix B**), the following existing watermains surround the site:

- A 600 mm diameter concrete watermain on the northwest side of Rebecca Street;
- A 150 mm diameter PVC watermain on the southeast side of Rebecca Street; and
- A 150 mm diameter watermain on the west side of Woodside Drive.

There are existing hydrants located on Rebecca Street approximately 20 m west and 63 m northeast of the subject site. A hydrant flow test will be completed in the spring in order to confirm the available flow and pressure in the existing water distribution system.

5.2 Proposed Water System

The subject development is proposed to be serviced from the existing 150 mm watermain on the southeast side of Rebecca Street. The three single family lots will be provided with individual service connections and water meters per Halton Region standards. The independent living community will be provided with a private water distribution system, with individual meters for each unit. The preliminary watermain layout is shown on **Figure 2.1**.

The proposed private water distribution system will be designed in accordance with Halton Region and MECP criteria, including but not limited to the following:

- Average Daily Demand: 0.275 m³ per capita
 - Residential Population Density:
 - 100 persons/ha (semi-detached)
 - 55 persons/ha (single family)
- ➡ Peaking Factors:
 - Maximum Day = 2.25
 - Maximum Hour = 4.00
- Minimum Pipe Size: 150 mm diameter
- Minimum Pipe Cover: 1.70 m
- Maximum Hydrant Spacing: 150 m (Residential)

Water demand and Fire Underwriters Survey (FUS) calculations can be found in **Appendix G**. The demands for each scenario analysed can be found in **Table 5.1** below. The available pressures in the existing system will be confirmed by hydrant flow test in the spring.



Table 5.1: Water Demands and	l Required	Pressure	Ranges
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Scenario	Water Demand	Required Pressure Range	
Average Day	0.18 L/s	350 – 550 kPa (Preferred)	
Maximum Day	0.40 L/s	275 – 700 kPa (Required)	
Maximum Hour	0.71 L/s		
Fire Flow	6,000 L/min	≥ 140 kPa	
Fire Flow + Maximum Day	6,024 L/min		

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6.0 GRADING

6.1 Existing Grading Conditions

The existing site is relatively flat, with slopes ranging from 1.0 - 3.0% on average. There is an existing ditch in the southeast section of the site which drains south to the existing Patricia-Picknell Elementary School grounds. The ground surface elevations range from 88.90 in the northwest corner of the site to 87.75 in the south corner of the site.

6.2 Proposed Grading Concept

In general, the proposed development has been graded in a manner which satisfies the Town of Oakville lot and road grading criteria, creates the required depth for the sanitary sewer, as well as provision of an efficient earthworks program, including:

- Minimum Road Grade: 0.7%
- Maximum Road Grade: 6.0%
- Minimum Lot Grade: 2%
- Maximum Lot Grade: 5%
- Minimum Driveway Grade: 2%
- Maximum Driveway Grade: 8%
- Minimize the need for retaining walls
- Minimize the volume of earth to be moved and minimize cut/fill differentials
- Minimize the need for rear lot catchbasins
- Achieve the stormwater management objectives required for the proposed development.

A preliminary grading plan is provided on **Figure 6.1**. Details will be provided at the and site plan application stage.

At the detailed design stage, the preliminary grading shown on **Figure 6.1** will be subject to a more in-depth analysis in an attempt to balance the cut and fill volumes and minimize slopes and retaining walls.

7.0 EROSION AND SEDIMENT CONTROL DURING CONSTRUCTION

Erosion and sediment control measures will be designed at the detailed design stage. These measures may include temporary sediment control fencing, a construction access driveway, check dams and temporary sediment control facilities where required. These measures will be designed and constructed as per the "Erosion and Sediment Control Guide for Urban Construction" document (TRCA, 2019).

The detailed erosion and sediment control plan will be approved by the Town of Oakville prior to any site alteration being undertaken. The plan will address phasing, inspection and monitoring aspects of erosion and sediment control. All reasonable measures will be taken to ensure sediment loading to the adjacent properties and storm sewers is minimized both during and following construction.

8.0 SUMMARY

This Functional Servicing Report has outlined the means by which:

- The proposed development can be serviced from the existing municipal services (i.e. storm, sanitary and water) within the Rebecca Street and Woodside Drive rights-of way;
- The stormwater management criteria can be achieved; and
- The proposed development can be graded in a manner which satisfies the Town of Oakville grading criteria and the stormwater management requirements for this development.

Respectfully Submitted:

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	PROPERTY BOUNDARY
	PROPOSED STORM SEWER / MANHOLE
۲	PROPOSED JELLYFISH TREATMENT UNIT
	PROPOSED 1200x1500 BOX CULVERT
	PROPOSED SANITARY SEWER / MANHOLE
	PROPOSED WATERMAIN
+	PROPOSED HYDRANT
• • • • • • • • • • • • • • • • • • •	EXISTING STORM SEWER / MANHOLE
	EXISTING SANITARY SEWER / MANHOLE
0	EXISTING WATERMAIN / CHAMBER
÷	EXISTING HYDRANT
	PERMEABLE PAVER
*ΝΩΤΕ· Ι ΔΥΩΙΙΤ Ις SCHEMATIC ΩΝΙ	Υ DETAILS TO BE
PROVIDED AT DETAILED DESIGN ST	AGE.
SCS group ltd	D CENTURIAN DRIVE, SUITE 100 ARKHAM, ONTARIO L3R 8B8 EL: (905) 475-1900 AX: (905) 475-8335
HALTON	REGION
1258 REBEC OAK	CCA STREET, VILLE
PRELIMINARY S	ERVICING PLAN
DESIGNED BY: M.L.M.	CHECKED BY: P.G.
SCALE: 1:750	DATE: APRIL 2022
PROJECT No:	FIGURE No:
2480	2.1



LEGEND:					
////	PROPERTY BOUNDARY				
	STORM DRAINAGE BOUNDARY				
	EXTERNAL STORM DRAINAGE BOUNDARY				
0.66ha	DRAINAGE AREA (HECTARES)				
	RUNOFF COEFFICIENT				
	CATCHMENT ID				
	MAJOR SYSTEM FLOW				
255:50	EXISTING CONTOUR				
0	EXISTING STORM SEWER AND MANHOLE				
	EXTERNAL STORM DRAINAGE				
EXT-1 0 43	- RUNOFF COEFFICIENT				
	— CATCHMENT ID				
	DRAINAGE AREA ACCOUNTED FOR WITHIN WOODSIDE DRIVE SEWER PER MUNICIPAL DRAWING NO. R-358-00-03 PREPARED BY TRAFALGAR ENGINEERING LTD.				
	30 CENTURIAN DRIVE, SUITE 100				
SCS consulting aroup Itd	TEL: (905) 475-1900				
HALTON REGION					
OAKVILLE					
EX STORM DF	ISTING RAINAGE PLAN				
DESIGNED BY: R.P.B.	CHECKED BY: P.A.T.				
SCALE: 1:750	DATE: APRIL 2022				
PROJECT No:	FIGURE No:				

3.1

2480



LEGEND:





SCALE:

PROJECT No:

LEGEND:



1:750

2480

DATE:

FIGURE No:

APRIL 2022

6.1

APPENDIX A

SITE PLAN





DESIGNED	UMG
REVIEWED	UMG
DATE	2022.02.31

APPENDIX B

RECORD DRAWINGS AND BACKGROUND INFORMATION



) į N 0=16. V=5.1 DRIV -- N WAR,MINSTER M 202 84 PLAN | No. 653 REG'¦D 88 87 86 83 5 90 89 85 84 4 S 0 C C ш Ω ш 8 24" PIPE LOWERED 1'-6" - C. B. C. .. SWATER MA - R W 10" V.T. SAN. SEWER O'V.T. SAN SEWER 632' of 72" CON. PIPE 978' of 72" CON PIPE ┟┈╴╸┝┥ ---------_____ £_____ _ _ _ -----__**__** MI 4 Ace 1 60.0 A C. B. Lc.0. MHL3 _____ BTCO.___ ------- B.T.C. 0. ----O B.T.CO. OBT CO H.EPC 0 8.7.0 0 OB.TCO. O HEP.C. OHERC. Q H. EPC. O HE.PC WOODSIDE DRIVE 1338 1332 1326 1320 1314 1308 CHURCH OF ENGLAND TWP. OF TRAFALGAR JOHN P. BURTON FIRE DEPT. (FUTURE TWP. LIBRARY) 13 5 14 15 17 18 16 19 REG'D ALAN NO. 669 --------..... 4 ------ \triangleleft 3 2957 W _____ -----APPROX. LINE OF ROCK ╺╾╡╶╌╴╼╸╏╫╋╼╍╍╍┼╾╸╶╾╴╺╼╼╍╌╌┿╴ ----_____ ↓ [. -----Ψ _____ 978' OT 72" CON PIPE C76-57T CL. III C 0.20% GRADE Q=209.0 V=8.0 632' OF 72" CON. PIPE C75-571 CL. III CO.20% GRADE Q=220.5 C.F.S. V=8.0 ÷..... N. M.Y. 20250 INV: 27659 10'SAN. MY 280.40 21'SAN. MY 280.03 21'SAN. MY 283.23 2.4 5 8 --------------. ġ. -------------------. 22 72 -----...... · . · · · · · · · · · · -----····· -----.... 1. A mark 1. A - --- ---s. 1111 s.e. as . di in mari a -----2.0 . . 1.62 51.61.81 s -- ----····· _____ -----------..... · · · · · 2222 bit 92 1010 0 0 50% • 291,8 . 10 291.9 295.3 -----292. 20 _____ - **6** , N 293 292 295 293 294. 293 - * 293 293 962 -----____ 0 0 120 80+91 81+91 18 00 21+50 0 ě 224 231 2 5 Ī ā y . S. 36 and a second

	R	OSEN N	IORRIS	-1	e a		ROS	EN MORF	7/ <i>S</i>	
1										
	W 	EWER		563' ar 7		WATER MAIN 21" V.T. SAN SEN	W			
R SER IOVE	VICE FOR CHURC 72" PIPE.	О В.Т.СО. СН	44		0 8.1.00.	s ' 1	17 ¹ .6 ⁴	O BTCO. Fil		B.T. CO.
			26	R E G'	27 D P L		28 10. 709	, 	ANDWELL DRIVE	29
		1				• •	1	•		
									₹ 291.6	- - 3 00
										290 APPROX.LINE GOF ROCK 280
3' 0	<u>f 72" CON.</u>	PIPE C 76	57T CL.	C 0.20% G	RADE Q=	227.2 C.F.S.	¥=8.0		72" INV 275 46 - 8	270
							REYISED A	S CONSTR	ACTED. 440	UST 23, 1960
				3 3 3 3 3	13+50 28 \$.12+00 2 8 1.1	533' C 0.30%	¢.,165 00+11	10+55 10+55 10+45 10+45	FINISHED ROAD GRADE EXIST. GROUND ELEV. CHAINAGE
	14+50 291.5	L 14+00 291.6	5 - F	-13+00 -13+00 -13+00 -13+00			TOW PLAN STORN SCALES: VERT HOR 2	N SHIP REBECC & PROFIL SEWER F TO FOURTE TO FOURTE	DF TRA	FALGAR EET PROPOSED LINE ROAD REEK
	5	TWP	FILE	S-32			CHECKED S. A FRANI TORON TO PROJ. NO	e. KLIN M ^{CA} CONSULTIN 0. 57 - 1	DESIGNED RTHUR A IMITED IG ENGINER	S. Rodovalovi & P.E. SSOCIATES ERS CH 1-1948



ASPHALI FARKING	EAST STREET LINE WEST LINE WEST LINE WEST LINE		H	Image: State of the state
40.0m				ALL BENCH MARK INFORMATION DERIVED FROM TOWN OF OAKVILLE BENCHMARK #36 HAVING AN ELEVATION OF 94.369
• 2.30%			90	3 MAR/27/01 SP/dk SANITARY LATERAL LOWERED 2 FEB/23/01 SP/dk REVISED PER TOWN/REGION COMMENTS
			89	1 JAN/16/01 SP/dk REVISED PER TOWN/REGION COMMENTS No Date By/DRN REVISIONS Design DB Chk'd SP Cad File 946P1 Drawn DK Chk'd SP Plot MAP / 29 / 01
	320		88	Scale Date MAR/29/01 HOR 5 10 15 20 25 VER 0 0.5 1 1.5 2 2.5 1:500 1:500 1:500 1:500 1:500
	+ o ≰		87	APPROVALS Municipal APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF OAKVING STANDARDS AND SPECIFICATIONS. Bell Hydro X
			86	R.G.GREEN, Director of Public Works
	- HCH		85	DESIGN OF WASTEWATER & WATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY
	Σ		84	Signed: Jul Lun Date: March 30, 2001 To have been to the second sec
			83	Consultant TRAFALGAR ENGINEERING LTD. 481 MORDEN ROAD OAKVILLE, ONTARIO L6K 3W6 TEL: (905) 338-3366 FAX: (905) 338-7734
mø PVC SAN Ø 1.85% NG PER OPSD 802.010]			82	Municipality TOWNOF
nø PVC STM ● 0.70% G PER OPSD 802.010		SANITAF	۲Y	
SAN MI SAN MI 001.0 83.1 83.1 83.1		SEWER	R S	Title WOODSIDE DRIVE
STM MF STM MF 2000 N 83.7 83.7		SEWER	R S	RECONSTRUCTION WOODSIDE DRIVE
86.64 86.18		ROAD/DI CENTERL	TCH INE	KEBECCA TO STA 0+320
0+300		STATIO	N	R-358-00-06 Contract No. Consultant Drawing No. 946P1 R-358-00 Consultant Drawing No. 946P1
				N-000Sheet1 of 2Regional File No.DO-375



NORTH 02200 02200 0.288 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40	REBECÇA ST REBECÇA ST UNESNORE RD NOR L A K E O N T A R I O KEY PLAN
CONC OF CONC OF CON	N DAK FENCE
ПV 83.60 1.5m CONC SW 300mm Cu CPT 67.0m-60000mm SIM 0 0.702 CB CB C 10 CB	22/0m - 675mm# STM \odot 0.6% LOT 4 52.5m - 300mm PVC 52.5m - 0.30% 510 - 0.00% 510 -
CHAIN LINK FENCE LOT 51	NOTE FOR GENERAL NOTES AND DETAILS REFER TO DWG 946D1 BENCHMARK ALL BENCH MARK INFORMATION DERIVED FROM TOWN OF OAKVILLE BENCHMARK #36 HAVING AN ELEVATION OF 94.369
IRAFALGAR EINGINEERING LID. 481 MORDEN ROAD OAKVILLE, ONTARIO L6K 3W6 TEL: (905) 338-3366 FAX: (905) 338-7734 trafalgareng@globalserve.net	RECONSTRUCTION STORM DRAINAGE AREA PLAN
REGIONAL MUNICIPALITY OF HALTON	R-358-00-03 Contract No. R-358-00 Sheet 1 of 1 Regional File No.
	00-375



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					-10,0m @ 0.00°	%
50 % s			90.0 m d) 0.20 %	86.2	₹	dD 1.00 % -▶
+++++++++++++++++++++++++++++++++++++++	1+180	1+202.5 1+202.5 1+211.0 1+220	1+260	1+280 1+280 1+294.5	1+300 1+313.0 1+318.5 1+320	0.155+1

	WATER SERVICE FOR 305 & 30 COME OFF WENDY LANE				
1209	SE 2-45 ° COMBO TO EX. 150 mm WATERMAIN	Leosa - Soc	KEY PI	REBECCA WILLOW REBECCA WILLOW REBECCA WILLOW REBECCA WILLOW REBECCA WILLOW REBECCA WILLOW REBECCA WILLOW REBECCA	HUNG CRUE CRUE CRUE CRUE CRUE CRUE CRUE CRUE
RE VAI EX 220 Mm SAA EX 1300 Mm STM. BH 6. BH 6. BH 6. BH 6. CB	MOVE EX. BOX BOX BOX BOX BOX BOX BOX BOX	ELL MIH EELL MIH EELL MIH EELL MIH EELL MIH EX. 150 inm WM. H BASELINE PROPOSED BASELINE HAV O HAV O HAV	ITEM 22.5° HORIZ. BEND 22.5° HORIZ. BEND HYDRANT & VALVE VALVE CHAMBER No.5 VALVE CHAMBER No.6 HYDRANT & VALVE 22.5° HORIZ. BEND 22.5° HORIZ. BEND 22.5° HORIZ. BEND 22.5° HORIZ. BEND	WATERMAIN DAT STATION CONSTR. OFFSET STD. DWG. INV EL 1+065.0 10.5 RT 86.7 1+068.0 9.5 RT 86.7 1+158.0 7.0 RT 1105.01 86.7 1+202.5 9.5 RT W-2 86.7 1+294.5 9.5 RT W-2 86.7 1+313.0 7.0 RT 1105.01 86.7 1+318.5 7.0 RT 86.7 86.7 1+338.0 10.5 RT 85.7 85.7	A ERT REMARKS '90
		THOMAS A. BLAKELOCK HIGH SCHOOL			
SANDWELL DRIVE.				FOR GENERAL NOTES AND I SEE DRAWING No.1	BENCHMARKS
H#6 2 TOPSOLL SANDY SILT (FILL) X. 150 mm WM.	Image: Construction Image: Construction Imag	Image: Second state 22.5° HORIZONTAL BEN Image: Second state 22.5° HORIZONTAL BEN	88	02/03/97 JAC AS CONSTR 11/19/96 WGN AS CONSTR NQ Date By Design J.S. Ch'kd Drawn R.M.M. Ch'kd Scale 10 5 0 Vert. 10 5 0 Municipal APHRSVASUE Municipal	UCTED UCTED UCTED REVISIONS T.R. Date JULY 1993 10 References 10 Field Notes
SILTY_CLAY (THE)		EX. 525 mm SAN. SEWER		MAR 2 8 1995 HALTON REGIO PUBLIC WORKS Regional Commissioner of Public Wo Director of Design & Constr UNION Marshall Mac Limited Thornhill Consulting Engineers	REGION BOOK # 497 & 498 Starner of Ession Profession J. SFRAMELI J. SFRAMELI J. SFRAMELI J. SFRAMELI Starner J. SFRAMELI J. SFRAMELI
MAIN BACKFILL)2-02			EXISTING Q ELEVATIONS	TITLE WATERN REBECCA	AIN REPLACEMENT STREET
90.0 m aD 0.20 %		ھ 0.00 % −80.0m dD 1.00 % -	WATERMAIN	TOWN OF FROM 30m E. OF WAR 50m E. OF WEN	OAKVILLE MINSTER DRIVE TO NDY LANE
1+240	1+280 1+294.5 1+300 86	14313.0 14313.0 1+318.5 1+338.0 1+331.0 1+338 1+340 85	INVERTS CHAINAGE	10-93022 CONTRACT Nº W-1452-95	O- 9397 Drawing № PR-1452 SHEET 5 OF 14





APPENDIX C

TOPOGRAPHIC SURVEY





APPENDIX D

STORM SERVICING CALCULATIONS

SCS consulting group Itd Rainfall Intensity (i) = Starting T _c (min)=	A (T _c +B) ^c = 10	_	A= B= c=	= 1170 = 5.8 = 0.843		5-Year St T	torm Desig Independ 1258 own of Oa = Includes 0 remaining 1	gn - Exist lent Livir Rebecca Ikville, Ha 0.33 ha from 258 Rebecca	ing Wood ng Facility Street alton Reg Woodside D St Site Area	dside Driv y gion rive Drainag a and 0.04 ha	' e e Plan, 0.33 h External Dr.	a of ainage			F	Project Project No Date Designed By Reviewed By:	: Independen . 2480 : 11-Apr-22 : M.L.M. P.G.	ıt Living Faci	ility	
LOCATION					5 1	EAD				EVTEDN			TOTAL FLOW	P:\2480 1258 Rebe	xca Street Oakville - I	Halton Region\Design\]	Pipe Design\Storm\[24	80-POST Dev-Storm D	esign Sheet-Rebecca	Street.xlsm]Design
	MAINTEN	ANCE HOLE			51	EAK				EATERN	AL FLOWS		IUIAL FLOW			FIFE DATA	`		-	ACCUM
STREET			5-YEAR AREA	RUNOFF COEFF.	"AR"	ACCUM. "AR"	RAINFALL INTENSITY	ACCUM. FLOW	AREA	FLOW RATE	EXT. FLOW	ACCUM. EXT. FLOW	TOTAL (Qdes)	LENGTH	SLOPE	PIPE DIAMETER	FULL FLOW CAPACITY	FULL FLOW	TIME OF CONC.	TIME
	FROM	то	(ha)	(R)			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	(min)
PATRICIA-PICKNELL SCHOOL GROUNDS	EX.DICB1	EX.MH5	0.70	0.37	0.26	0.26	114.21	0.081	0.000	0.000	0.000	0.000	0.081	13.0	2.00	300	0.137	1.935	0.11	10.11
WOODSIDE DRIVE	EX.MH5	EX.MH4	0.71	0.70	0.50	0.75	113.54	0.238	0.000	0.000	0.000	0.000	0.238	60.0	1.75	375	0.232	2.100	0.48	10.59
WOODSIDE DRIVE	EX.PLUG	EX.MH4	1.02	0.60	0.61	0.61	114.21	0.194	0.000	0.000	0.000	0.000	0.194	10.5	2.00	450	0.403	2.535	0.07	10.07
			1.10	0.40	0.44	1.01	110.75	0.555	0.000	0.000	0.000	0.000	0.555	(0.0	0.75	(00	0.521	1.001	0.(1	11.20
WOODSIDE DRIVE	EX.MH4	EX.MH3	1.10	0.40	0.44	1.81	110.75	0.555	0.000	0.000	0.000	0.000	0.555	69.0	0.75	600	0.531	1.881	0.61	11.20
woodside drive	EX.MH3	EA.MH2	0.37	0.40	0.15	1.95	107.38	0.583	0.000	0.000	0.000	0.000	0.583	67.0	0.70	600	0.513	1.81/	0.61	11.81
SEDGEWICK DRIVE	EX.DICB2	EX.CBMH6	0.47	0.35	0.16	0.16	114.21	0.052	0.000	0.000	0.000	0.000	0.052	7.5	1.00	250	0.059	1.211	0.10	10.10
SEDGEWICK DRIVE	EX.CBMH6	EX.MH2	0.11	0.40	0.04	0.21	113.59	0.066	0.000	0.000	0.000	0.000	0.066	52.5	0.30	300	0.053	0.749	1.17	11.27
																			1	
SEDGEWICK DRIVE	EX.MH2	EX.MH1	1.21	0.40	0.48	2.65	104.21	0.766	0.000	0.000	0.000	0.000	0.766	22.0	0.60	675	0.651	1.820	0.20	12.02
SEDGEWICK FOREST OUTFALL	EX.MH1	EX.HW	0.28	0.40	0.11	2.76	103.22	0.791	0.000	0.000	0.000	0.000	0.791	4.0	0.60	675	0.651	1.820	0.04	12.05

SCS consulting group Itd Rainfall Intensity (i) =	$=$ <u>A</u> $(T_c+B)^c$	_	A= B= c=	1170 5.8 0.843	5	5-Year Sto T	orm Desig Independ 1258 own of Oa = Includes 1	gn - Propo dent Livir Rebecca akville, H 258 Rebecca	osed Woo ng Facility Street alton Reg 1 St and 0.04	dside Dri y gion ha External	ve Drainage Ar	ea				Project Project No Date Designed By	: Independen . 2480 : 11-Apr-22 : M.L.M.	1t Living Faci	ility	
Starting T _c (min)=	= 10						= Allowable	Release Rat	e						I	Reviewed By:	P.G.			
					5 V	T A D			I	EVTEDN			TOTAL FLOW	P:\2480 1258 Reb	ecca Street Oakville -	Halton Region\Design\	Pipe Design\Storm\[24	80-POST Dev-Storm D	esign Sheet-Rebecca	Street.xlsm]Desig
LOCATION					51	EAR				EATERN	AL FLOWS		TOTAL FLOW			PIPE DATA	•		4	
CTREET	MAINTEN	ANCE HOLE	5-YEAR AREA	RUNOFF COEFF	"AR"	ACCUM.	RAINFALL	ACCUM. FLOW	AREA	FLOW RATE	EXT. FLOW	ACCUM. EXT_FLOW	TOTAL (Odes)	LENGTH	SLOPE	PIPE DIAMETER	FULL FLOW	7 FULL FLOW	TIME OF	ACCUM. TIME
SIREEI	FROM	то									(21)		((2005)	<i>(</i>)						OF CONC.
			(ha)	(R)			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	(min)
1258 REBECCA STREET	MH1	EX.MH5	0.00	0.00	0.00	0.00	114.21	0.000	0.70	116.29	0.081	0.081	0.081	15.0	0.50	375	0.124	1.123	0.22	10.22
WOODSIDE DRIVE	EX.MH5	EX.MH4	0.71	0.70	0.50	0.50	112.87	0.156	0.00	0.00	0.000	0.081	0.237	60.0	1.75	375	0.232	2.100	0.48	10.70
WOODSIDE DRIVE	EX.PLUG	EX.MH4	1.02	0.60	0.61	0.61	114.21	0.194	0.00	0.00	0.000	0.000	0.194	10.5	2.00	450	0.403	2.535	0.07	10.07
WOODSIDE DRIVE	EX.MH4	EX.MH3	1.10	0.40	0.44	1.55	110.12	0.474	0.00	0.00	0.000	0.081	0.555	69.0	0.75	600	0.531	1.881	0.61	11.31
WOODSIDE DRIVE	EX.MH3	EX.MH2	0.37	0.40	0.15	1.70	106.79	0.503	0.00	0.00	0.000	0.081	0.585	67.0	0.70	600	0.513	1.817	0.61	11.92
																			1	
SEDGEWICK DRIVE	EX.DICB2	EX.CBMH6	0.47	0.35	0.16	0.16	114.21	0.052	0.00	0.00	0.000	0.000	0.052	7.5	1.00	250	0.059	1.211	0.10	10.10
SEDGEWICK DRIVE	EX.CBMH6	EX.MH2	0.11	0.40	0.04	0.21	113.59	0.066	0.00	0.00	0.000	0.000	0.066	52.5	0.30	300	0.053	0.749	1.17	11.27
																				<u> </u>
SEDGEWICK DRIVE	EX.MH2	EX.MH1	1.21	0.40	0.48	2.39	103.66	0.688	0.00	0.00	0.000	0.081	0.769	22.0	0.60	675	0.651	1.820	0.20	12.13
SEDGEWICK FOREST OUTFALL	EX.MH1	EX.HW	0.28	0.40	0.11	2.50	102.68	0.713	0.00	0.00	0.000	0.081	0.795	4.0	0.60	675	0.651	1.820	0.04	12.16

100-Year Storm Design - Proposed Rebecca Street Independent Living Facility 1258 Rebecca Street Town of Oakville, Halton Region

Rainfall Intensity (i) =	Α		A=	2150					Project No. 2480											
	$(T_c+B)^c$		B=	5.7					Date: 11-Apr-22											
			c=	0.861			Designed By: M.L.M.													
Starting T _c (min)=	10					Reviewed By: P.G.														
														P:\2480 1258	Rebecca Street Oakvi	lle - Halton Region\Desi	gn\Pipe Design\Storm\[24	480-POST Dev-Storm E	esign Sheet-Rebecc	a Street.xlsm]Design
LOCATION					100 Y	EAR				EXTERNA	AL FLOWS		TOTAL FLOW			PIPE DATA				
STREET	MAN	HOLE	100-YEAR AREA	RUNOFF COEFF.	"AR"	ACCUM. "AR"	RAINFALL INTENSITY	ACCUM. FLOW	AREA	FLOW RATE	EXT. FLOW	ACCUM. EXT. FLOW	TOTAL (Odes)	LENGTH	SLOPE	PIPE DIAMETER	FULL FLOW CAPACITY	FULL FLOW VELOCITY	TIME OF CONC.	ACCUM. TIME
SINEL	FROM	то	(ha)	"R"			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	OF CONC. (min)
REBECCA STREET	EX.MH3	EX.MH2	0.05	0.60	0.030	0.030	200.80	0.017	0.000	0.000	0.000	0.000	0.017	171.6	0.20	1800	5.138	2.020	1.42	11.42

Project: Independent Living Facility

APPENDIX E

STORMWATER MANAGEMENT CALCULATIONS

ALLOWABLE RELEASE RATE AREA ACCOUNTED FOR IN WOODSIDE DRIVE SEWER

5	Year	storm
_		

IDF Parameters*	a = 1170 t = 10 b = 5.8 c = 0.843	min
IDF Parameters*	t = 10 b = 5.8 c = 0.843	min

C1 = 0.40

Runoff Coefficient:

Allowable Release Rate Calculation												
Outlet	Area	time	Intensity	Flow								
ID t i=a/(t+b)^c Q=CiA/360												
	ha min mm/hr l/s											
Woodside Drive	0.33	10.00	114.21	42.4								
* a,b,c's per Town of Oakville												

As identified on the Woodside Drive Reconstruction Storm Drainage Area Plan prepared by Trafalgar Engineering Ltd. dated March 2001 (refer to **Appendix B**), approximately 0.33 ha of the existing site has been accounted for within the Woodside Drive storm sewer system.

ALLOWABLE RELEASE RATE **EXISTING DRAINAGE TO** WOODSIDE DRIVE SEWER

<u>5 Year st</u>	orm
------------------	-----

IDF Parameters*	a = 1170 t = 10 b = 5.8 c = 0.843	min
Runoff Coefficient:	C1 = 0.37	

Runoff Coefficient:

Allowable Release Rate Calculation											
Outlet	Area	time	Intensity	Flow							
ID t i=a/(t+b)^c Q=CiA/360											
	ha	min	mm/hr	l/s							
Woodside Drive	0.70	10.00	114.21	81.41							
	* a b c's per Town of Oakville										

Although the Woodside Drive sewer was initially designed to accommodate an area of 0.33 ha with a runoff coefficient of 0.40, in the existing condition approximately 0.70 ha with a runoff coefficient of 0.37 drains into the Woodside Drive sewer. An updated storm sewer analysis was completed and determined that runoff from existing development will not increase the surcharge within the existing Woodside Drive sewer. Therefore, the allowable release rate to the Woodside Drive storm sewer is 81.41 L/s.

PROPOSED WEIGHTED RUNOFF COEFFICIENT

Catchment	201	Outlets to:	Woodside Drive	
	Runoff Coefficient	Area (ha)	Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Asphalt	0.90	0.10	0.21	0.24
Rooftops	0.90	0.09	0.18	0.20
Permeable Pavement	0.55	0.12	0.15	0.18
Grass	0.25	0.13	0.07	0.09
TOTAL		0.44	0.62	0.71
Catchment	202	Outlets to:	Woodside Drive	
	Runoff Coefficient	Area (ha)	Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Future Residential Development	0.60	0.17	0.60	0.75
TOTAL		0.17	0.60	0.75
Catchment	EXT-1	Outlets to:	Woodside Drive	
	Runoff	• (1)	Coefficient	Weighted Runoff
Aanhalt		Area (na)	0.07	
Asphalt	0.90	0.003	0.07	0.07
Grass	0.30	0.03	0.10	0.20
TOTAL	0.20	0.04	0.43	0.50
Catchment	203	Outlets to:	Rebecca Street	
	Runoff Coefficient	Area (ha)	Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Future Residential Development	0.60	0.05	0.60	0.75
TOTAL		0.05	0.60	0.75
Woodside Drive Total				
	Runoff		Weighted Runoff	
Catchment	Coefficient	Area	Coefficient	-
201	0.62	0.44	0.42	
202 EXT_1	0.60	0.17	0.10	
TOTAL	0.40	0.65	0.60	=
		0.00	0.00	
Rebecca Street Total	- <i>"</i>			
Catabaset	Runott	۸	Weighted Runoff	
		Area		-
ΤΟΤΔΙ	0.00	0.05	0.00	-
TOTAL		0.05	0.00	
Overall Total				
	Runoff		Weighted Runoff	
Catchment	Coefficient	Area	Coefficient	_
201	0.62	0.44	0.39	
202	0.60	0.17	0.15	
EA1-1	0.43	0.04	0.02	
203	0.00	0.05	0.04	=
IUIAL		0.70	0.60	

P:\2480 1258 Rebecca Street Oakville - Halton Region\Design\SWM\FSP\Design Calculations\2480 - Commercial SWM Design (MRM & WB)-Version1.xlsm

SUMMARY

						100 Year			
Catchment ID	Routing		Runoff Coef.	Area (ha)	Release Rate (L/s) ^{1 3}	Storage Required (m ³) ¹	Storage Available (m³)	Orifice Release Rate (L/s) ²	Uncontrolled Release Rate (L/s)
201	is routed through		0.71	0.44	81.4	175.7	180.0	81.4	
202	is routed through	201	0.75	0.17	72.1	0.0	0.0	-	72
EXT-1	is routed through	202	0.50	0.04	11.1	0.0	0.0	-	11
203	is routed through		0.75	0.05	20.0	0.0	0.0	-	20
Total				0.70	184.6	175.7	180.0	-	

Woodside Drive Allowable Release Rate 81.4 L/s

Woodside Drive Proposed Release Rate 81.4 L/s

Rebecca Street Proposed Release Rate 20.0 L/s

Notes:

¹ Per Modified Rational Calculations (attached)

² See attached for orifice details

³ The allowable release rate was determined using the total existing drainage to the Woodside Drive storm sewer

Area ID:	201		
Area =	0 112 ha		
"C" =	0.71		
AC= Tc =	0.3159 10.0 min		
Time Increment =	15.0 min 81 40 l/s	of Oakville	100 Year
Max.Storage =	175.7 m ³	a=	2150
		b= c=	5.7 0.861

NOTE: Catchment 202 is routed through Catchment 201

Time	Rainfall	Storm	Runoff	Released	Storage	
	Intensity	Runoff	Volume'	Volume	Volume	
(min)	(mm/hr)	(l/s)	(m ⁻)	(m ⁻)	(m ²)	
10.0	200.8	176.33	149.1	48.8	100.2	
25.0	112.7	98.99	224.2	85.5	138.7	
40.0	80.0	70.28	276.8	122.1	154.7	
55.0	62.7	55.04	322.2	158.7	163.5	
70.0	51.8	45.51	364.2	195.4	168.8	
85.0	44.4	38.95	404.1	232.0	172.1	
100.0	38.9	34.14	442.8	268.6	174.1	
115.0	34.7	30.45	480.5	305.2	175.2	
130.0	31.4	27.53	517.6	341.9	175.7	<<<<
145.0	28.6	25.16	554.1	378.5	175.6	
160.0	26.4	23.18	590.2	415.1	175.1	
175.0	24.5	21.52	626.0	451.8	174.3	
190.0	22.9	20.09	661.6	488.4	173.2	
205.0	21.5	18.85	696.9	525.0	171.8	
220.0	20.2	17.77	732.0	561.7	170.3	
235.0	19.1	16.81	766.9	598.3	168.6	
250.0	18.2	15.96	801.7	634.9	166.8	
265.0	17.3	15.19	836.3	671.5	164.8	
280.0	16.5	14.50	870.9	708.2	162.7	
295.0	15.8	13.88	905.3	744.8	160.5	
310.0	15.2	13.31	939.7	781.4	158.2	
325.0	14.6	12.79	973.9	818.1	155.8	
340.0	14.0	12.31	1008.1	854.7	153.4	
355.0	13.5	11.87	1042.2	891.3	150.9	

¹ The released volume from Catchment 202 has been added to the runoff volume of Catchment 201

ON-SITE DETENTION AND ORIFICE DETAILS

Area	ID	201
A Cu		20

Orifice Equation: $Q = C_d A (2gh)^{1/2}$

Type of Control: vertical Location: 1

Pipe Storage

Diameter	Area	Length	Volume
(mm)	(m²)	(m)	(m ³)
1.2 * 1.5 BOX	1.800	100	180.0
	Total Volume		180.0

	Stage (m)	Head (m)	Storage (m ³)	Discharge (m ³ /s)
Invert E.L.	86.25	0.00	0.0	0.00
100 Year WL	87.75	1.41	180.0	0.081

Area ID:	202		
Area ID: Area = "C" = AC= Tc = Time Increment = Release Rate = Max.Storage =	0.172 ha 0.75 0.1292 10.0 min 15.0 min 72.10 l/s 0.0 m ³	of Oakville a= b=	100 Year 2150 5.7
		C=	0.861

NOTE: Catchment 202 is routed through Catchment 201

Time	Rainfall	Storm	Runoff	Released	Storage	
	Intensity	Runoff	Volume	Volume	Volume	
(min)	(mm/hr)	(l/s)	(m ³)	(m ³)	(m ³)	
10.0	200.8	72.10	43.3	43.3	0.0	<<<<

Area ID: EXT-1

Area = "C" = AC= Tc = Time Increment =	0.040 ha 0.50 0.0200 10.0 min 15.0 min		
Release Rate =	11.14 l/s	of Oakville	100 Year
Max.Storage =	0.0 m ³	a= b= c=	2150 5.7 0.861

NOTE: Catchment EXT-1 is routed through Catchment 201.

Time	Rainfall	Storm	Runoff	Released	Storage	
	Intensity	Runoff	Volume	Volume	Volume	
(min)	(mm/hr)	(l/s)	(m ³)	(m ³)	(m ³)	
10.0	200.8	11.14	6.7	6.7	0.0	<<<<

Area ID:	203				
Aroo =	0.049	ha			
Area – "C" =	0.040	na			
AC=	0.0359				
Tc =	10.0	min			
Time Increment =	15.0	min			
Release Rate =	20.01	l/s	of Oakville	100 Year	
Max.Storage =	0.0	m ³	a=	2150	
			b=	5.7	
			C=	0.861	

Time	Rainfall	Storm	Runoff	Released	Storage	
	Intensity	Runoff	Volume	Volume	Volume	
(min)	(mm/hr)	(l/s)	(m ³)	(m ³)	(m ³)	
10.0	200.8	20.01	12.0	12.0	0.0	<<<<

APPENDIX F

SANITARY FLOW CALCULATIONS

T

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1258 Rebecca Street

Proposed Sanitary Flow Calculations	
Average Residential Flow Rate	275.0 litres/capita/day
Residential Population Density	
Single Family	55 persons/ha
Semi-detached	100 persons/ha
Residential Population	
Single Family (0.22 ha)	12 persons
Semi-detached (0.44 ha)	44 persons
Total population	56 persons
Peaking Factor	4.30
Residential Peak Flow	0.77 L/s
Site Area	0.66 ha
Infiltration (0.286 L/s/ha)	0.189 L/s
Total Proposed Peak Sanitary Flow	0.96 L/s
Existing Sanitary Flow Calculations	
Community Services Flow Rate	11,000 litres/ha/day
Community Services Population Density	40 persons/ha
Community Services Population (0.66 ha)	26.4 persons
Peaking Factor	3.49
Existing Peak Flow	0.29 L/s
Site Area	0.66 ha
Infiltration (0.286 L/s/ha)	0.189 L/s
Total Existing Peak Flow	0.48 L/s

SCS consulting group Itd												Sanit 1258 H To	ary Desig Rebecca alton Reg wn of Oal	n Sheet Street jion cville							Project:	: 1258 Rebecca	Street				
Minimum Sewer Diameter (mm) =	200	Avg. Dome	stic Flow (l	/cap/day) =	275																Project No.	. 2480					
Mannings n =	0.013	Infi	ltration Rat	te (l/s/ha) =	0.286																Date:	21-Apr-22					
Minimum Velocity (m/s) =	0.60	Max. Har	mon Peakir	ng Factor =	0.0																Designed By:	: M.M.					
Maximum Velocity (m/s) =	3.65	Min. Har	mon Peakir	ng Factor =	2.0															H	Reviewed By:	P.G.					
Minimum Pipe Slope (%) =	0.50	NOMIN	VAL PIPE S	SIZE USED	1																	P:\2480 1258	Rebecca Street Oakville	- Halton Region\Des	gn\Pipe Design\Sani	itary∖[2480-Sanitary S	ieet Design.xlsm]Desig
LOCATION						RESIDE	NTIAL			IN	DUSTRIAL	COMMERCI	AL/INSTITU	FIONAL		FLOW CALCULATIONS PIPE DATA											
	MAN	HOLE		ACCUM		DE	NSITY	DECIDENTIAL	ACCUM.		ACCUM	BOBULATION	FLOW	ACCUM.		TOTAL	AVG.	ACCUM. AVG.	DEAVING	PEAKED	ICI	TOTAL		DIDE			
STREET			AREA	ACCUM. AREA	UNITS	PER UNIT	PER HA	POPULATION	RESIDENTIAL POPULATION	AREA	AREA	DENSITY	RATE	EQUIV. POPULATION	INFILTRATION	ACCUM. POPULATION	DOMESTIC FLOW	DOMESTIC FLOW	FACTOR	RESIDENTIAL FLOW	FLOW	FLOW	LENGTH	DIAMETER	SLOPE	CAPACITY	VELOCITY
	FROM	то																									
			(ha)	(ha)	(#)	(p/unit)	(p/ha)			(ha)	(ha)	(p/ha)	(l/s/ha)		(L/s)		(L/s)	(L/s)		(L/s)	(L/s)	(L/s)	(m)	(mm)	(%)	(L/s)	(m/s)
1258 REBECCA STREET	CTRL.MH	EX.MH1A	0.66	0.66	0		84.8	56	56	0	0	0	0	0	0.19	56	0.2	0.2	4.30	0.77	0.0	0.96	15.9	200	1.00	32.8	1.04
REBECCA STREET	EX.MH1A	EX.MH2A	0	0.66	0			0	56	0	0	0	0	0	0.19	56	0.0	0.2	4.30	0.77	0.0	0.96	85.3	525	0.25	214.9	0.99

APPENDIX G

WATER MODELLING ANALYSIS

Multi Use Water Demand Table

Date: April 2022 Project No.: 2480 Prepared By: M.L.M.

WATER CONNECTION							
Connection Point	Rebecca Street						
Residential Water Usage Rate	0.275 m³/ca/day						
Single Family Population	12 persons						
Semi-detached Population	44 persons						
Hydrant flow test	To be completed in spring						
Hydrant flow test location							

	Presure (kPa)	Flow (in L/s)	Time
Minimum water pressure			
Maximum water pressure			

	WATER DEMANDS										
No.	Demand Type	Residential Peaking Factor	Single Family Demand (L/s)	Residential Peaking Factor	Semi-Detached Demand (L/s)	Total Demand (L/s)					
1	Average Day	1.00	0.04	1.00	0.14	0.18					
2	Maximum Day	2.25	0.09	2.25	0.32	0.40					
3	Maximum Hour	4.00	0.15	4.00	0.56	0.71					
5	Fire flow (see <i>Note 1</i>)	-	67 (4,000 L/min)	-	100 (6,000 L/min)	100.0 (6,000 L/min)					
6	Maximum day plus fire flow	-	-	-	-	100.4 (6,024 L/min)					

Notes

1. Single Family fire demand is based on FUS Note J - "Short Method" for detached one family dwellings. Semi-Detached fire demand calculations are attached.

				PROJECT IN	FORMATIC	N						
Address:		1258 Rebe	cca Street		Notes:	Semi-Detached homes						
-		Town of	Oakville			Fire area is based on Buildings 5-7 , wood						
						frame structur	es separated b	y less than 3 m.				
BASE FLOV	V CALCULA	TION						FLOW (L/min)				
A=	Effective a	rea		335	m ²							
C=	Wood fram	ne		1.5								
F=	Required fi	ire flow		6,040	L/min.							
"F" Rou	nded to ne	earest 1,000		6,000	L/min.			6,000				
FLOW 'F' A	DJUSTMEN	NTS				CREDITS	CHARGES	FLOW (L/min)				
0			0/									
Uccupancy	Adjustmei	nts (F)	% 1E%	000		000		E 100				
Liniteu	compustic	ne	-13%	-900		-900		5,100				
Exposure A	djustment	s (E)										
Expo	sure	Sep. (m)	Charge									
N	J	30	10%									
E	<u>.</u>	15	15%									
S	5	70	0%									
V	V	32	5%									
E = Total E	kposure Ch	arge	30%	1,530			1530	6,630				
Sprinkler A	djusments	(S)										
Sprinklered	as per NF	PA 13	No	0				6,630				
Standard V	Vater Supp	ly	Yes	-510		-510		6,120				
Fully super	vised wate	r supply	No	0				6,120				
PEOLUPEP					(1 /min)			- C 000				
REQUIRED	FLOWS (F	=F+E+SJ			(L/min)			6,000				

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