

**TRAFFIC IMPACT STUDY
BRONTE GREEN SUBDIVISION
MERTON TERTIARY PLAN
OAKVILLE**

**TRAFFIC IMPACT STUDY
BRONTE GREEN SUBDIVISION
MERTON TERTIARY PLAN
OAKVILLE**

FEBRUARY 2014

**READ, VOORHEES & ASSOCIATES
TORONTO, ONTARIO**

*Read, Voorhees & Associates Limited, 2 Duncan Mill Road, Toronto, Ontario M3B 1Z4
Tel: 416 445-4360 / Fax: 416 445-4809 / readvoorhees@rva.ca*

TABLE OF CONTENTS

| | Page |
|------------------------------------------------------------------------------|------|
| 1. INTRODUCTION..... | 1 |
| 2. DRAFT PLAN OF SUBDIVISION..... | 1 |
| 3. EXISTING CONDITIONS..... | 2 |
| 3.1 Road System | 2 |
| 3.2 Traffic Volumes | 3 |
| 3.3 Transit Service..... | 3 |
| 4. TRAFFIC FORECASTS..... | 4 |
| 4.1 Background Traffic | 4 |
| 4.2 Bronte Green Subdivision Traffic..... | 4 |
| 4.3 Total Traffic..... | 6 |
| 5. TRAFFIC OPERATIONS | 6 |
| 5.1 Signalized Intersections..... | 6 |
| 5.1.1 Bronte Road and Upper Middle Road | 8 |
| 5.1.2 Bronte Road and North Access..... | 8 |
| 5.1.3 Bronte Road and South Access..... | 8 |
| 5.1.4 Bronte Road and Halton Region Woodlands Operations Centre Access | 9 |
| 5.1.5 Bronte Road and North Service Road..... | 9 |
| 5.1.6 North Service Road and Halton Region Access..... | 10 |
| 5.1.7 Bronte Road and QEW Westbound Off-ramp | 10 |
| 5.1.8 Bronte Road and QEW Eastbound Off-ramp | 11 |
| 5.2 Internal Roadways | 12 |
| 5.3 Traffic Calming..... | 12 |
| 6. TRANSIT SERVICE..... | 13 |
| 6.1 Existing Oakville Transit Routes..... | 13 |
| 6.2 Internal Transit Route and Stops | 13 |
| 7. CONCLUSIONS..... | 13 |

LIST OF TABLES

| | Page |
|----------------------------------------------------------------|------|
| TABLE 1 - BRONTE GREEN TRIP GENERATION | 5 |
| TABLE 2 - SIGNALIZED INTERSECTION ANALYSIS (AM PEAK HOUR)..... | 7 |
| TABLE 3 - SIGNALIZED INTERSECTION ANALYSIS (PM PEAK HOUR)..... | 7 |

LIST OF FIGURES

- FIGURE 1. STUDY AREA
- FIGURE 2. BRONTE GREEN DRAFT PLAN OF SUBDIVISION
- FIGURE 3. EXISTING TRAFFIC
- FIGURE 4. 2019 BACKGROUND TRAFFIC
- FIGURE 5. RESIDENTIAL SITE TRAFFIC
- FIGURE 6. COMMERCIAL SITE TRAFFIC
- FIGURE 7. 2019 TOTAL TRAFFIC
- FIGURE 8. TRAFFIC CALMING LOCATIONS
- FIGURE 9. TRANSIT ROUTE AND STOP LOCATIONS

TRAFFIC IMPACT STUDY BRONTE GREEN SUBDIVISION MERTON TERTIARY PLAN OAKVILLE

1. INTRODUCTION

This Traffic Impact Study (TIS) is submitted in support of applications made by Bronte Green Corporation for rezoning and for a draft plan of subdivision for the Bronte Green development within the Merton Tertiary Plan area in the Town of Oakville.

The Town of Oakville is currently in the process of preparing the Merton (QEW/Bronte Road) Tertiary Plan for the lands north of the QEW between Bronte Road and Third Line. Figure 1 shows the Merton Tertiary Plan boundary and the location of the Bronte Green subdivision.

Read, Voorhees has been retained to prepare a traffic impact study (TIS) for the Bronte Green application.

The design hours for the traffic analysis are the weekday morning and afternoon commuter peak hours. A five year horizon period to 2019 has been used for the subdivision analysis. Implementation is anticipated to have full occupancy by the end of 2016.

For longer term planning analysis a ten year horizon period to 2024 has also been evaluated.

The study area includes the two proposed subdivision access intersections on Bronte Road, and the existing signalized intersections at Bronte Road and Upper Middle Road, Bronte Road and Woodlands Operations Centre, Bronte Road and North Service Road, Bronte Road and the WB QEW off-ramp, and Bronte Road and the EB QEW off-ramp.

2. DRAFT PLAN OF SUBDIVISION

The development is located on the existing Saw Whet golf course lands. The draft plan of subdivision is shown on Figure 2.

The subdivision is primarily residential with a commercial or 'Main Street' area on Street A adjacent to Bronte Road.

The residential unit count is 785, made up of 180 townhouse units and 605 detached units. There is also a 0.49 ha. high density residential block on the north side of Street A at Bronte Road, and a 0.69 ha. Main Street mixed use block opposite on the south side of Street A. No specific development is yet proposed on these two blocks, but an assumption of 90 apartment units and 1,725 m² of retail use and 1,725 m² of office use have been included in the traffic forecast.

The road system within the subdivision has Street A as a major collector with a right-of-way of 25 metres on the first block in from Bronte Road and 20 metres on the remainder of the road. It runs from Bronte Road to the east limit of the subdivision.

There are two minor collectors, Street B and Street C which have a right-of-way of 18 metres. Street C intersects with Bronte Road and then turns south and runs down to Street B. Street B will run from Street C east to Street A, but as an interim condition will have a cul-de-sac near the SMW pond until future development provides the connection to Street A.

All other public roads are local roads with a 16 metre right-of-way.

The Fourteen Mile Creek valley is a major geographic feature which precludes any feasible access to the north or east from the Saw Whet property. Connection to the existing Oakville road system will be on Bronte Road at Street A and at Street C.

Provision has been made for a future extension of Street A south into the Deerfield lands, which is expected to continue to North Service Road. As noted above, provision has been made for extension of Street B east through the Deerfield lands to meet the Street A extension. Provision is also made for an extension of Street B west to link into the Woodlands Centre access on Bronte Road. However, this linkage is not assumed to be in place for the subdivision traffic analysis.

The Street A intersection on Bronte Road will be the location of an access for development of the lands on the west side of Bronte Road. Interim operation will be as a T intersection until the west side of Bronte Road develops.

The north end of the subdivision north of Fourteen Mile Creek and west of the hydro corridor will be developed as a condominium block. The developable frontage on Upper Middle Road is very close to Bronte Road, and therefore provision of a full moves access intersection on Upper Middle Road is not possible. The area will be accessed by a private internal road system that extends north from Street C. Internal circulation will be provided on private roads with 10 metre rights-of-way.

Spacing between the new intersections on Bronte Road is 440 metres from Upper Middle Road to Street C, and 360 metres between the Street C and Street A intersections. The distance between Street A and the Woodlands Operations Access is 400 metres.

3. EXISTING CONDITIONS

3.1 Road System

Freeway service to the general Merton area is provided by the QEW which is a 6 lane facility plus 2 HOV lanes on this section. The highway provides connection to the east to Toronto and beyond and to the west to Hamilton and beyond. An interchange is located at Bronte Road.

Highway 407 is a 6 lane freeway located further to the north well outside the study area, also providing east-west service. An interchange is provided at Bronte Road.

Bronte Road is a four lane arterial road plus turn lanes at intersections. It provides north-south service through the area, and as noted has interchanges with the QEW to the south, and with Highway 407 to the north. Posted speed limit is 60 km/h. Bronte Road is under Region of Halton jurisdiction. The Region's TMP includes a recommendation for widening of Bronte Road to six lanes in the future from Speers Road to Highway 407. Bronte Road will be designated as a transit corridor with two of the lanes utilized as HOV lanes.

Upper Middle Road is an east-west arterial road north of the site that provides connection to the area further north of the QEW and with other north-south arterials. Upper Middle Road is under Region of Halton jurisdiction.

North Service Road is a major collector that serves the lands north of the QEW. The North Service Road runs from Bronte Road east to Third Line, and continues easterly across Oakville to Dorval Drive and Kerr Street. North Service Road is under Town jurisdiction.

Signalized intersections are located at Bronte Road and Upper Middle Road, at Bronte Road and Woodlands Operations access, at Bronte Road and North Service Road, at North Service Road and Halton Region Access, and at the two QEW Bronte Road interchange ramps.

3.2 Traffic Volumes

Figure 3 shows the existing peak hour traffic volumes in the vicinity of the site. The volumes are from the following counts:

| | |
|------------------------------------------------|--------------------------------|
| Bronte Road and Upper Middle Road | February 2012 by Halton Region |
| Bronte Road and Woodlands Entrance | October 2012 by Read Voorhees |
| Bronte Road and North Service Road | June 2011 by Halton Region |
| North Service Road and Halton Centre driveways | December 2010 by Read Voorhees |
| Bronte Road and QEW westbound Off-ramp | June 2011 by Halton Region |
| Bronte Road and QEW eastbound Off-ramp | November 2013 by Read Voorhees |

3.3 Transit Service

There are two Oakville Transit routes serving the Merton Tertiary Plan area and Halton Region Centre. The Upper Middle Route 6 service operates from the Bronte GO station along Bronte Road and across Upper Middle Road to the east end of Oakville at Winston Park. The Westoak Trails Route 13 service also operates from Bronte GO station up to and across West Oak Trails Blvd and connects to the Oakville GO Station at Cross Street. Headways are 20 minutes for the Upper Middle route, and 30 minutes for the Westoak Trails route.

As noted above, a Bronte Road widened to six lanes in the future will be a transit corridor with HOV lanes. However, the widening is not anticipated for the 2019 horizon period.

4. TRAFFIC FORECASTS

4.1 Background Traffic

The Halton Region Transportation Master Plan and the Oakville Transportation Master Plan (TMP) were updated in 2011 to provide traffic forecasts to 2031.

For long term planning in developing the Merton Tertiary Plan growth rates on the arterial roads in the study area were developed by a comparison of the 2031 assignments for the recommended plan in the TMP and the 2006 existing volumes calibration run. However, for the five year horizon period for the Bronte Green subdivision the background traffic on Bronte Road has been forecast by application of an annual growth rate of 2% over the intersection turning movements shown on Figure 3.

The Halton Region office complex on Bronte Road is within the Merton Tertiary Plan boundary. However, the existing development is not expected to change, so this segment is accounted for within the existing conditions data. There are no other site development approvals in the immediate vicinity of the Bronte Green proposal.

In the Merton Tertiary Plan traffic analysis allowance was made for possible commercial development as per the zoning on the QEW-Bronte Developments block on the east side of Bronte Road between the QEW Westbound off-ramp and North Service Road. However, there is no development application at present and therefore no forecast is added to the background traffic in this TIS.

Figure 4 shows the 2019 background traffic in the study area based on the above described arterial road growth rates applied to the existing volumes at the intersections.

4.2 Bronte Green Subdivision Traffic

Trip generation rates from the ITE Trip Generation Manual, Eighth Edition have been used as the base for subdivision traffic. For the single family units the rates for land use code 210 have been applied, and for townhouse units the rates for land use code 231 have been applied. For apartment units the rates for land use code 230 have been applied.

The retail commercial space will largely serve the subdivision, but there will also be some trips attracted as passby trips from traffic on Bronte Road. The rates from the ITE Trip Generation Manual for land use code 820 Shopping Centre have been applied using the fitted curve equation. The office auto trips will largely come from external zones. The rates from the ITE Trip Generation Manual for land use code 710 Office Building have been applied.

The ITE trip rates do not include a specific allowance for transit mode usage. Since future development in Oakville is being developed with a transit first policy and high quality transit service is being planned, the traffic generation forecast incorporates an anticipated transit mode split. For the 2019 horizon year a transit mode split of 5% has been applied to the site

traffic forecast for the Bronte Green subdivision. The overall Town objective is a 20% transit mode split by 2031.

The subdivision traffic forecast is shown in Table 1.

Table 1 - BRONTE GREEN TRIP GENERATION

| USE | UNITS | A.M. PEAK HOUR | | P.M. PEAK HOUR | |
|----------------------------|------------------------|----------------|------------|----------------|------------|
| | | In | Out | In | Out |
| Single family trip rate | Per unit | 0.19 | 0.56 | 0.64 | 0.37 |
| Units and Trips | 605 | 115 | 339 | 387 | 224 |
| Townhouse trip rate | Per unit | 0.17 | 0.50 | 0.45 | 0.33 |
| Units and Trips | 180 | 31 | 90 | 81 | 59 |
| Apartment trip rate | Per unit | 0.07 | 0.37 | 0.35 | 0.17 |
| Units and Trips | 90 | 6 | 33 | 32 | 15 |
| SUB-TOTAL | 875 | 152 | 462 | 500 | 298 |
| Transit trips | | 8 | 23 | 25 | 15 |
| NET SUB-TOTAL | | 144 | 439 | 475 | 283 |
| Retail trip rate | Per 100 m ² | 2.03 | 1.27 | 5.86 | 6.09 |
| Floor Area and Trips | 1725 m ² | 35 | 22 | 101 | 105 |
| Office trip rate | Per 100 m ² | 1.36 | 0.19 | 0.25 | 1.24 |
| Floor Area and Trips | 1725 m ² | 26 | 4 | 5 | 23 |
| TOTAL AUTO TRIPS | | 205 | 461 | 576 | 388 |
| EXTERNAL AUTO TRIPS | | 164 | 425 | 461 | 295 |

The site generated traffic assigned to the road system is shown in Figures 5 and 6, for the residential use and for the commercial uses respectively.

The residential trips are oriented primarily to and from employment areas in Oakville and the adjacent GTA municipalities. The retail trips are assumed to be oriented by and large to the subdivision, with 25% as linked trips associated with the other purpose trips made by residents. A passby component of 25% is assumed to be from Bronte Road through traffic.

The directional distribution and assignment by roadway is as follows:

| | Residential | Retail | Office |
|----------------------------|-------------|--------------------|-----------|
| Internal to Bronte Green | 4% | 75% (25% link) | 0% |
| West on QEW | 15 | 0 | 15 |
| East on QEW | 31 | 0 | 15 |
| East on Upper Middle | 10 | 0 | 15 |
| West on Upper Middle | 0 | 0 | 5 |
| East on North Service Road | 10 | 0 | 15 |
| South on Bronte Road | 10 | 12 (passby) | 20 |
| North on Bronte Road | <u>20</u> | <u>13 (passby)</u> | <u>15</u> |
| TOTAL | 100% | 100% | 100% |

4.3 Total Traffic

Figure 7 shows the total 2019 traffic at the study area intersections.

5. TRAFFIC OPERATIONS

5.1 Signalized Intersections

The intersections have been analyzed using the Synchro program. The output data is included in the Appendix. The operating parameters used are a saturation flow rate of 1900 vphg, a cycle length of 120 seconds, and the timing and phasing is optimized. For existing conditions a peak hour factor of 0.92 is applied, and this is also used for the 2019 horizon scenarios.

In the future Bronte Road is to be widened to six lanes through the study area, from Upper Middle Road south to Speers Road, with the curb lanes to be utilized as HOV lanes. However, this is not anticipated to be in place by 2019. Therefore the analysis has assumed operation on Bronte Road to be as per existing conditions.

Table 4 shows the results of the analysis for existing traffic, for 2019 background traffic and for 2019 total traffic conditions. The table shows the overall intersection results, and data for any individual through movements that have v/c ratios higher than 0.85 and turning movements with a v/c ratio higher than 1.0.

Table 2 - Signalized Intersection Analysis (AM Peak Hour)

| Intersection / Condition | Existing Traffic | | | Future Background 2019 Traffic | | | Future Total 2019 Traffic | | |
|--------------------------|------------------|-----|---------|--------------------------------|-----|---------|---------------------------|-----|---------|
| | Delay (sec) | LOS | HCM v/c | Delay (sec) | LOS | HCM v/c | Delay (sec) | LOS | HCM v/c |
| A.M. Peak Hour | | | | | | | | | |
| Bronte & Upper Middle | 23.3 | C | 0.64 | 27.5 | C | 0.77 | 33.8 | C | 0.78 |
| Bronte & North Access | - | - | - | - | - | - | 5.0 | A | 0.72 |
| Bronte & South Access | - | - | - | - | - | - | 14.8 | B | 0.86 |
| Bronte & Woodlands | 2.9 | A | 0.60 | 3.4 | A | 0.65 | 3.8 | A | 0.75 |
| Bronte & North Service | 3.1 | A | 0.46 | 3.2 | A | 0.54 | 3.5 | A | 0.62 |
| NSR & Region Access | 18.9 | B | 0.20 | 19.6 | B | 0.20 | 22.8 | C | 0.21 |
| Bronte & WB Off-ramp | 12.8 | B | 0.33 | 12.0 | B | 0.40 | 11.9 | B | 0.45 |
| WB right | 48.6 | D | 0.39 | 44.4 | D | 0.11 | 45.8 | D | 0.20 |
| WB left | 48.1 | D | 0.42 | 48.5 | D | 0.55 | 48.9 | D | 0.54 |
| NB thru | 3.5 | A | 0.31 | 1.9 | A | 0.37 | 2.3 | A | 0.38 |
| Bronte & EB Off-ramp | 26.0 | C | 0.70 | 40.2 | D | 0.93 | 46.8 | D | 0.95 |
| WB left | 52.4 | D | 0.78 | 65.6 | E | 0.97 | 72.6 | E | 0.98 |
| WB thru/right | 34.7 | C | 0.36 | 25.5 | C | 0.21 | 26.9 | C | 0.23 |
| SB left | 24.1 | C | 0.77 | 83.0 | F | 1.01 | 69.6 | E | 1.00 |
| NB thru | 25.8 | C | 0.51 | 40.3 | D | 0.74 | 80.8 | F | 1.02 |

Table 3 - Signalized Intersection Analysis (PM Peak Hour)

| Intersection / Condition | Existing Traffic | | | Future Background 2019 Traffic | | | Future Total 2019 Traffic | | |
|--------------------------|------------------|-----|---------|--------------------------------|-----|---------|---------------------------|-----|---------|
| | Delay (sec) | LOS | HCM v/c | Delay (sec) | LOS | HCM v/c | Delay (sec) | LOS | HCM v/c |
| P.M. Peak Hour | | | | | | | | | |
| Bronte and UMR | 15.1 | B | 0.58 | 17.4 | B | 0.69 | 22.3 | C | 0.73 |
| Bronte & North Access | - | - | - | - | - | - | 3.1 | A | 0.69 |
| Bronte & South Access | - | - | - | - | - | - | 20.2 | C | 0.85 |
| NB thru | - | - | - | - | - | - | 25.1 | C | 0.90 |
| Bronte and Woodlands | 3.1 | A | 0.56 | 3.5 | A | 0.65 | 5.0 | A | 0.77 |
| Bronte & North Service | 6.9 | A | 0.59 | 9.2 | A | 0.69 | 16.8 | B | 0.84 |
| NB thru | 3.5 | A | 0.65 | 7.9 | A | 0.76 | 18.1 | B | 0.94 |
| NSR & Region Access | 13.9 | B | 0.14 | 14.0 | B | 0.14 | 14.0 | B | 0.16 |
| Bronte & WB Off-ramp | 16.8 | B | 0.79 | 15.2 | B | 0.77 | 19.5 | B | 0.88 |
| WB right | 51.7 | D | 0.83 | 52.1 | D | 0.72 | 63.2 | E | 0.87 |
| WB left | 31.7 | C | 0.24 | 46.5 | D | 0.70 | 45.0 | D | 0.74 |
| NB thru | 9.1 | A | 0.77 | 5.4 | A | 0.79 | 9.8 | A | 0.89 |
| Bronte & EB Off-ramp | 41.7 | D | 0.94 | 31.5 | C | 0.85 | 40.4 | D | 0.93 |
| WB left | 36.3 | D | 0.34 | 72.8 | E | 0.92 | 65.8 | E | 0.89 |
| WB thru/right | 51.4 | D | 0.89 | 40.6 | D | 0.51 | 43.5 | D | 0.62 |
| NB thru | 54.6 | D | 0.98 | 31.0 | C | 0.86 | 49.2 | D | 0.98 |
| SB left | 79.5 | E | 0.95 | 66.4 | E | 0.87 | 82.3 | F | 0.98 |

5.1.1 Bronte Road and Upper Middle Road

The Bronte Road and Upper Middle Road intersection is presently operating at a v/c ratio of 0.64 in the a.m. peak hour and 0.58 in the p.m. peak hour. Level of service is at level C in the a.m. peak hour and level B in the p.m. peak hour. The signal phasing for existing conditions includes a southbound left turn phase, a northbound left turn phase, and a westbound left turn phase. A westbound double left turn lane configuration is now in place. These conditions are carried forward for the future traffic analysis.

With the 2019 background volumes level of service remains at level C in the a.m. peak hour and remains at level B in the p.m. peak hour. The v/c ratios are 0.77 in the a.m. peak hour and 0.69 in the p.m. peak hour.

With the Bronte Green traffic added to the road system, the Bronte Road and Upper Middle Road intersection level of service remains at level C in the a.m. peak hour and changes to level C in the p.m. peak hour. The v/c ratio in the a.m. peak hour increases by 0.01 to 0.78, and in the p.m. peak hour increases by 0.04 to 0.73.

No additional mitigation is required to accommodate the subdivision traffic.

5.1.2 Bronte Road and North Access

The North Access road in the subdivision plan will operate at level of service A in the a.m. peak hour and at level A in the p.m. peak hour. This access will service all the residential uses at the north end of the subdivision and by some of the units in the remainder of the subdivision. Two outbound lanes should be provided on the approach to Bronte Road, and designated as separate left turn and right turn lanes.

A separate southbound left turn lane is required at the intersection, but the volume of left turns during the peak hours does not require a separate signal phase. A northbound right turn lane will be provided to maximize available capacity on Bronte Road.

During the a.m. peak hour the southbound through lanes on Bronte Road are calculated to operate at level of service A based on average vehicle delay, and with a v/c ratio of 0.77. In the p.m. peak hour northbound Bronte Road is calculated to operate at level of service A based on average vehicle delay and with a v/c ratio of 0.69.

5.1.3 Bronte Road and South Access

The South Access road for the subdivision will be the busier of the two access roadways on Bronte Road since it is more central to the overall development, and it will serve the commercial site. The intersection will in the future have a west leg that serves the lands west of Bronte Road. However, initially it will operate as a T intersection. Two outbound lanes are required at the intersection on the east leg, operating as a left turn lane and a right turn lane. In the future the right lane will also accommodate any through traffic.

Northbound and southbound left turn lanes will be provided at the intersection, as will northbound and southbound right turn lanes to maximize available capacity on Bronte Road.

With the volumes forecast a separate southbound left turn phase is required in the p.m. peak hour. During the a.m. peak hour there is only a small volume of left turns. The intersection will operate in the a.m. peak hour with a v/c ratio of 0.86, and at level of service B. During the p.m. peak hour the v/c ratio is 0.85 and the level of service is level C.

Similar to the condition for Bronte Road noted above for the North Access, during the a.m. peak hour the southbound through traffic is calculated to operate at level of service A, and will have a v/c ratio of 0.88. In the p.m. peak hour the northbound through traffic on Bronte Road will operate at level of service C with a v/c ratio of 0.90.

5.1.4 Bronte Road and Halton Region Woodlands Operations Centre Access

The Bronte Road intersection at the Halton Region Woodlands Operations Centre access driveway is presently operating at a v/c ratio of 0.60 in the a.m. peak hour and 0.56 in the p.m. peak hour. Level of service is at level A in both peak hours. The volumes in and out of the Centre are minor and the signal is required in order to provide safe access out to a busy Bronte Road. Average vehicle delay at the intersection is only 2.5 seconds in the a.m. peak hour and 3.1 seconds in the p.m. peak hour.

For 2019 conditions with the background volumes the level of service remains at level A in both peak hours, and the v/c ratios are 0.65 in the a.m. peak hour and 0.65 in the p.m. peak hour.

With the Bronte Green subdivision traffic added to the road system, the intersection level of service remains at level A in the a.m. peak hour and remains at level A in the p.m. peak hour. The v/c ratio in the a.m. peak hour increases by 0.10 to 0.75, and in the p.m. peak hour increases by 0.12 to 0.77.

The intersection has adequate capacity and no other improvement is necessary to accommodate the 2019 forecast and the proposed Bronte Green development.

5.1.5 Bronte Road and North Service Road

The Bronte Road and North Service Road intersection is presently operating at a v/c ratio of 0.46 in the a.m. peak hour and 0.59 in the p.m. peak hour. Level of service is at level A in the a.m. peak hour and at level A in the p.m. peak hour.

With the 2019 background volumes level of service remains at level A in the a.m. peak hour and at level A in the p.m. peak hour. The intersection v/c ratios are 0.54 in the a.m. peak hour and 0.69 in the p.m. peak hour.

With the Bronte Green traffic added to the road system, the Bronte Road and North Service Road intersection level of service remains at level A in the a.m. peak hour and changes to level B in the p.m. peak hour. The v/c ratio in the a.m. peak hour increases by 0.08 to 0.62, and in the p.m. peak hour increases by 0.15 to 0.84.

The intersection already operates with two westbound left turn lanes, and no improvements are required to accommodate the proposed subdivision.

5.1.6 North Service Road and Halton Region Access

The North Service Road intersection with the Halton Region Centre access driveways is presently operating at a v/c ratio of 0.20 in the a.m. peak hour and 0.14 in the p.m. peak hour. Level of service is at level B in both peak hours.

No change is anticipated for the 2019 background volumes.

A small volume of Bronte Green subdivision traffic is expected to use the North Service Road to travel to and from the east. However, this will have negligible impact on the intersection. With the subdivision traffic added to the road volumes the v/c ratio in the a.m. peak hour increases by 0.01 to 0.21, and in the p.m. peak hour increases by 0.02 to 0.16.

The increases in average vehicle delay is small at 3 seconds in the a.m. peak hour, but because this changes from 19.1 seconds to 22.7 seconds this crosses the dividing line between levels of service B and C. In the p.m. peak hour there is no change in average vehicle delay and therefore no change from level of service B.

5.1.7 Bronte Road and QEW Westbound Off-ramp

The Bronte Road and QEW Westbound Off-ramp intersection is presently operating at a v/c ratio of 0.33 in the a.m. peak hour and 0.79 in the p.m. peak hour. Level of service is at level B in both peak hours.

The current right turn volume on the Off-ramp is higher than the left turn volume, particularly in the p.m. peak hour. However, the lane designation has two left turn lanes and one right turn lane. With the 2019 background traffic, the right turn volume is getting to a v/c ratio of 0.94 and is approaching the capacity of one lane. Therefore it is recommended that the present lane designation of two left turn lanes and one right turn lane be modified to make the centre lane an optional left/right lane. This requires only revised pavement marking, and does not involve any road construction

With this change the Bronte Road and QEW Westbound Off-ramp intersection level of service for 2019 background traffic remains at level B in both peak hours. The v/c ratio in the a.m. peak hour is 0.40, and in the p.m. peak hour is 0.77.

With the Bronte Green subdivision traffic added, the Bronte Road and QEW Westbound Off-ramp intersection level of service remains at level B in the a.m. peak hour and remains at

level B in the p.m. peak hour. The v/c ratio in the a.m. peak hour increases by 0.05 to 0.45, and in the p.m. peak hour increases by 0.11 to 0.88.

5.1.8 Bronte Road and QEW Eastbound Off-ramp

The Bronte Road and QEW Eastbound Off-ramp intersection is presently operating at a v/c ratio of 0.70 in the a.m. peak hour and 0.94 in the p.m. peak hour. Level of service is at level C in the a.m. peak hour and level D in the p.m. peak hour. The 2013 volumes at this intersection appear to have increased considerably over a previous count in 2010, doubling the volume for some ramp movements. Therefore the intersection is already approaching capacity in the p.m. peak hour if these volumes are representative of regular use.

With the 2019 background volumes and the current ramp geometry the level of service would move into level D in the a.m. peak hour and level E in the p.m. peak hour. The v/c ratios would be 0.77 in the a.m. peak hour and 1.02 in the p.m. peak hour.

With the Bronte Green traffic added to the intersection, the Bronte Road and QEW Eastbound Off-ramp intersection would change to level of service D in the a.m. peak hour, and change to level F in the p.m. peak hour. The v/c ratio in the a.m. peak hour would increase to 0.86, and in the p.m. peak hour to 1.18.

Therefore with the future 2019 volume increases as forecast, mitigation may be required. The Merton Tertiary Plan traffic analysis recommended that for the long term the improvement that would add capacity to the intersection is a second right turn lane on the eastbound off-ramp on the approach to Bronte Road. This movement is a heavy right turn volume, currently 481 vph in the a.m. and 576 vph in the p.m. peak hour. The 2019 right turn volume is forecast to increase by 70 to 551 vph in the a.m., and increase by 130 to 706 vph in the p.m. peak hour.

However, an interim mitigation measure will also accommodate the 2019 volumes, without having to construct an additional lane. At the QEW Eastbound Off-ramp the current lane designation has two left turn lanes and a through-right lane. The existing volumes of left and right turns on the off-ramp are about equal in the a.m. peak hour, but the right turn is substantially higher than the left turn in the p.m. peak hour. This imbalance in the p.m. peak hour is forecast to be even greater in the future scenarios. Therefore it is recommended that the lane designations on the off ramp be revised to have only one exclusive left turn lane, designate the centre lane as a through/right lane to accommodate the through movement into the carpool lot, and have one exclusive right turn lane.

With this revision the Bronte Road and QEW Eastbound Off-ramp intersection will operate for 2019 background traffic in the a.m. peak hour with a v/c ratio of 0.93 and level of service D. In the p.m. peak hour the 2019 background v/c ratio is 0.85 and level of service is C.

For 2019 total traffic in the a.m. peak hour the v/c ratio is 0.95 and level of service is D, and in the p.m. peak hour the v/c ratio is 0.93 and level of service is D.

As noted above, this mitigation does not require any construction, but for the long term traffic forecasts beyond 2019 an additional right turn lane is recommended on the approach to Bronte Road to accommodate higher volumes.

It is noted that the Synchro analysis has been carried out using a peak hour factor of 0.92. Under capacity conditions the peak hour factor will increase towards 1.0, and the intersection v/c ratios will decline compared to the noted values.

5.2 Internal Roadways

The roadways within Bronte Green subdivision will be constructed to the standard established for each classification of road in the Town's Design Guidelines.

The highest directional volumes are in the order of 650 vph on Street A, the South Access road, at the intersection with Bronte Road. The volumes disperse along Street A eastward into the subdivision. This section of the South Access is adjacent to the commercial block, and a right-of-way of 25 metres has been provided. A four lane cross section is recommended in this block to facilitate access and possibly provide parking. All other roadways in the subdivision can be constructed with two through lanes. The central Street A collector road has a 20 metre right-of-way, and can have a third centre turning lane provided in the cross section.

All intersections within the subdivisions can operate satisfactorily with Stop sign control. Traffic signals are not warranted at any intersection within the Bronte Green plan.

5.3 Traffic Calming

The primary initial measure for traffic calming is identification of sections of straight roadway that are longer than 300 metres for roads that are expected to operate with a posted speed limit of 50 km/h. This would apply to the collector system, made up of Street A, Street C and Street B. For local roads that are posted with speed limits of 40 km/h the critical length of straight road is 160 metres.

The traffic calming features are to be located to achieve the Town's goals of eliminating the potential for speeding, and creating safe pedestrian and cycling environments. The use of all-way Stop sign control at the intersection of the collector roads also acts as a traffic calming factor.

Figure 8 shows the location of the proposed traffic calming features.

It is recommended that all-way Stop sign control be implemented at the intersection of Street A and Street C, and at the intersection of Street B and Street C. This would leave the east section of Street A as a long section of straight road that can be mitigated with a curb extension treatment at the intersection with Street T/Street V. Street C would also have a long straight section between Streets A and B, which can be mitigated with a curb extension treatment at the intersection with Street M.

The traffic calming features can be finalized as part of the detailed road design that will subsequently be prepared for the subdivision.

6. TRANSIT SERVICE

6.1 Existing Oakville Transit Routes

At the present time Oakville Transit operates regular service along Bronte Road on Route 6 and Route 13. A 400 metre walking distance from Bronte Road would cover the area over to the hydro corridor. Service to development east of the hydro corridor would require a route into the subdivision.

6.2 Internal Transit Route and Stops

Transit service for the Merton Tertiary Plan area in the long term would likely be provided by a route through the lands on the Street A collector road intersecting Bronte Road and North Service Road.

As the subdivision develops the area from Bronte Road to the hydro corridor can be served by the transit service on Bronte Road since it is within a 400 metre coverage zone. The units east of the hydro corridor would require an internal transit route for coverage since that area extends a further 400 metres east of the hydro corridor. This would require a routing to and from Bronte Road along Street A with an interim turn around provision until the Deerfield lands develop and provide a connection to North Service Road.

Transit stop locations would be located at the intersections with Street C, Street I, Street U and at an interim turnaround loop at the end of Street A. Average stop spacing is in the order of 150 to 200 metres.

Figure 9 shows the transit route and transit stop locations along Street A.

7. CONCLUSIONS

The Bronte Green subdivision is located on the east side of Bronte Road, and is presently operating as the Saw Whet golf course.

The residential unit count is 785, made up of 180 townhouse units and 605 detached units. There is also a 0.49 ha. high density residential block on the north side of Street A at Bronte Road, and a 0.69 ha. mixed use block on the opposite south side of Street A. An assumption of 90 apartment units and 1,725 m² of retail uses and 1,725 m² of office uses been included in the traffic forecast.

Road access for the subdivision will be two connections to Bronte Road, at Street A and at Street C. Provision has been made for future extension of Street A south into the Deerfield lands, which is expected to continue to North Service Road. Provision has also been made for extension of Street B east to meet a Street A extension, and for a future extension of Street B west to link into the Woodlands Centre access to Bronte Road.

A 5 year horizon period to 2019 has been used for traffic forecasting. The subdivision is expected to be completed and occupied by the end of 2016. The growth rate applied to Bronte Road for traffic forecasting is a 2% annual rate applied to existing volumes. Bronte Road is planned to be widened to six lanes in the future from Upper Middle Road down to Speers Road, but this is not expected to be in place for the 2019 horizon period.

The traffic operations analysis indicates that the existing road system can accommodate the 2019 background forecast plus the Bronte Green traffic within the study area. However, operational changes that modify the lane configurations are recommended at the two QEW off-ramp intersections.

At the Bronte Road and QEW Westbound Off-ramp it is recommended that the centre lane be designated as an optional left or right turn lane. The right turn volume in the p.m. peak hour is much higher than the left turn volume. Similarly, at the Bronte Road and QEW Eastbound Off-ramp it is recommended that the ramp lane designations be modified to create a left turn lane, a through/right lane, and a right turn lane. The right turn volume in the p.m. peak hour is much higher than the left turn volume. No new construction at the ramp terminals is required for these modifications.

The traffic volumes within the Bronte Green subdivision can be accommodated on two lane roadways throughout the plan, although it is recommended that the section of Street A adjacent to the commercial block be constructed as a four lane road.

All intersections within the subdivision can operate satisfactorily with Stop sign control.

Traffic calming can be provided within the subdivision with the all-way Stop control that is recommended on the collector road system, and with curb extensions along the straight sections of the collector roads.

Transit service is now being provided along Bronte Road, and in the long term Bronte Road is to be designated as a transit corridor with HOV lanes. Transit service is expected to operate in the longer term future on Street A between Bronte Road and North Service Road. In the interim an internal route to and from Bronte Road can be provided to have all units within 400 metres of transit service.

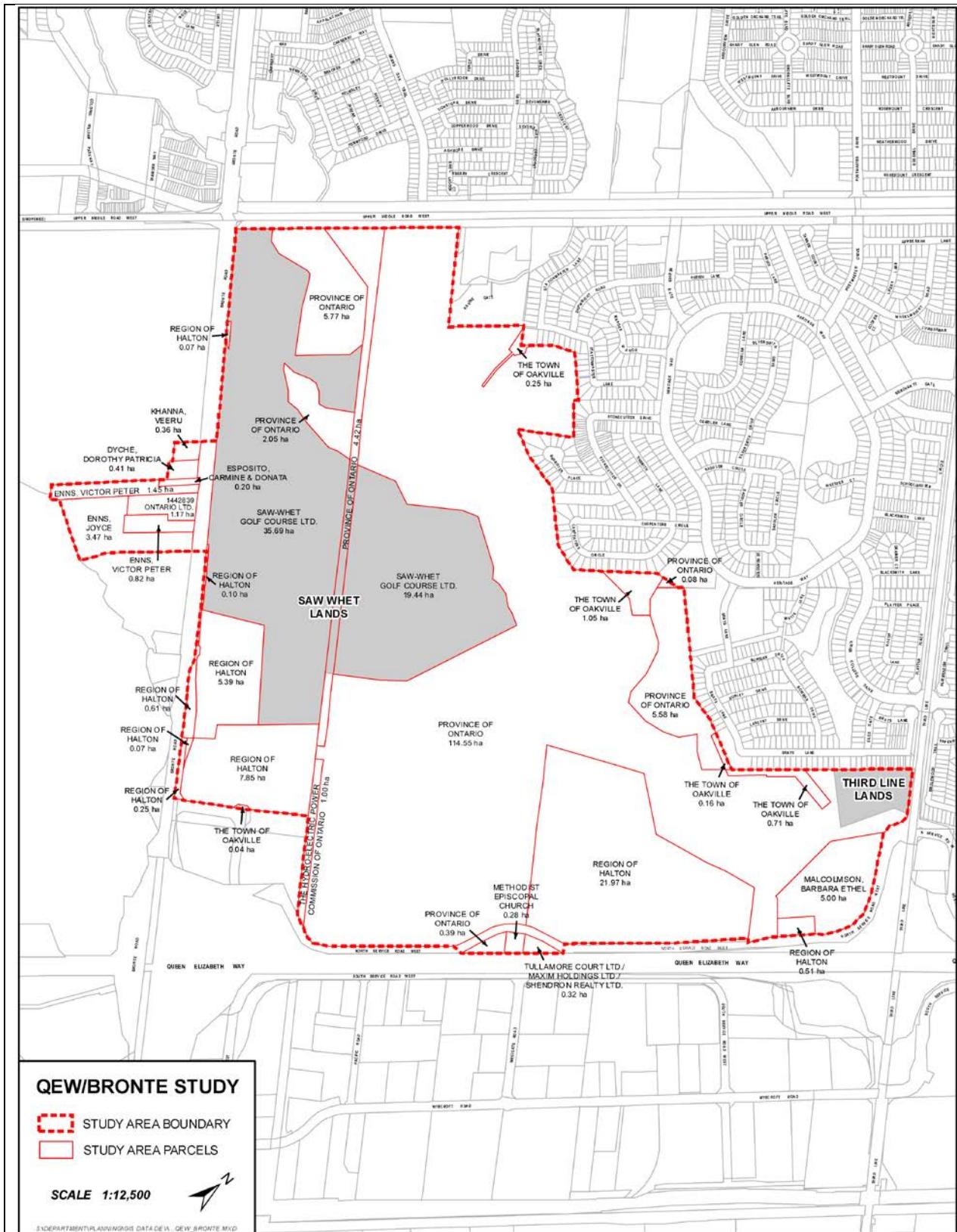
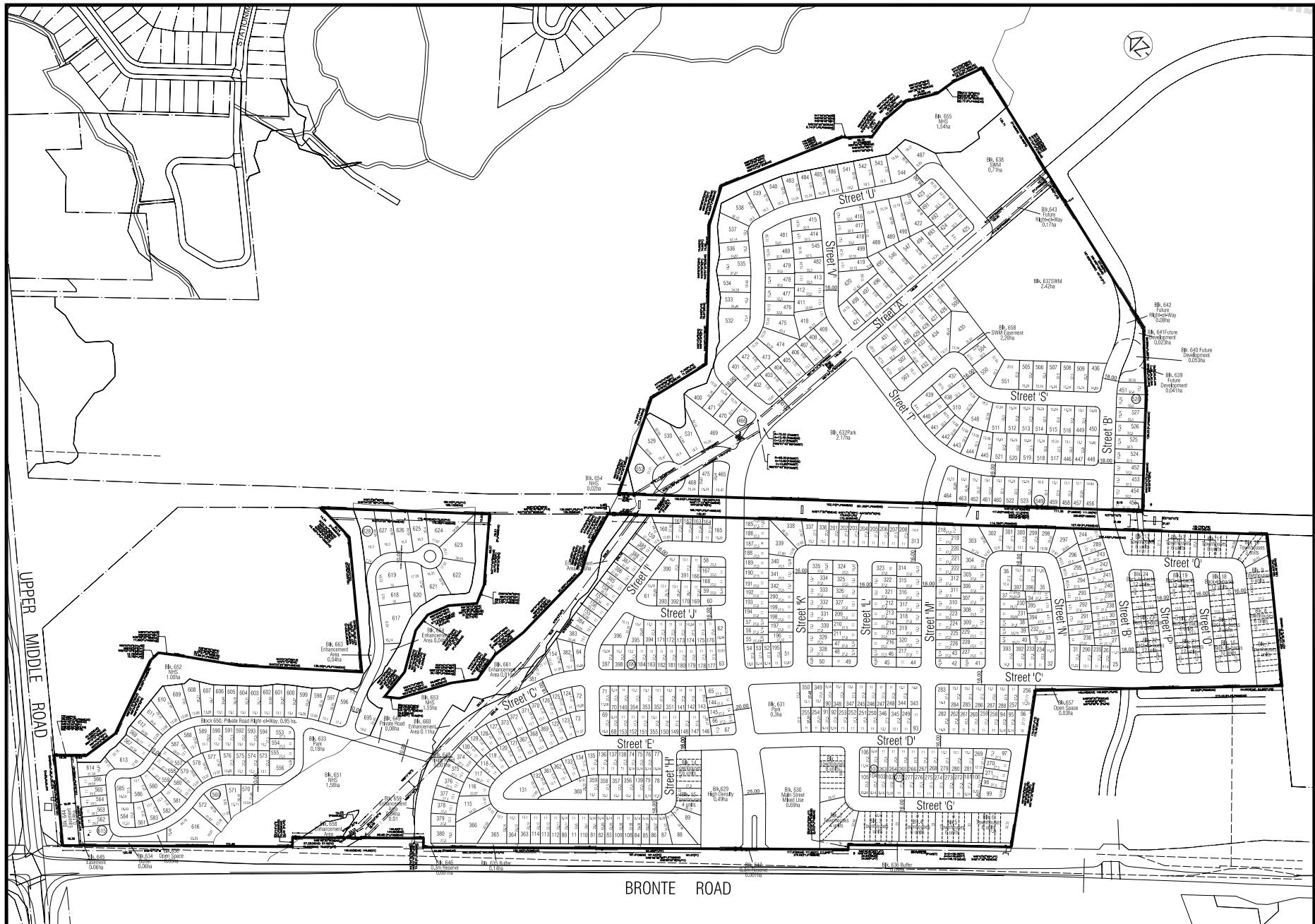
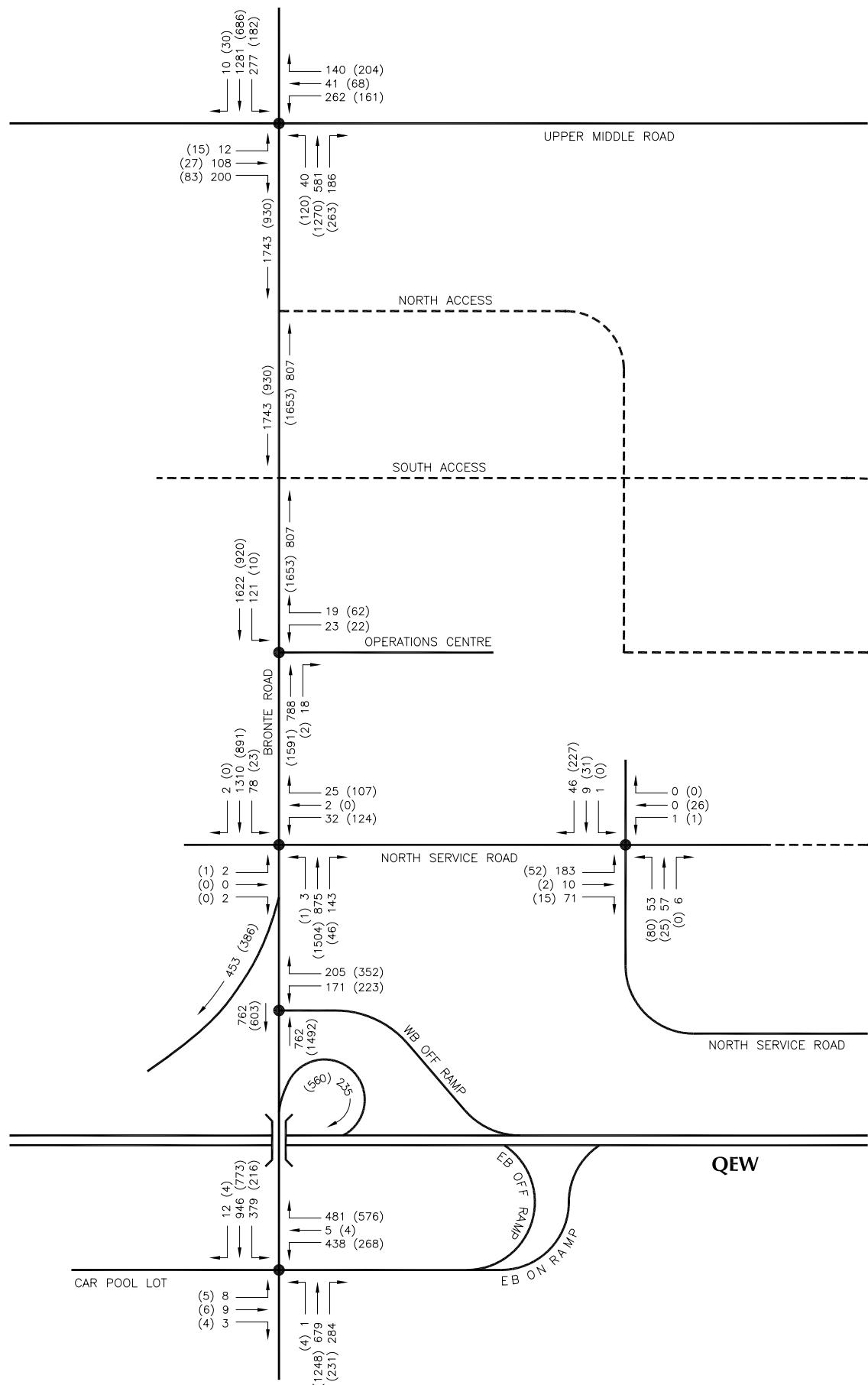


Figure 1 – Merton (QEW Bronte Road) Planning Study Area



DRAFT PLAN OF SUBDIVISION
FIGURE 2

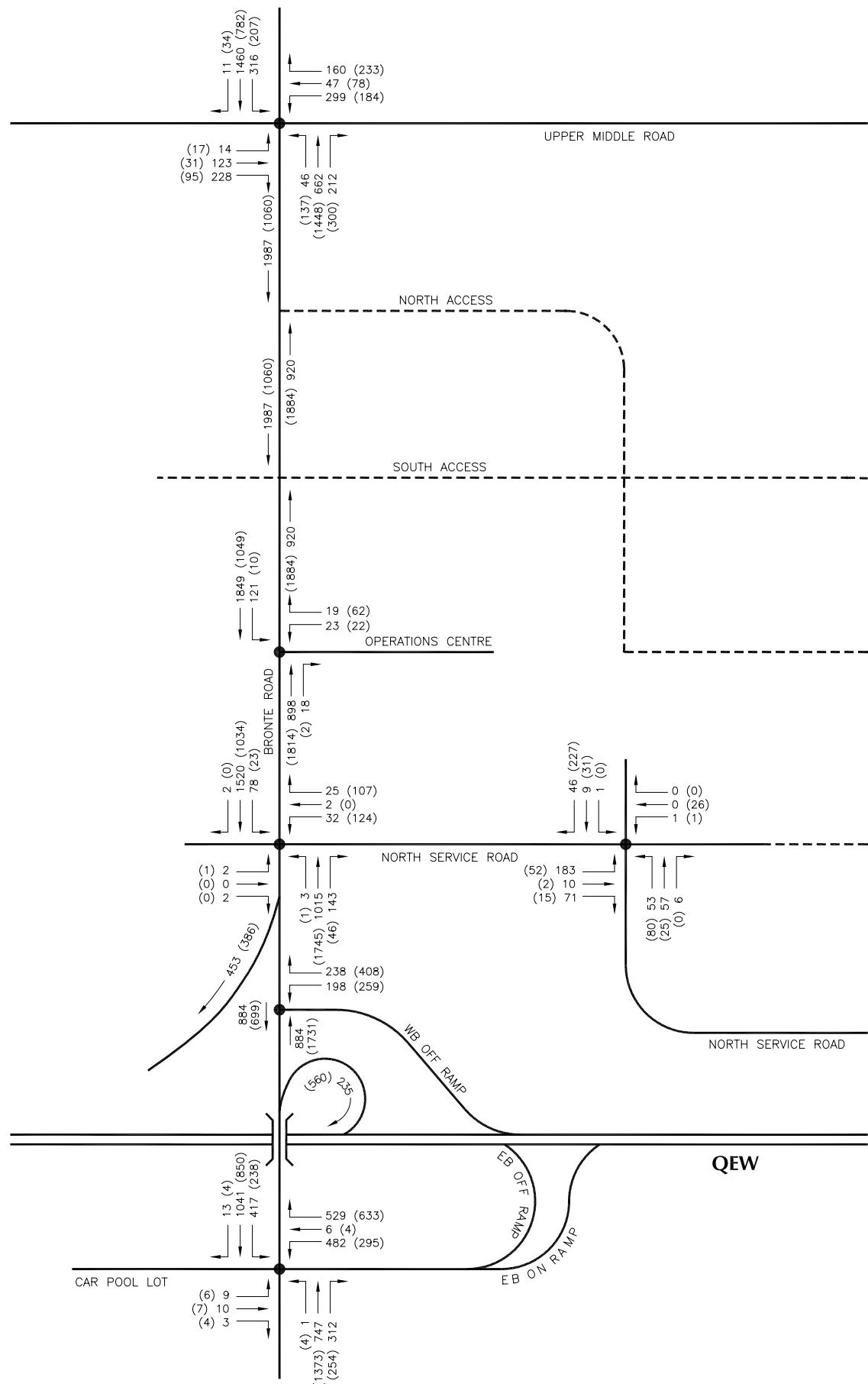


LEGEND

- 48 A.M. PEAK HOUR VOLUME
(11) P.M. PEAK HOUR VOLUME
● SIGNALIZED INTERSECTION

EXISTING TRAFFIC

FIGURE 3

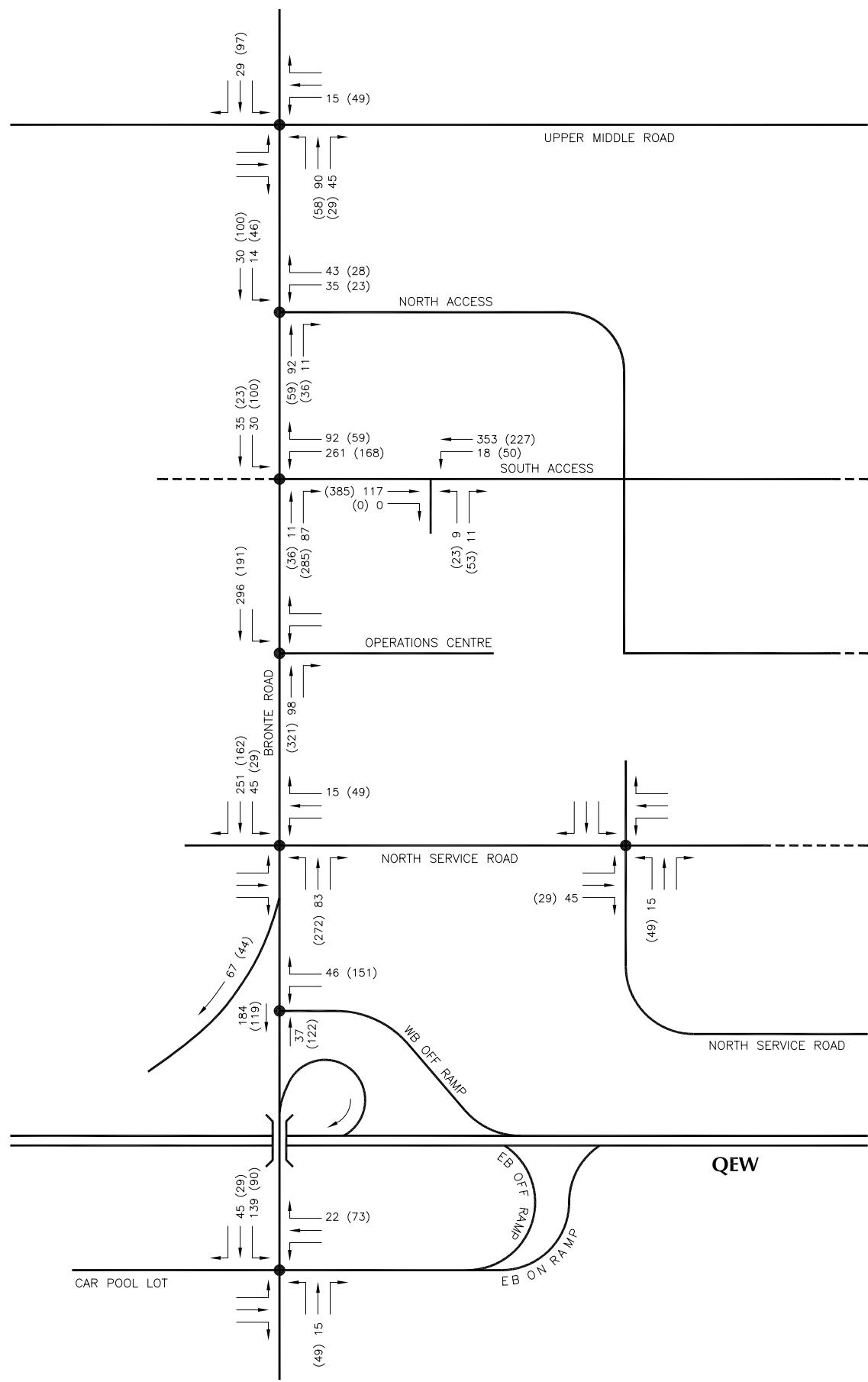


LEGEND

- 48 A.M. PEAK HOUR VOLUME
(11) P.M. PEAK HOUR VOLUME
● SIGNALIZED INTERSECTION

2019 BACKGROUND TRAFFIC

FIGURE 4

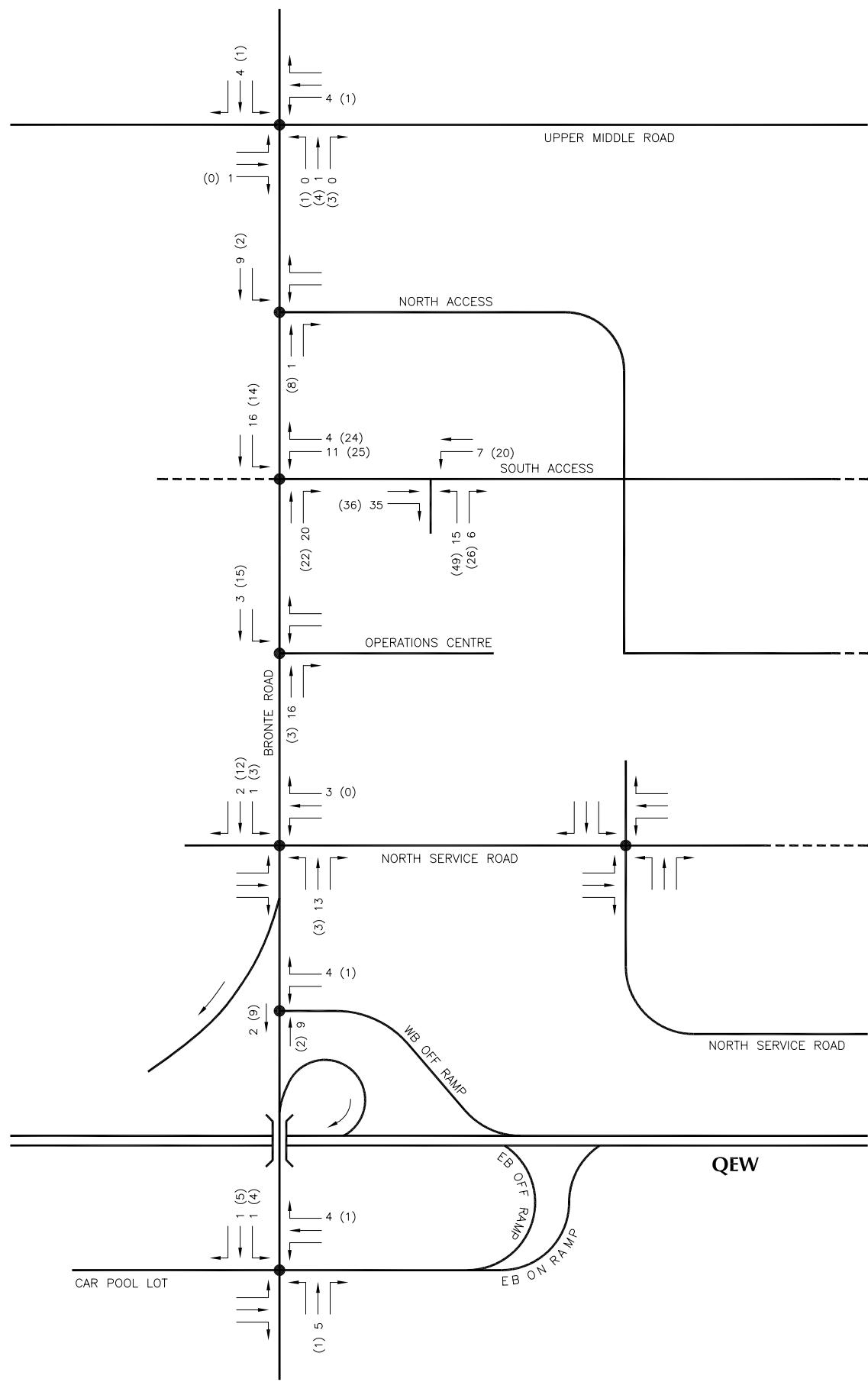


LEGEND

- 48 A.M. PEAK HOUR VOLUME
(11) P.M. PEAK HOUR VOLUME
● SIGNALIZED INTERSECTION

RESIDENTIAL SITE TRAFFIC

FIGURE 5

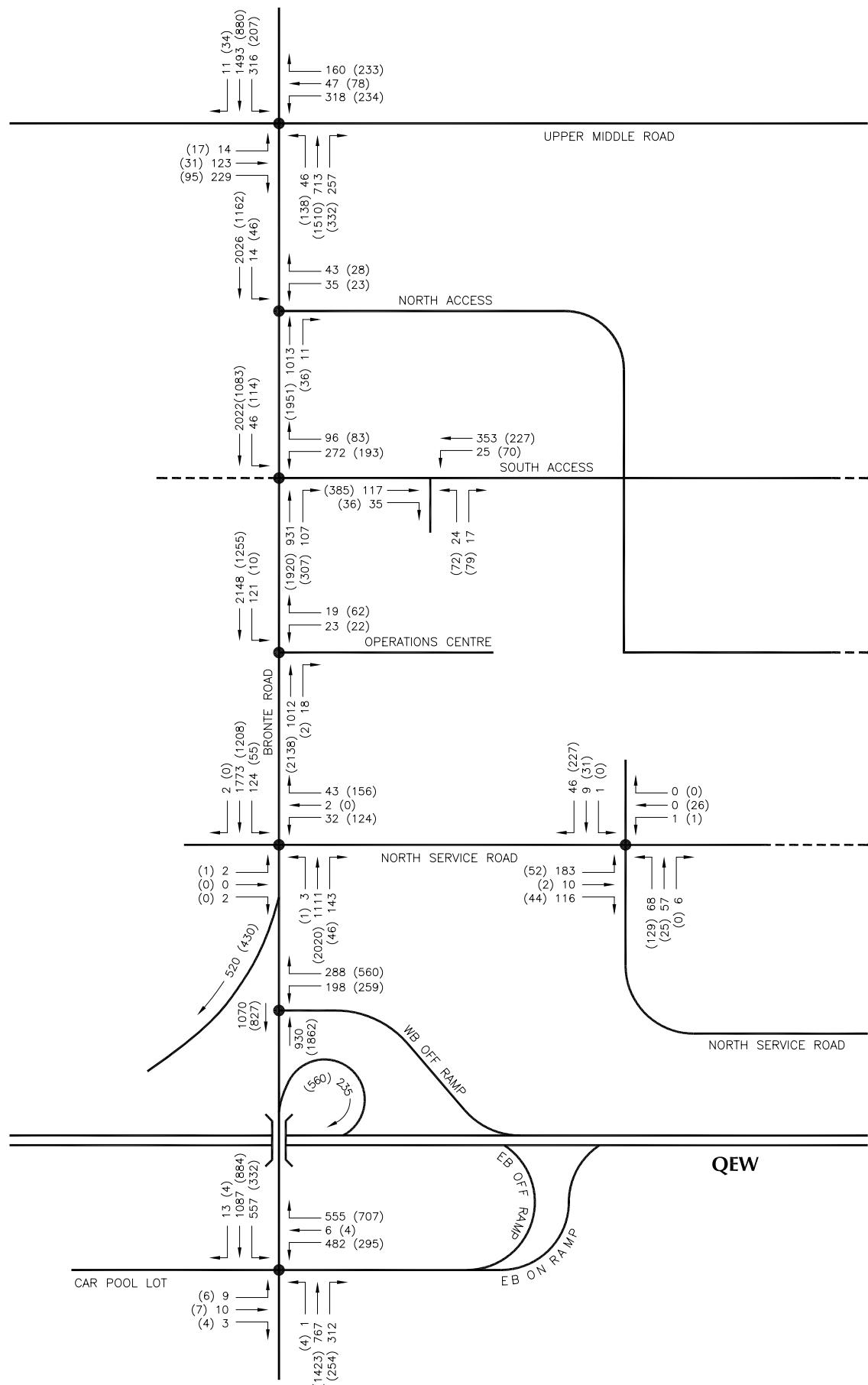


LEGEND

- 48 A.M. PEAK HOUR VOLUME
(11) P.M. PEAK HOUR VOLUME
● SIGNALIZED INTERSECTION

COMMERCIAL SITE TRAFFIC

FIGURE 6

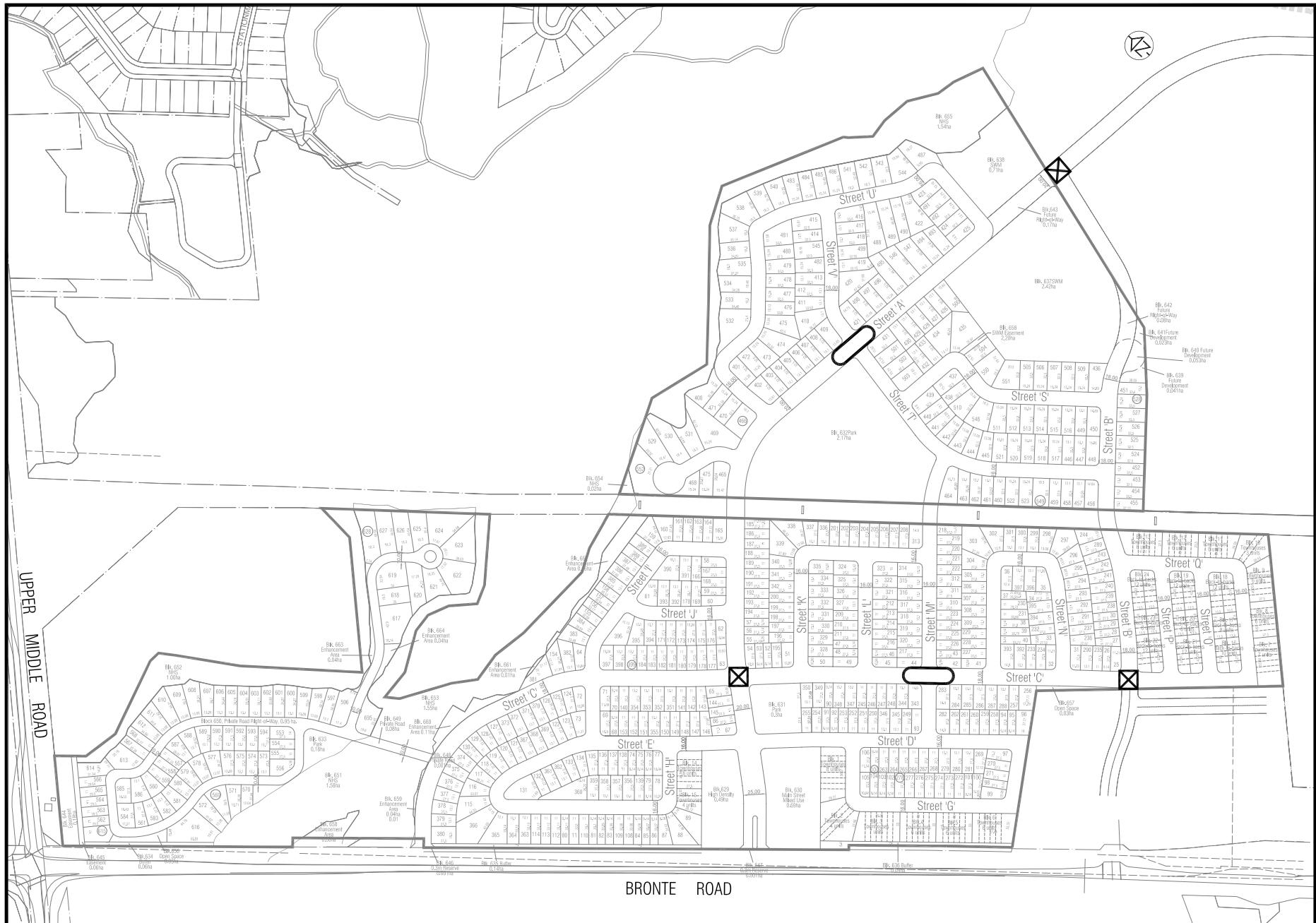


LEGEND

- 48 A.M. PEAK HOUR VOLUME
(11) P.M. PEAK HOUR VOLUME
● SIGNALIZED INTERSECTION

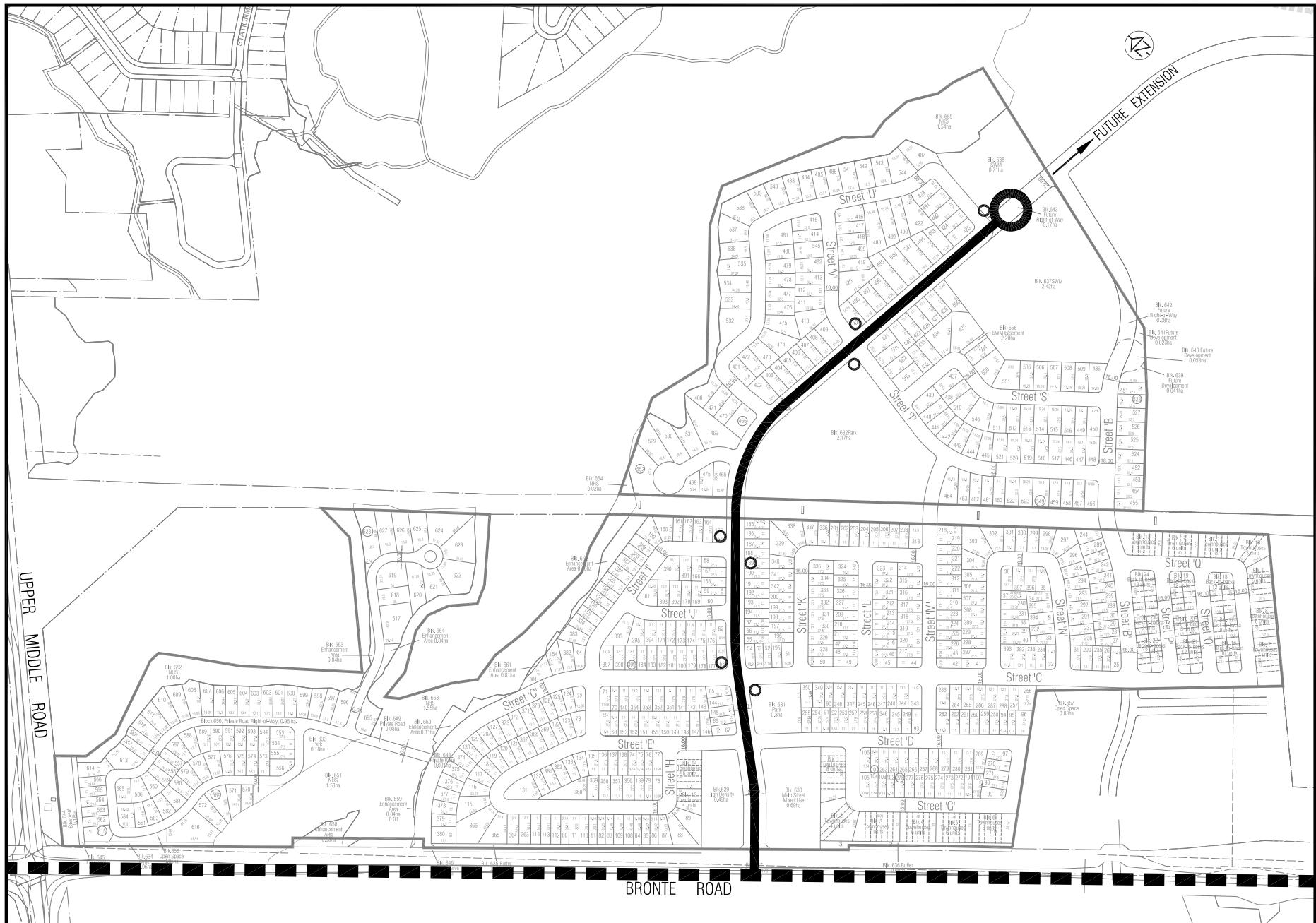
2019 TOTAL TRAFFIC

FIGURE 7



TRAFFIC CALMING LOCATIONS

FIGURE 8



TRANSIT PLAN AND STOP LOCATIONS

FIGURE 9

APPENDIX

SYNCHRO OUTPUT

HCM Signalized Intersection Capacity Analysis

15: WOODLANDS & BRONTE

EXISTING

AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|-------|----------------------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 23 | 19 | 794 | 18 | 121 | 1716 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1566 | 1521 | 3400 | 1597 | 1785 | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.32 | 1.00 |
| Satd. Flow (perm) | 1566 | 1521 | 3400 | 1597 | 608 | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 25 | 21 | 863 | 20 | 132 | 1865 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 3 | 0 | 0 |
| Lane Group Flow (vph) | 25 | 1 | 863 | 17 | 132 | 1865 |
| Heavy Vehicles (%) | 14% | 5% | 5% | 0% | 0% | 5% |
| Turn Type | custom | | | Perm | Perm | |
| Protected Phases | | | 2 | | | 6 |
| Permitted Phases | 8 | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 5.1 | 5.1 | 100.9 | 100.9 | 100.9 | 100.9 |
| Effective Green, g (s) | 8.1 | 8.1 | 103.9 | 103.9 | 103.9 | 103.9 |
| Actuated g/C Ratio | 0.07 | 0.07 | 0.87 | 0.87 | 0.87 | 0.87 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 106 | 103 | 2944 | 1383 | 526 | 2944 |
| v/s Ratio Prot | | | 0.25 | | | c0.55 |
| v/s Ratio Perm | c0.02 | 0.00 | | 0.01 | 0.22 | |
| v/c Ratio | 0.24 | 0.01 | 0.29 | 0.01 | 0.25 | 0.63 |
| Uniform Delay, d1 | 53.0 | 52.2 | 1.4 | 1.1 | 1.4 | 2.4 |
| Progression Factor | 1.00 | 1.00 | 1.09 | 1.51 | 0.67 | 0.60 |
| Incremental Delay, d2 | 1.1 | 0.1 | 0.2 | 0.0 | 0.9 | 0.8 |
| Delay (s) | 54.2 | 52.3 | 1.8 | 1.7 | 1.8 | 2.3 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 53.3 | | 1.8 | | | 2.3 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 2.9 | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | | 0.60 | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | | 57.4% | ICU Level of Service | | B |
| Analysis Period (min) | | | 15 | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

6: WB OFF RAMP & BRONTE

EXISTING

AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|----------------------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 171 | 205 | 762 | 0 | 0 | 762 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 0.95 | | | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3298 | 1452 | 3336 | | | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3298 | 1452 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 186 | 223 | 828 | 0 | 0 | 828 |
| RTOR Reduction (vph) | 0 | 146 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 186 | 77 | 828 | 0 | 0 | 828 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |
| Turn Type | Perm | | | | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | 8 | | | |
| Actuated Green, G (s) | 13.3 | 13.3 | 92.7 | | | 92.7 |
| Effective Green, g (s) | 16.3 | 16.3 | 95.7 | | | 95.7 |
| Actuated g/C Ratio | 0.14 | 0.14 | 0.80 | | | 0.80 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 448 | 197 | 2660 | | | 2712 |
| v/s Ratio Prot | c0.06 | | c0.25 | | | 0.24 |
| v/s Ratio Perm | | | 0.05 | | | |
| v/c Ratio | 0.42 | 0.39 | 0.31 | | | 0.31 |
| Uniform Delay, d1 | 47.5 | 47.3 | 3.3 | | | 3.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | | | 1.27 |
| Incremental Delay, d2 | 0.6 | 1.3 | 0.3 | | | 0.3 |
| Delay (s) | 48.1 | 48.6 | 3.5 | | | 4.4 |
| Level of Service | D | D | A | | | A |
| Approach Delay (s) | 48.4 | | 3.5 | | | 4.4 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 12.8 | HCM Level of Service | | B | |
| HCM Volume to Capacity ratio | | 0.33 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 40.4% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

15: WOODLANDS & BRONTE

EXISTING

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|-------|----------------------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 22 | 62 | 1591 | 2 | 10 | 920 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1566 | 1521 | 3400 | 1597 | 1785 | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.12 | 1.00 |
| Satd. Flow (perm) | 1566 | 1521 | 3400 | 1597 | 223 | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 24 | 67 | 1729 | 2 | 11 | 1000 |
| RTOR Reduction (vph) | 0 | 49 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 24 | 18 | 1729 | 2 | 11 | 1000 |
| Heavy Vehicles (%) | 14% | 5% | 5% | 0% | 0% | 5% |
| Turn Type | custom | | | Perm | Perm | |
| Protected Phases | | | 2 | | | 6 |
| Permitted Phases | 8 | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 6.6 | 6.6 | 99.4 | 99.4 | 99.4 | 99.4 |
| Effective Green, g (s) | 9.6 | 9.6 | 102.4 | 102.4 | 102.4 | 102.4 |
| Actuated g/C Ratio | 0.08 | 0.08 | 0.85 | 0.85 | 0.85 | 0.85 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 125 | 122 | 2901 | 1363 | 190 | 2901 |
| v/s Ratio Prot | | | c0.51 | | | 0.29 |
| v/s Ratio Perm | c0.02 | 0.01 | | 0.00 | 0.05 | |
| v/c Ratio | 0.19 | 0.15 | 0.60 | 0.00 | 0.06 | 0.34 |
| Uniform Delay, d1 | 51.6 | 51.4 | 2.6 | 1.3 | 1.4 | 1.8 |
| Progression Factor | 1.00 | 1.00 | 0.24 | 0.27 | 0.76 | 0.76 |
| Incremental Delay, d2 | 0.8 | 0.6 | 0.7 | 0.0 | 0.6 | 0.3 |
| Delay (s) | 52.3 | 52.0 | 1.4 | 0.3 | 1.6 | 1.7 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 52.1 | | 1.4 | | | 1.7 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 3.1 | HCM Level of Service | | A | |
| HCM Volume to Capacity ratio | | 0.56 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 54.5% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\pmExist.syn

HCM Signalized Intersection Capacity Analysis

6: WB OFF RAMP & BRONTE

EXISTING

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 223 | 352 | 1492 | 0 | 0 | 603 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 1.00 | 0.95 | | | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3298 | 1452 | 3336 | | | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3298 | 1452 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 242 | 383 | 1622 | 0 | 0 | 655 |
| RTOR Reduction (vph) | 0 | 19 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 242 | 364 | 1622 | 0 | 0 | 655 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |
| Turn Type | Perm | | | | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | 8 | | | |
| Actuated Green, G (s) | 33.2 | 33.2 | 72.8 | | | 72.8 |
| Effective Green, g (s) | 36.2 | 36.2 | 75.8 | | | 75.8 |
| Actuated g/C Ratio | 0.30 | 0.30 | 0.63 | | | 0.63 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 995 | 438 | 2107 | | | 2148 |
| v/s Ratio Prot | 0.07 | | c0.49 | | | 0.19 |
| v/s Ratio Perm | | | c0.25 | | | |
| v/c Ratio | 0.24 | 0.83 | 0.77 | | | 0.30 |
| Uniform Delay, d1 | 31.6 | 39.1 | 15.8 | | | 10.1 |
| Progression Factor | 1.00 | 1.00 | 0.51 | | | 0.96 |
| Incremental Delay, d2 | 0.1 | 12.6 | 0.9 | | | 0.4 |
| Delay (s) | 31.7 | 51.7 | 9.1 | | | 10.0 |
| Level of Service | C | D | A | | | B |
| Approach Delay (s) | 44.0 | | 9.1 | | | 10.0 |
| Approach LOS | D | | A | | | B |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 16.8 | HCM Level of Service | | | B |
| HCM Volume to Capacity ratio | | 0.79 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | | 8.0 |
| Intersection Capacity Utilization | | 69.7% | ICU Level of Service | | | C |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

15: WOODLANDS & BRONTE

2019 BACKGROUND

AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|-------|-------|----------------------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 23 | 19 | 898 | 18 | 121 | 1849 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1566 | 1521 | 3400 | 1597 | 1785 | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.29 | 1.00 |
| Satd. Flow (perm) | 1566 | 1521 | 3400 | 1597 | 539 | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 25 | 21 | 976 | 20 | 132 | 2010 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 3 | 0 | 0 |
| Lane Group Flow (vph) | 25 | 1 | 976 | 17 | 132 | 2010 |
| Heavy Vehicles (%) | 14% | 5% | 5% | 0% | 0% | 5% |
| Turn Type | custom | | | Perm | Perm | |
| Protected Phases | | | 2 | | | 6 |
| Permitted Phases | 8 | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 5.1 | 5.1 | 100.9 | 100.9 | 100.9 | 100.9 |
| Effective Green, g (s) | 8.1 | 8.1 | 103.9 | 103.9 | 103.9 | 103.9 |
| Actuated g/C Ratio | 0.07 | 0.07 | 0.87 | 0.87 | 0.87 | 0.87 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 106 | 103 | 2944 | 1383 | 467 | 2944 |
| v/s Ratio Prot | | | 0.29 | | | c0.59 |
| v/s Ratio Perm | c0.02 | 0.00 | | 0.01 | 0.25 | |
| v/c Ratio | 0.24 | 0.01 | 0.33 | 0.01 | 0.28 | 0.68 |
| Uniform Delay, d1 | 53.0 | 52.2 | 1.5 | 1.1 | 1.4 | 2.6 |
| Progression Factor | 1.00 | 1.00 | 1.48 | 2.21 | 0.95 | 0.76 |
| Incremental Delay, d2 | 1.1 | 0.1 | 0.3 | 0.0 | 0.9 | 0.8 |
| Delay (s) | 54.2 | 52.3 | 2.5 | 2.4 | 2.3 | 2.8 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 53.3 | | 2.5 | | | 2.8 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 3.4 | | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | 0.65 | | | | |
| Actuated Cycle Length (s) | | 120.0 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 61.1% | | ICU Level of Service | | B |
| Analysis Period (min) | | 15 | | | | |

c = Critical Lane Group

HCM Signalized Intersection Capacity Analysis

6: WB OFF RAMP & BRONTE

2019 BACKGROUND

AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|----------------------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 198 | 238 | 884 | 0 | 0 | 884 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.95 | | | 0.95 |
| Fr _t | 0.95 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3140 | 1321 | 3336 | | | 3400 |
| Flt Permitted | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3140 | 1321 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 215 | 259 | 961 | 0 | 0 | 961 |
| RTOR Reduction (vph) | 66 | 128 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 258 | 23 | 961 | 0 | 0 | 961 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |
| Turn Type | Perm | | | | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | 8 | | | | |
| Actuated Green, G (s) | 15.0 | 15.0 | 91.0 | | | 91.0 |
| Effective Green, g (s) | 18.0 | 18.0 | 94.0 | | | 94.0 |
| Actuated g/C Ratio | 0.15 | 0.15 | 0.78 | | | 0.78 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 471 | 198 | 2613 | | | 2663 |
| v/s Ratio Prot | c0.08 | | c0.29 | | | 0.28 |
| v/s Ratio Perm | | 0.02 | | | | |
| v/c Ratio | 0.55 | 0.11 | 0.37 | | | 0.36 |
| Uniform Delay, d1 | 47.2 | 44.1 | 4.0 | | | 3.9 |
| Progression Factor | 1.00 | 1.00 | 0.40 | | | 1.15 |
| Incremental Delay, d2 | 1.3 | 0.3 | 0.3 | | | 0.3 |
| Delay (s) | 48.5 | 44.4 | 1.9 | | | 4.8 |
| Level of Service | D | D | A | | | A |
| Approach Delay (s) | 47.2 | | 1.9 | | | 4.8 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 12.0 | HCM Level of Service | | B | |
| HCM Volume to Capacity ratio | | 0.40 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 40.9% | ICU Level of Service | | A | |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\am2019Back.syn

HCM Signalized Intersection Capacity Analysis

6: WB OFF RAMP & BRONTE

2019 BACKGROUND

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 259 | 408 | 1731 | 0 | 0 | 699 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.95 | | | 0.95 |
| Fr _t | 0.94 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3094 | 1321 | 3336 | | | 3400 |
| Flt Permitted | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3094 | 1321 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 282 | 443 | 1882 | 0 | 0 | 760 |
| RTOR Reduction (vph) | 20 | 20 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 475 | 210 | 1882 | 0 | 0 | 760 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |
| Turn Type | Perm | | | | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | 8 | | | |
| Actuated Green, G (s) | 23.3 | 23.3 | 82.7 | | | 82.7 |
| Effective Green, g (s) | 26.3 | 26.3 | 85.7 | | | 85.7 |
| Actuated g/C Ratio | 0.22 | 0.22 | 0.71 | | | 0.71 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 678 | 290 | 2382 | | | 2428 |
| v/s Ratio Prot | 0.15 | | c0.56 | | | 0.22 |
| v/s Ratio Perm | | | c0.16 | | | |
| v/c Ratio | 0.70 | 0.72 | 0.79 | | | 0.31 |
| Uniform Delay, d1 | 43.2 | 43.5 | 11.2 | | | 6.3 |
| Progression Factor | 1.00 | 1.00 | 0.32 | | | 1.17 |
| Incremental Delay, d2 | 3.3 | 8.6 | 1.8 | | | 0.3 |
| Delay (s) | 46.5 | 52.1 | 5.4 | | | 7.7 |
| Level of Service | D | D | A | | | A |
| Approach Delay (s) | 48.3 | | 5.4 | | | 7.7 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 15.2 | HCM Level of Service | | B | |
| HCM Volume to Capacity ratio | | 0.77 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 71.4% | ICU Level of Service | | C | |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

Baseline

%user_name%

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Back.syn

Synchro 7 - Report

HCM Signalized Intersection Capacity Analysis

3: EB OFF RAMP & BRONTE

2019 BACKGROUND

PM PEAK HOUR



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|------|------|------|-------|------|-------|-------|------|
| Lane Configurations | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| Volume (vph) | 6 | 7 | 4 | 295 | 4 | 634 | 4 | 1373 | 254 | 238 | 850 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.95 | | 1.00 | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1782 | 1785 | | 1700 | 1340 | 1335 | 1785 | 3336 | 1551 | 1653 | 3398 | |
| Flt Permitted | 0.69 | 1.00 | | 0.59 | 1.00 | 1.00 | 0.31 | 1.00 | 1.00 | 0.06 | 1.00 | |
| Satd. Flow (perm) | 1294 | 1785 | | 1053 | 1340 | 1335 | 578 | 3336 | 1551 | 112 | 3398 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 7 | 8 | 4 | 321 | 4 | 689 | 4 | 1492 | 276 | 259 | 924 | 4 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 182 | 182 | 0 | 0 | 93 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 7 | 8 | 0 | 321 | 167 | 162 | 4 | 1492 | 183 | 259 | 928 | 0 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | | | | | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 5% | 0% | 12% | 0% | 7% | 3% | 8% | 5% | 0% |
| Turn Type | Perm | | | pm+pt | | | Perm | Perm | | Perm | pm+pt | |
| Protected Phases | | 4 | | | 3 | 8 | | | 2 | | 1 | 6 |
| Permitted Phases | 4 | | | | 8 | | 8 | 2 | | 2 | | 6 |
| Actuated Green, G (s) | 2.8 | 2.8 | | 26.2 | 26.2 | 59.3 | 59.3 | 59.3 | 79.8 | 79.8 | | |
| Effective Green, g (s) | 5.8 | 5.8 | | 27.2 | 29.2 | 62.3 | 62.3 | 62.3 | 79.8 | 82.8 | | |
| Actuated g/C Ratio | 0.05 | 0.05 | | 0.23 | 0.24 | 0.52 | 0.52 | 0.52 | 0.66 | 0.69 | | |
| Clearance Time (s) | 7.0 | 7.0 | | 4.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 63 | 86 | | 349 | 326 | 325 | 300 | 1732 | 805 | 299 | 2345 | |
| v/s Ratio Prot | | 0.00 | | c0.16 | 0.12 | | | c0.45 | | c0.13 | 0.27 | |
| v/s Ratio Perm | 0.01 | | | c0.05 | | 0.12 | 0.01 | | 0.12 | 0.45 | | |
| v/c Ratio | 0.11 | 0.10 | | 0.92 | 0.51 | 0.50 | 0.01 | 0.86 | 0.23 | 0.87 | 0.40 | |
| Uniform Delay, d1 | 54.6 | 54.6 | | 44.4 | 39.3 | 39.1 | 14.0 | 25.1 | 15.7 | 37.1 | 7.9 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.22 | 0.66 | |
| Incremental Delay, d2 | 0.8 | 0.5 | | 28.4 | 1.4 | 1.2 | 0.1 | 5.9 | 0.7 | 21.3 | 0.5 | |
| Delay (s) | 55.4 | 55.1 | | 72.8 | 40.6 | 40.3 | 14.0 | 31.0 | 16.4 | 66.4 | 5.7 | |
| Level of Service | E | E | | E | D | D | B | C | B | E | A | |
| Approach Delay (s) | | 55.2 | | | 50.7 | | | 28.7 | | | 19.0 | |
| Approach LOS | | | E | | D | | | C | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 31.5 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.85 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 10.0 |
| Intersection Capacity Utilization | 84.1% | ICU Level of Service | E |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis

18: UPPER MIDDLE & BRONTE

2019 TOTAL

AM PEAK HOUR



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|-------|-------|------|------|------|------|-------|------|-------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ | ↑ ↗ | ↑ ↘ | ↑ ↙ | ↑ ↖ |
| Volume (vph) | 14 | 123 | 228 | 314 | 47 | 160 | 46 | 752 | 257 | 316 | 1489 | 11 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 0.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1785 | 1879 | 1597 | 3395 | 1879 | 1566 | 1785 | 3336 | 1536 | 1750 | 3433 | 1597 |
| Flt Permitted | 0.72 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.25 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1360 | 1879 | 1597 | 3395 | 1879 | 1566 | 180 | 3336 | 1536 | 465 | 3433 | 1597 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 134 | 248 | 341 | 51 | 174 | 50 | 817 | 279 | 343 | 1618 | 12 |
| RTOR Reduction (vph) | 0 | 0 | 24 | 0 | 0 | 118 | 0 | 0 | 144 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 15 | 134 | 224 | 341 | 51 | 56 | 50 | 817 | 135 | 343 | 1618 | 8 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 2% | 0% | 2% | 0% | 7% | 4% | 2% | 4% | 0% |
| Turn Type | Perm | Perm | Prot | | Perm | Perm | | Perm | pm+pt | | Perm | |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 17.3 | 17.3 | 17.3 | 13.0 | 35.3 | 35.3 | 55.1 | 55.1 | 55.1 | 70.7 | 70.7 | 70.7 |
| Effective Green, g (s) | 20.3 | 20.3 | 20.3 | 15.0 | 38.3 | 38.3 | 58.1 | 58.1 | 58.1 | 73.7 | 73.7 | 73.7 |
| Actuated g/C Ratio | 0.17 | 0.17 | 0.17 | 0.12 | 0.32 | 0.32 | 0.48 | 0.48 | 0.48 | 0.61 | 0.61 | 0.61 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 230 | 318 | 270 | 424 | 600 | 500 | 87 | 1615 | 744 | 453 | 2108 | 981 |
| v/s Ratio Prot | | 0.07 | | c0.10 | 0.03 | | | 0.24 | | 0.10 | c0.47 | |
| v/s Ratio Perm | 0.01 | | c0.14 | | | 0.04 | 0.28 | | 0.09 | 0.37 | | 0.01 |
| v/c Ratio | 0.07 | 0.42 | 0.83 | 0.80 | 0.08 | 0.11 | 0.57 | 0.51 | 0.18 | 0.76 | 0.77 | 0.01 |
| Uniform Delay, d1 | 41.9 | 44.6 | 48.2 | 51.1 | 28.6 | 28.8 | 22.1 | 21.1 | 17.5 | 13.3 | 16.9 | 9.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 0.75 | 0.75 | 0.62 | 1.30 | 1.37 | 5.71 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.1 | 0.9 | 18.6 | 10.4 | 0.1 | 0.1 | 23.6 | 1.1 | 0.5 | 7.1 | 2.7 | 0.0 |
| Delay (s) | 42.0 | 45.5 | 66.7 | 48.5 | 21.6 | 18.1 | 52.3 | 30.1 | 100.4 | 20.4 | 19.6 | 9.0 |
| Level of Service | D | D | E | D | C | B | D | C | F | C | B | A |
| Approach Delay (s) | | 58.6 | | | 36.7 | | | 48.2 | | | 19.7 | |
| Approach LOS | | E | | | D | | | D | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|------|
| HCM Average Control Delay | 33.8 | HCM Level of Service | C |
| HCM Volume to Capacity ratio | 0.78 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 11.0 |
| Intersection Capacity Utilization | 74.2% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis
27: NORTH ACCESS & BRONTE

2019 TOTAL
AM PEAK HOUR

| |  |  |  |  |  |  |
|-----------------------------------|-----------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations |  |  |  |  |  |  |
| Volume (vph) | 35 | 43 | 1012 | 11 | 14 | 2017 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1750 | 1566 | 3368 | 1566 | 1750 | 3368 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.25 | 1.00 |
| Satd. Flow (perm) | 1750 | 1566 | 3368 | 1566 | 457 | 3368 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 38 | 47 | 1100 | 12 | 15 | 2192 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 2 | 0 | 0 |
| Lane Group Flow (vph) | 38 | 4 | 1100 | 10 | 15 | 2192 |
| Heavy Vehicles (%) | 2% | 2% | 6% | 2% | 2% | 6% |
| Turn Type | Perm | | Perm | Perm | | |
| Protected Phases | 8 | | 2 | | 6 | |
| Permitted Phases | | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 7.0 | 7.0 | 99.0 | 99.0 | 99.0 | 99.0 |
| Effective Green, g (s) | 10.0 | 10.0 | 102.0 | 102.0 | 102.0 | 102.0 |
| Actuated g/C Ratio | 0.08 | 0.08 | 0.85 | 0.85 | 0.85 | 0.85 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 146 | 131 | 2863 | 1331 | 388 | 2863 |
| v/s Ratio Prot | c0.02 | | 0.33 | | c0.65 | |
| v/s Ratio Perm | | 0.00 | | 0.01 | 0.03 | |
| v/c Ratio | 0.26 | 0.03 | 0.38 | 0.01 | 0.04 | 0.77 |
| Uniform Delay, d ₁ | 51.5 | 50.5 | 2.0 | 1.4 | 1.4 | 3.9 |
| Progression Factor | 1.00 | 1.00 | 0.94 | 1.26 | 0.57 | 0.87 |
| Incremental Delay, d ₂ | 1.0 | 0.1 | 0.4 | 0.0 | 0.1 | 1.2 |
| Delay (s) | 52.5 | 50.6 | 2.2 | 1.7 | 0.9 | 4.6 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 51.5 | | 2.2 | | 4.6 | |
| Approach LOS | D | | A | | A | |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 5.0 | | HCM Level of Service | A | |
| HCM Volume to Capacity ratio | | 0.72 | | | | |
| Actuated Cycle Length (s) | | 120.0 | | Sum of lost time (s) | 8.0 | |
| Intersection Capacity Utilization | | 65.8% | | ICU Level of Service | C | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

25: SOUTH ACCESS & BRONTE

2019 TOTAL

AM PEAK HOUR

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|------|----------------------|------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 269 | 95 | 931 | 90 | 36 | 2022 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1750 | 1566 | 3368 | 1566 | 1750 | 3466 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.25 | 1.00 |
| Satd. Flow (perm) | 1750 | 1566 | 3368 | 1566 | 462 | 3466 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 292 | 103 | 1012 | 98 | 39 | 2198 |
| RTOR Reduction (vph) | 0 | 81 | 0 | 27 | 0 | 0 |
| Lane Group Flow (vph) | 292 | 22 | 1012 | 71 | 39 | 2198 |
| Heavy Vehicles (%) | 2% | 2% | 6% | 2% | 2% | 3% |
| Turn Type | | Perm | | Perm | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 22.3 | 22.3 | 83.7 | 83.7 | 83.7 | 83.7 |
| Effective Green, g (s) | 25.3 | 25.3 | 86.7 | 86.7 | 86.7 | 86.7 |
| Actuated g/C Ratio | 0.21 | 0.21 | 0.72 | 0.72 | 0.72 | 0.72 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 369 | 330 | 2433 | 1131 | 334 | 2504 |
| v/s Ratio Prot | c0.17 | | 0.30 | | | c0.63 |
| v/s Ratio Perm | | 0.01 | | 0.05 | 0.08 | |
| v/c Ratio | 0.79 | 0.07 | 0.42 | 0.06 | 0.12 | 0.88 |
| Uniform Delay, d1 | 44.8 | 37.9 | 6.6 | 4.8 | 5.0 | 12.6 |
| Progression Factor | 1.00 | 1.00 | 1.64 | 3.57 | 0.89 | 0.53 |
| Incremental Delay, d2 | 11.0 | 0.1 | 0.5 | 0.1 | 0.5 | 3.2 |
| Delay (s) | 55.9 | 38.0 | 11.3 | 17.4 | 4.9 | 9.8 |
| Level of Service | E | D | B | B | A | A |
| Approach Delay (s) | 51.2 | | 11.9 | | | 9.8 |
| Approach LOS | D | | B | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 14.8 | | HCM Level of Service | | B |
| HCM Volume to Capacity ratio | | 0.86 | | | | |
| Actuated Cycle Length (s) | | 120.0 | | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | 77.5% | | ICU Level of Service | | D |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

Baseline

%user_name%

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\am2019Total.syn

Synchro 7 - Report

HCM Signalized Intersection Capacity Analysis

15: WOODLANDS & BRONTE

2019 TOTAL

AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|------|-------|----------------------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 23 | 19 | 996 | 18 | 121 | 2145 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1566 | 1521 | 3400 | 1597 | 1785 | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.26 | 1.00 |
| Satd. Flow (perm) | 1566 | 1521 | 3400 | 1597 | 479 | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 25 | 21 | 1083 | 20 | 132 | 2332 |
| RTOR Reduction (vph) | 0 | 20 | 0 | 3 | 0 | 0 |
| Lane Group Flow (vph) | 25 | 1 | 1083 | 17 | 132 | 2332 |
| Heavy Vehicles (%) | 14% | 5% | 5% | 0% | 0% | 5% |
| Turn Type | custom | | Perm | Perm | | |
| Protected Phases | | | 2 | | | 6 |
| Permitted Phases | 8 | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 5.1 | 5.1 | 100.9 | 100.9 | 100.9 | 100.9 |
| Effective Green, g (s) | 8.1 | 8.1 | 103.9 | 103.9 | 103.9 | 103.9 |
| Actuated g/C Ratio | 0.07 | 0.07 | 0.87 | 0.87 | 0.87 | 0.87 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 106 | 103 | 2944 | 1383 | 415 | 2944 |
| v/s Ratio Prot | | | 0.32 | | | c0.69 |
| v/s Ratio Perm | c0.02 | 0.00 | | 0.01 | 0.28 | |
| v/c Ratio | 0.24 | 0.01 | 0.37 | 0.01 | 0.32 | 0.79 |
| Uniform Delay, d1 | 53.0 | 52.2 | 1.6 | 1.1 | 1.5 | 3.4 |
| Progression Factor | 1.00 | 1.00 | 1.69 | 2.53 | 1.04 | 0.61 |
| Incremental Delay, d2 | 1.1 | 0.1 | 0.3 | 0.0 | 1.0 | 1.1 |
| Delay (s) | 54.2 | 52.3 | 3.0 | 2.8 | 2.5 | 3.2 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 53.3 | | 3.0 | | | 3.2 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | | 3.8 | HCM Level of Service | | A |
| HCM Volume to Capacity ratio | | | 0.75 | | | |
| Actuated Cycle Length (s) | | | 120.0 | Sum of lost time (s) | | 8.0 |
| Intersection Capacity Utilization | | | 69.3% | ICU Level of Service | | C |
| Analysis Period (min) | | | 15 | | | |

c = Critical Lane Group

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\am2019Total.syn

HCM Signalized Intersection Capacity Analysis
6: WB OFF RAMP & BRONTE

2019 TOTAL
AM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------|------|------|------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 198 | 284 | 921 | 0 | 0 | 1068 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.95 | | | 0.95 |
| Fr _t | 0.94 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3110 | 1321 | 3336 | | | 3400 |
| Flt Permitted | 0.97 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3110 | 1321 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 215 | 309 | 1001 | 0 | 0 | 1161 |
| RTOR Reduction (vph) | 116 | 129 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 241 | 38 | 1001 | 0 | 0 | 1161 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |

| Turn Type | Perm | | |
|------------------------|-------|------|-------|
| Protected Phases | 8 | 2 | 6 |
| Permitted Phases | | 8 | |
| Actuated Green, G (s) | 14.3 | 14.3 | 91.7 |
| Effective Green, g (s) | 17.3 | 17.3 | 94.7 |
| Actuated g/C Ratio | 0.14 | 0.14 | 0.79 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 448 | 190 | 2633 |
| v/s Ratio Prot | c0.08 | 0.30 | c0.34 |
| v/s Ratio Perm | | 0.03 | |
| v/c Ratio | 0.54 | 0.20 | 0.38 |
| Uniform Delay, d1 | 47.6 | 45.2 | 3.8 |
| Progression Factor | 1.00 | 1.00 | 0.51 |
| Incremental Delay, d2 | 1.3 | 0.5 | 0.3 |
| Delay (s) | 48.9 | 45.8 | 2.3 |
| Level of Service | D | D | A |
| Approach Delay (s) | 47.9 | | 2.3 |
| Approach LOS | D | A | A |

| Intersection Summary | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 11.9 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.45 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 44.8% | ICU Level of Service | A |
| Analysis Period (min) | 15 | | |

c = Critical Lane Group

HCM Signalized Intersection Capacity Analysis

3: EB OFF RAMP & BRONTE

2019 TOTAL

AM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|------|-------|-------|------|-------|----------------------|-------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 9 | 10 | 3 | 482 | 6 | 551 | 1 | 762 | 312 | 556 | 1086 | 13 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | | 2.0 | 3.0 | 0.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Fr _t | 1.00 | 0.97 | | 1.00 | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1785 | 1818 | | 1668 | 1413 | 1405 | 1785 | 3305 | 1529 | 1750 | 3428 | |
| Flt Permitted | 0.56 | 1.00 | | 0.55 | 1.00 | 1.00 | 0.24 | 1.00 | 1.00 | 0.14 | 1.00 | |
| Satd. Flow (perm) | 1061 | 1818 | | 959 | 1413 | 1405 | 444 | 3305 | 1529 | 249 | 3428 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 10 | 11 | 3 | 524 | 7 | 599 | 1 | 828 | 339 | 604 | 1180 | 14 |
| RTOR Reduction (vph) | 0 | 3 | 0 | 0 | 192 | 5 | 0 | 0 | 215 | 0 | 1 | 0 |
| Lane Group Flow (vph) | 10 | 11 | 0 | 524 | 116 | 294 | 1 | 828 | 124 | 604 | 1193 | 0 |
| Confl. Peds. (#/hr) | | | | | | | | | | 1 | 1 | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 7% | 0% | 8% | 0% | 8% | 2% | 2% | 4% | 0% |
| Turn Type | Perm | | | pm+pt | | pm+ov | Perm | | Perm | pm+pt | | |
| Protected Phases | | 4 | | | 3 | 8 | 1 | | 2 | | 1 | 6 |
| Permitted Phases | 4 | | | | 8 | | 8 | 2 | | 2 | 6 | |
| Actuated Green, G (s) | 4.4 | 4.4 | | 40.4 | 40.4 | 77.4 | 26.6 | 26.6 | 26.6 | 66.6 | 66.6 | |
| Effective Green, g (s) | 7.4 | 7.4 | | 41.4 | 43.4 | 83.4 | 29.6 | 29.6 | 29.6 | 66.6 | 69.6 | |
| Actuated g/C Ratio | 0.06 | 0.06 | | 0.34 | 0.36 | 0.70 | 0.25 | 0.25 | 0.25 | 0.55 | 0.58 | |
| Clearance Time (s) | 6.0 | 6.0 | | 3.0 | 6.0 | 3.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 65 | 112 | | 532 | 511 | 976 | 110 | 815 | 377 | 601 | 1988 | |
| v/s Ratio Prot | | 0.01 | | c0.28 | 0.08 | 0.10 | | c0.25 | | c0.31 | 0.35 | |
| v/s Ratio Perm | 0.01 | | | | 0.06 | | 0.11 | 0.00 | | 0.08 | 0.25 | |
| v/c Ratio | 0.15 | 0.10 | | 0.98 | 0.23 | 0.30 | 0.01 | 1.02 | 0.33 | 1.00 | 0.60 | |
| Uniform Delay, d ₁ | 53.3 | 53.2 | | 37.7 | 26.6 | 7.1 | 34.1 | 45.2 | 37.0 | 34.0 | 16.2 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.99 | |
| Incremental Delay, d ₂ | 1.1 | 0.4 | | 34.9 | 0.2 | 0.2 | 0.2 | 35.6 | 2.3 | 37.2 | 1.3 | |
| Delay (s) | 54.4 | 53.5 | | 72.6 | 26.9 | 7.2 | 34.3 | 80.8 | 39.4 | 69.6 | 17.3 | |
| Level of Service | D | D | | E | C | A | C | F | D | E | B | |
| Approach Delay (s) | | | 53.9 | | | 42.9 | | | 68.7 | | 34.9 | |
| Approach LOS | | | D | | | D | | | E | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | | 46.8 | | | | HCM Level of Service | | | D | | |
| HCM Volume to Capacity ratio | | | 0.95 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 120.0 | | | | Sum of lost time (s) | | | 9.0 | | |
| Intersection Capacity Utilization | | | 95.2% | | | | ICU Level of Service | | | F | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\am2019Total.syn

HCM Signalized Intersection Capacity Analysis

18: UPPER MIDDLE & BRONTE

2019 TOTAL

PM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|-------|------|------|-------|------|-------|------|-------|------|------|
| Lane Configurations | ↑ | ↑↑ | | ↑↑ | ↑ | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ | ↑ |
| Volume (vph) | 17 | 31 | 95 | 233 | 78 | 233 | 137 | 1506 | 329 | 207 | 879 | 34 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 0.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | | 0.97 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Fr _t | 1.00 | 0.89 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1785 | 3167 | | 3395 | 1879 | 1566 | 1785 | 3336 | 1536 | 1750 | 3433 | 1597 |
| Flt Permitted | 0.70 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.30 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1319 | 3167 | | 3395 | 1879 | 1566 | 563 | 3336 | 1536 | 115 | 3433 | 1597 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 18 | 34 | 103 | 253 | 85 | 253 | 149 | 1637 | 358 | 225 | 955 | 37 |
| RTOR Reduction (vph) | 0 | 94 | 0 | 0 | 0 | 143 | 0 | 0 | 87 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 18 | 43 | 0 | 253 | 85 | 110 | 149 | 1637 | 271 | 225 | 955 | 27 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 2% | 0% | 2% | 0% | 7% | 4% | 2% | 4% | 0% |
| Turn Type | Perm | | Prot | | Perm | Perm | | Perm | Perm | pm+pt | | Perm |
| Protected Phases | | 4 | | 3 | 8 | | | 2 | | 1 | | 6 |
| Permitted Phases | 4 | | | | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | 7.3 | 7.3 | | 8.0 | 20.3 | 20.3 | 67.6 | 67.6 | 67.6 | 85.7 | 85.7 | 85.7 |
| Effective Green, g (s) | 10.3 | 10.3 | | 10.0 | 23.3 | 23.3 | 70.6 | 70.6 | 70.6 | 88.7 | 88.7 | 88.7 |
| Actuated g/C Ratio | 0.09 | 0.09 | | 0.08 | 0.19 | 0.19 | 0.59 | 0.59 | 0.59 | 0.74 | 0.74 | 0.74 |
| Clearance Time (s) | 7.0 | 7.0 | | 5.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 113 | 272 | | 283 | 365 | 304 | 331 | 1963 | 904 | 332 | 2538 | 1180 |
| v/s Ratio Prot | 0.01 | | c0.07 | 0.05 | | | | c0.49 | | c0.10 | 0.28 | |
| v/s Ratio Perm | 0.01 | | | | | c0.07 | 0.26 | | 0.18 | 0.40 | | 0.02 |
| v/c Ratio | 0.16 | 0.16 | | 0.89 | 0.23 | 0.36 | 0.45 | 0.83 | 0.30 | 0.68 | 0.38 | 0.02 |
| Uniform Delay, d1 | 50.8 | 50.8 | | 54.5 | 40.8 | 41.9 | 13.8 | 20.0 | 12.3 | 32.1 | 5.7 | 4.2 |
| Progression Factor | 1.00 | 1.00 | | 0.72 | 0.76 | 0.96 | 0.95 | 0.82 | 1.12 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.7 | 0.3 | | 27.1 | 0.3 | 0.7 | 3.0 | 3.1 | 0.6 | 5.4 | 0.4 | 0.0 |
| Delay (s) | 51.5 | 51.1 | | 66.5 | 31.5 | 41.0 | 16.2 | 19.4 | 14.4 | 37.5 | 6.1 | 4.2 |
| Level of Service | D | D | E | C | D | B | B | B | D | A | A | |
| Approach Delay (s) | | 51.1 | | | 50.6 | | | 18.4 | | | 11.8 | |
| Approach LOS | | D | | | D | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 22.3 | | | | | | | | C | | |
| HCM Volume to Capacity ratio | | 0.73 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | | | | | | 7.0 | | | |
| Intersection Capacity Utilization | | 77.0% | | | | | | | | D | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

HCM Signalized Intersection Capacity Analysis
27: NORTH ACCESS & BRONTE

2019 TOTAL
PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|----------------------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 23 | 28 | 1943 | 36 | 46 | 1160 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1750 | 1566 | 3368 | 1566 | 1750 | 3368 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.07 | 1.00 |
| Satd. Flow (perm) | 1750 | 1566 | 3368 | 1566 | 131 | 3368 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 25 | 30 | 2112 | 39 | 50 | 1261 |
| RTOR Reduction (vph) | 0 | 25 | 0 | 6 | 0 | 0 |
| Lane Group Flow (vph) | 25 | 5 | 2112 | 33 | 50 | 1261 |
| Heavy Vehicles (%) | 2% | 2% | 6% | 2% | 2% | 6% |
| Turn Type | Perm | | Perm | Perm | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 6.2 | 6.2 | 99.8 | 99.8 | 99.8 | 99.8 |
| Effective Green, g (s) | 9.2 | 9.2 | 102.8 | 102.8 | 102.8 | 102.8 |
| Actuated g/C Ratio | 0.08 | 0.08 | 0.86 | 0.86 | 0.86 | 0.86 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 134 | 120 | 2885 | 1342 | 112 | 2885 |
| v/s Ratio Prot | c0.01 | | c0.63 | | | 0.37 |
| v/s Ratio Perm | | 0.00 | | 0.02 | 0.38 | |
| v/c Ratio | 0.19 | 0.04 | 0.73 | 0.02 | 0.45 | 0.44 |
| Uniform Delay, d1 | 51.9 | 51.3 | 3.3 | 1.3 | 2.0 | 2.0 |
| Progression Factor | 1.00 | 1.00 | 0.51 | 1.12 | 0.96 | 0.71 |
| Incremental Delay, d2 | 0.7 | 0.1 | 0.8 | 0.0 | 11.2 | 0.4 |
| Delay (s) | 52.6 | 51.5 | 2.5 | 1.4 | 13.1 | 1.8 |
| Level of Service | D | D | A | A | B | A |
| Approach Delay (s) | 52.0 | | 2.4 | | | 2.3 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 3.1 | HCM Level of Service | | A | |
| HCM Volume to Capacity ratio | | 0.69 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 63.7% | ICU Level of Service | | B | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

HCM Signalized Intersection Capacity Analysis

25: SOUTH ACCESS & BRONTE

2019 TOTAL

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|-------|-------|----------------------|-------|-------|------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 178 | 75 | 1920 | 301 | 110 | 1083 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1750 | 1566 | 3368 | 1566 | 1750 | 3466 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.05 | 1.00 |
| Satd. Flow (perm) | 1750 | 1566 | 3368 | 1566 | 88 | 3466 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 193 | 82 | 2087 | 327 | 120 | 1177 |
| RTOR Reduction (vph) | 0 | 70 | 0 | 55 | 0 | 0 |
| Lane Group Flow (vph) | 193 | 12 | 2087 | 272 | 120 | 1177 |
| Heavy Vehicles (%) | 2% | 2% | 6% | 2% | 2% | 3% |
| Turn Type | Perm | | Perm | pm+pt | | |
| Protected Phases | 8 | | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 15.2 | 15.2 | 79.9 | 79.9 | 90.8 | 90.8 |
| Effective Green, g (s) | 18.2 | 18.2 | 82.9 | 82.9 | 91.8 | 93.8 |
| Actuated g/C Ratio | 0.15 | 0.15 | 0.69 | 0.69 | 0.76 | 0.78 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 4.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 265 | 238 | 2327 | 1082 | 177 | 2709 |
| v/s Ratio Prot | c0.11 | | c0.62 | | c0.04 | 0.34 |
| v/s Ratio Perm | | 0.01 | | 0.17 | 0.48 | |
| v/c Ratio | 0.73 | 0.05 | 0.90 | 0.25 | 0.68 | 0.43 |
| Uniform Delay, d1 | 48.5 | 43.5 | 15.1 | 6.9 | 31.9 | 4.3 |
| Progression Factor | 1.00 | 1.00 | 1.41 | 1.37 | 1.34 | 0.69 |
| Incremental Delay, d2 | 9.6 | 0.1 | 3.8 | 0.3 | 9.2 | 0.5 |
| Delay (s) | 58.1 | 43.6 | 25.1 | 9.9 | 52.0 | 3.5 |
| Level of Service | E | D | C | A | D | A |
| Approach Delay (s) | 53.8 | | 23.0 | | | 7.9 |
| Approach LOS | D | | C | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 20.2 | HCM Level of Service | | C | |
| HCM Volume to Capacity ratio | | 0.85 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 11.0 | |
| Intersection Capacity Utilization | | 79.0% | ICU Level of Service | | D | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

HCM Signalized Intersection Capacity Analysis

15: WOODLANDS & BRONTE

2019 TOTAL

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|--------|-------|----------------------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑↑ | ↑ | ↑ | ↑↑ |
| Volume (vph) | 22 | 62 | 2135 | 2 | 10 | 1211 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |
| Fr _t | 1.00 | 0.85 | 1.00 | 0.85 | 1.00 | 1.00 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | 1566 | 1521 | 3400 | 1597 | 1785 | 3400 |
| Flt Permitted | 0.95 | 1.00 | 1.00 | 1.00 | 0.05 | 1.00 |
| Satd. Flow (perm) | 1566 | 1521 | 3400 | 1597 | 89 | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 24 | 67 | 2321 | 2 | 11 | 1316 |
| RTOR Reduction (vph) | 0 | 16 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 24 | 51 | 2321 | 2 | 11 | 1316 |
| Heavy Vehicles (%) | 14% | 5% | 5% | 0% | 0% | 5% |
| Turn Type | custom | | | Perm | Perm | |
| Protected Phases | | | 2 | | | 6 |
| Permitted Phases | 8 | 8 | | 2 | 6 | |
| Actuated Green, G (s) | 8.3 | 8.3 | 97.7 | 97.7 | 97.7 | 97.7 |
| Effective Green, g (s) | 11.3 | 11.3 | 100.7 | 100.7 | 100.7 | 100.7 |
| Actuated g/C Ratio | 0.09 | 0.09 | 0.84 | 0.84 | 0.84 | 0.84 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 147 | 143 | 2853 | 1340 | 75 | 2853 |
| v/s Ratio Prot | | | c0.68 | | | 0.39 |
| v/s Ratio Perm | 0.02 | c0.03 | | 0.00 | 0.12 | |
| v/c Ratio | 0.16 | 0.35 | 0.81 | 0.00 | 0.15 | 0.46 |
| Uniform Delay, d1 | 50.0 | 50.9 | 4.9 | 1.6 | 1.8 | 2.5 |
| Progression Factor | 1.00 | 1.00 | 0.57 | 1.21 | 1.11 | 1.14 |
| Incremental Delay, d2 | 0.5 | 1.5 | 1.3 | 0.0 | 3.7 | 0.5 |
| Delay (s) | 50.5 | 52.4 | 4.1 | 1.9 | 5.6 | 3.4 |
| Level of Service | D | D | A | A | A | A |
| Approach Delay (s) | 51.9 | | 4.1 | | | 3.4 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 5.0 | HCM Level of Service | | A | |
| HCM Volume to Capacity ratio | | 0.77 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 69.5% | ICU Level of Service | | C | |
| Analysis Period (min) | | 15 | | | | |
| c Critical Lane Group | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

HCM Signalized Intersection Capacity Analysis

8: NSR & BRONTE

2019 TOTAL

PM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|------------------------|------|------|------|-------|------|-------|------|------|-------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 1 | 0 | 0 | 124 | 0 | 156 | 1 | 2017 | 46 | 52 | 1196 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | | | 4.0 | | 3.0 | 4.0 | 4.0 | 4.0 | 0.0 | 4.0 | 4.0 |
| Lane Util. Factor | | | | 1.00 | | 0.95 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 0.95 |
| Fr _t | | | | 1.00 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 |
| Flt Protected | | | | 0.95 | | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 0.95 | 1.00 |
| Satd. Flow (prot) | | | | 1785 | | 1615 | 1615 | 1439 | 1785 | 3275 | 1566 | 1733 |
| Flt Permitted | | | | 0.71 | | 0.85 | 0.76 | 1.00 | 0.17 | 1.00 | 1.00 | 0.05 |
| Satd. Flow (perm) | | | | 1335 | | 1440 | 1287 | 1439 | 320 | 3275 | 1566 | 85 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 1 | 0 | 0 | 135 | 0 | 170 | 1 | 2192 | 50 | 57 | 1300 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 7 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 1 | 0 | 67 | 68 | 159 | 1 | 2192 | 43 | 57 | 1300 | 0 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 5% | 0% | 11% | 0% | 9% | 2% | 3% | 6% | 0% |
| Turn Type | Perm | | | pm+pt | | | Perm | Perm | | pm+ov | | Perm |
| Protected Phases | | 4 | | | 3 | 8 | | | 2 | 3 | | 6 |
| Permitted Phases | 4 | | | | 8 | | 8 | 2 | | 2 | 6 | |
| Actuated Green, G (s) | | 5.1 | | 23.1 | 23.1 | 23.1 | 82.9 | 82.9 | 97.9 | 82.9 | 82.9 | |
| Effective Green, g (s) | | 8.1 | | 23.1 | 26.1 | 26.1 | 85.9 | 85.9 | 103.9 | 85.9 | 85.9 | |
| Actuated g/C Ratio | | 0.07 | | 0.19 | 0.22 | 0.22 | 0.72 | 0.72 | 0.87 | 0.72 | 0.72 | |
| Clearance Time (s) | | 7.0 | | 3.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | 7.0 | 7.0 | |
| Vehicle Extension (s) | | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 90 | | 299 | 329 | 313 | 229 | 2344 | 1356 | 61 | 2411 | | |
| v/s Ratio Prot | | | 0.03 | 0.03 | | | | 0.67 | 0.00 | | 0.39 | |
| v/s Ratio Perm | | 0.00 | | 0.02 | 0.01 | c0.11 | 0.00 | | 0.02 | c0.67 | | |
| v/c Ratio | | 0.01 | | 0.22 | 0.21 | 0.51 | 0.00 | 0.94 | 0.03 | 0.93 | 0.54 | |
| Uniform Delay, d1 | | 52.2 | | 40.9 | 38.5 | 41.3 | 4.9 | 14.7 | 1.1 | 14.6 | 7.9 | |
| Progression Factor | | 1.00 | | 0.96 | 0.96 | 0.96 | 0.88 | 0.92 | 0.47 | 0.88 | 0.64 | |
| Incremental Delay, d2 | | 0.0 | | 0.4 | 0.3 | 1.3 | 0.0 | 4.6 | 0.0 | 92.8 | 0.8 | |
| Delay (s) | | 52.3 | | 39.7 | 37.3 | 40.9 | 4.3 | 18.1 | 0.5 | 105.6 | 5.8 | |
| Level of Service | D | | D | D | D | A | B | A | F | | A | |
| Approach Delay (s) | 52.3 | | | | 39.8 | | | 17.7 | | | 10.0 | |
| Approach LOS | D | | | | D | | | B | | | B | |

Intersection Summary

| | | | |
|-----------------------------------|-------|----------------------|-----|
| HCM Average Control Delay | 16.8 | HCM Level of Service | B |
| HCM Volume to Capacity ratio | 0.84 | | |
| Actuated Cycle Length (s) | 120.0 | Sum of lost time (s) | 8.0 |
| Intersection Capacity Utilization | 78.7% | ICU Level of Service | D |
| Analysis Period (min) | 15 | | |

c Critical Lane Group

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

HCM Signalized Intersection Capacity Analysis

11: NSR-EW & NSR-Halton

2019 TOTAL

PM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|-------|-------|------|------|----------------------|------|-------|------|------|------|------|------|
| Lane Configurations | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | | ↑ ↗ | ↑ ↘ | ↑ ↗ |
| Volume (vph) | 52 | 2 | 44 | 1 | 26 | 0 | 129 | 25 | 0 | 0 | 31 | 227 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | | | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Frt | 1.00 | 0.86 | | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | 1785 | 1593 | | 1785 | 1879 | | 1716 | 1879 | | | 1879 | 1597 |
| Flt Permitted | 0.74 | 1.00 | | 0.72 | 1.00 | | 0.73 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | 1388 | 1593 | | 1361 | 1879 | | 1328 | 1879 | | | 1879 | 1597 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 57 | 2 | 48 | 1 | 28 | 0 | 140 | 27 | 0 | 0 | 34 | 247 |
| RTOR Reduction (vph) | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 99 |
| Lane Group Flow (vph) | 57 | 18 | 0 | 1 | 28 | 0 | 140 | 27 | 0 | 0 | 34 | 148 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% | 4% | 0% | 0% | 0% | 0% | 0% |
| Turn Type | Perm | | | Perm | | | Perm | | | Perm | | Perm |
| Protected Phases | | 2 | | | 6 | | | 8 | | | 4 | |
| Permitted Phases | 2 | | | 6 | | | 8 | | | 4 | | 4 |
| Actuated Green, G (s) | 37.0 | 37.0 | | 37.0 | 37.0 | | 69.0 | 69.0 | | | 69.0 | 69.0 |
| Effective Green, g (s) | 40.0 | 40.0 | | 40.0 | 40.0 | | 72.0 | 72.0 | | | 72.0 | 72.0 |
| Actuated g/C Ratio | 0.33 | 0.33 | | 0.33 | 0.33 | | 0.60 | 0.60 | | | 0.60 | 0.60 |
| Clearance Time (s) | 7.0 | 7.0 | | 7.0 | 7.0 | | 7.0 | 7.0 | | | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | | 3.0 | 3.0 | | | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 463 | 531 | | 454 | 626 | | 797 | 1127 | | | 1127 | 958 |
| v/s Ratio Prot | | 0.01 | | | 0.01 | | | 0.01 | | | 0.02 | |
| v/s Ratio Perm | c0.04 | | | 0.00 | | | c0.11 | | | | 0.09 | |
| v/c Ratio | 0.12 | 0.03 | | 0.00 | 0.04 | | 0.18 | 0.02 | | | 0.03 | 0.15 |
| Uniform Delay, d1 | 27.8 | 27.0 | | 26.7 | 27.1 | | 10.7 | 9.7 | | | 9.8 | 10.6 |
| Progression Factor | 0.91 | 0.79 | | 1.00 | 1.00 | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.5 | 0.1 | | 0.0 | 0.1 | | 0.5 | 0.0 | | | 0.0 | 0.3 |
| Delay (s) | 25.8 | 21.3 | | 26.7 | 27.2 | | 11.2 | 9.8 | | | 9.8 | 10.9 |
| Level of Service | C | C | | C | C | | B | A | | | A | B |
| Approach Delay (s) | | 23.7 | | | 27.2 | | | 11.0 | | | 10.8 | |
| Approach LOS | | C | | | C | | | B | | | B | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 14.0 | | | HCM Level of Service | | | B | | | | |
| HCM Volume to Capacity ratio | | 0.16 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | | Sum of lost time (s) | | | 8.0 | | | | |
| Intersection Capacity Utilization | | 34.5% | | | ICU Level of Service | | | A | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

HCM Signalized Intersection Capacity Analysis

6: WB OFF RAMP & BRONTE

2019 TOTAL

PM PEAK HOUR



| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
|-----------------------------------|------|-------|----------------------|------|------|------|
| Lane Configurations | ↑↑ | ↑ | ↑↑ | | | ↑↑ |
| Volume (vph) | 259 | 559 | 1853 | 0 | 0 | 818 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | | | 4.0 |
| Lane Util. Factor | 0.97 | 0.91 | 0.95 | | | 0.95 |
| Fr _t | 0.92 | 0.85 | 1.00 | | | 1.00 |
| Flt Protected | 0.98 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (prot) | 3051 | 1321 | 3336 | | | 3400 |
| Flt Permitted | 0.98 | 1.00 | 1.00 | | | 1.00 |
| Satd. Flow (perm) | 3051 | 1321 | 3336 | | | 3400 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 282 | 608 | 2014 | 0 | 0 | 889 |
| RTOR Reduction (vph) | 13 | 13 | 0 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 573 | 291 | 2014 | 0 | 0 | 889 |
| Heavy Vehicles (%) | 5% | 10% | 7% | 2% | 2% | 5% |
| Turn Type | Perm | | | | | |
| Protected Phases | 8 | | 2 | | | 6 |
| Permitted Phases | | | 8 | | | |
| Actuated Green, G (s) | 27.4 | 27.4 | 78.6 | | | 78.6 |
| Effective Green, g (s) | 30.4 | 30.4 | 81.6 | | | 81.6 |
| Actuated g/C Ratio | 0.25 | 0.25 | 0.68 | | | 0.68 |
| Clearance Time (s) | 7.0 | 7.0 | 7.0 | | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | | | 3.0 |
| Lane Grp Cap (vph) | 773 | 335 | 2268 | | | 2312 |
| v/s Ratio Prot | 0.19 | | c0.60 | | | 0.26 |
| v/s Ratio Perm | | | c0.22 | | | |
| v/c Ratio | 0.74 | 0.87 | 0.89 | | | 0.38 |
| Uniform Delay, d1 | 41.2 | 42.9 | 15.5 | | | 8.3 |
| Progression Factor | 1.00 | 1.00 | 0.44 | | | 1.12 |
| Incremental Delay, d2 | 3.8 | 20.3 | 3.0 | | | 0.4 |
| Delay (s) | 45.0 | 63.2 | 9.8 | | | 9.7 |
| Level of Service | D | E | A | | | A |
| Approach Delay (s) | 51.2 | | 9.8 | | | 9.7 |
| Approach LOS | D | | A | | | A |
| Intersection Summary | | | | | | |
| HCM Average Control Delay | | 19.5 | HCM Level of Service | | B | |
| HCM Volume to Capacity ratio | | 0.88 | | | | |
| Actuated Cycle Length (s) | | 120.0 | Sum of lost time (s) | | 8.0 | |
| Intersection Capacity Utilization | | 81.0% | ICU Level of Service | | D | |
| Analysis Period (min) | | 15 | | | | |

c Critical Lane Group

Baseline

%user_name%

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn

Synchro 7 - Report

HCM Signalized Intersection Capacity Analysis

3: EB OFF RAMP & BRONTE

2019 TOTAL

PM PEAK HOUR

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-----------------------------------|------|-------|------|-------|----------------------|------|------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 6 | 7 | 4 | 295 | 4 | 707 | 4 | 1422 | 254 | 328 | 879 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 0.99 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.95 | | 1.00 | 0.85 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1783 | 1785 | | 1700 | 1340 | 1335 | 1785 | 3336 | 1551 | 1653 | 3398 | |
| Flt Permitted | 0.69 | 1.00 | | 0.59 | 1.00 | 1.00 | 0.30 | 1.00 | 1.00 | 0.07 | 1.00 | |
| Satd. Flow (perm) | 1294 | 1785 | | 1053 | 1340 | 1335 | 561 | 3336 | 1551 | 123 | 3398 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 7 | 8 | 4 | 321 | 4 | 768 | 4 | 1546 | 276 | 357 | 955 | 4 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 178 | 178 | 0 | 0 | 98 | 0 | 0 | 0 |
| Lane Group Flow (vph) | 7 | 8 | 0 | 321 | 210 | 206 | 4 | 1546 | 178 | 357 | 959 | 0 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | | | | | | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 5% | 0% | 12% | 0% | 7% | 3% | 8% | 5% | 0% |
| Turn Type | Perm | | | pm+pt | | | Perm | Perm | | Perm | pm+pt | |
| Protected Phases | | 4 | | | 3 | 8 | | | 2 | | 1 | 6 |
| Permitted Phases | 4 | | | 8 | | | 8 | 2 | | 2 | | 6 |
| Actuated Green, G (s) | 2.8 | 2.8 | | 27.1 | 27.1 | 53.8 | 53.8 | 53.8 | 78.9 | 78.9 | | 78.9 |
| Effective Green, g (s) | 5.8 | 5.8 | | 28.1 | 30.1 | 56.8 | 56.8 | 56.8 | 78.9 | 81.9 | | |
| Actuated g/C Ratio | 0.05 | 0.05 | | 0.23 | 0.25 | 0.47 | 0.47 | 0.47 | 0.66 | 0.66 | | 0.68 |
| Clearance Time (s) | 7.0 | 7.0 | | 4.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 3.0 | | 7.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | | 3.0 |
| Lane Grp Cap (vph) | 63 | 86 | | 361 | 336 | 335 | 266 | 1579 | 734 | 363 | 2319 | |
| v/s Ratio Prot | | 0.00 | | c0.16 | 0.16 | | | c0.46 | | c0.18 | 0.28 | |
| v/s Ratio Perm | 0.01 | | | c0.05 | | 0.15 | 0.01 | | 0.11 | 0.47 | | |
| v/c Ratio | 0.11 | 0.10 | | 0.89 | 0.62 | 0.61 | 0.02 | 0.98 | 0.24 | 0.98 | 0.41 | |
| Uniform Delay, d1 | 54.6 | 54.6 | | 43.4 | 39.9 | 39.8 | 16.8 | 31.0 | 18.8 | 39.9 | 8.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.04 | 0.62 | |
| Incremental Delay, d2 | 0.8 | 0.5 | | 22.3 | 3.6 | 3.3 | 0.1 | 18.2 | 0.8 | 40.8 | 0.5 | |
| Delay (s) | 55.4 | 55.1 | | 65.8 | 43.5 | 43.1 | 16.9 | 49.2 | 19.6 | 82.3 | 5.7 | |
| Level of Service | E | E | | E | D | D | B | D | B | F | A | |
| Approach Delay (s) | | 55.2 | | | 49.9 | | | 44.7 | | | 26.5 | |
| Approach LOS | | E | | | D | | | D | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM Average Control Delay | | 40.4 | | | HCM Level of Service | | | | D | | | |
| HCM Volume to Capacity ratio | | 0.93 | | | | | | | | | | |
| Actuated Cycle Length (s) | | 120.0 | | | Sum of lost time (s) | | | 10.0 | | | | |
| Intersection Capacity Utilization | | 90.5% | | | ICU Level of Service | | | E | | | | |
| Analysis Period (min) | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

Baseline

%user_name%

Synchro 7 - Report

C:\Documents and Settings\Dan\My Documents\Traffic\Synchro\Bronte Green\2014 Subdivision\pm2019Total.syn