

Hydrogeological Investigation  
Dundas Urban Core(DUC) Block 297  
Dundas Street East  
Oakville, Ontario

**Prepared For:**  
Valery Homes

**Project No.:** 24-228-100  
**Date:** October 4, 2024



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**24-228-100**

**October 4, 2024**

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**RE: Hydrogeological Investigation–DUC Block 297- Joshua Creek Subdivision, Dundas Street E, Oakville**

DS Consultants Limited (DS) was retained by Valery Group to complete a hydrogeological investigation for the proposed development at DUC Block 297 near 1429 Dundas Street East in Oakville, Ontario (Herein referred to as “the site”). The proposed development at the site will be comprised of a high-rise building with up to a combined two(2) levels of underground parking(P1-P2 Levels). Detailed designs were not available but a conceptual plan is available at the time of drafting this report. The established grade at 165 meters above sea level (masl) and the lowest finished floor elevation of 162 and 159 masl, for common P1 and P2 levels are assumed for the preliminary hydrogeological investigation.

This hydrogeological investigation includes an overview of the existing geological and hydrogeological conditions at the Site and the surrounding area, an assessment of the hydrogeological constraints, and impacts of the proposed development on the local groundwater, and provides an estimation of construction dewatering during the proposed development phase. If needed, the results of this investigation can be used in support of an application for a Category 3 Permit to Take Water (PTTW) or an Environmental Activity Sector Registry (EASR) for construction dewatering from the Ministry of the Environment Conservation and Parks (MECP). Based on the results of this investigation, the following conclusions and recommendations are presented:

1. As part of the hydrogeological investigation, DS completed a search of the MECP Water Well Records (WWRs) database. Based on the MECP WWR search, there are 48 water wells within 500 meters of the site. Two (2) wells were noted for domestic (DO) use. All other wells were noted as either monitoring (MO), test hole (TH) or not in use (NU).
2. In August 2024, DS drilled six (6) boreholes (BH24-1 to 24-6) and equipped five(5) drilled boreholes with a monitoring well as part of the concurrent geotechnical and hydrogeological investigations. The boreholes were advanced to depths ranging from 6.1 to 12.6 meters below the ground surface (mbgs). Two monitoring wells were screened at a depth of 7.8 and 10.7 m below the existing ground surface(mbgs) into shale bedrock and three wells into overburden at a depth between 4.7 and 6.1 mbgs.
3. The site lies within the South Slope physiographic region of southern Ontario and is characterized by drumlinized till plains landforms. Surficial geology at the site is mapped as clay-silt textured till

derived from glaciolacustrine deposits or shale. Shale bedrock of the Queenston formation was encountered during drilling varying in depth from 7.6 mbgs to 15.4 mbgs indicative of an incised valley infilled with till sediments.

4. Groundwater levels were measured in all available monitoring wells on August 27, 2024 by DS personnel. Groundwater levels varied between 3.1 to 5.64 mbgs with a corresponding elevation of 161.1 to 158 masl at the site. Based on groundwater elevations, the flow direction is expected to be towards Joshua Creek.
5. Three(3) Single Well Response Tests (slug tests) were completed by DS on August 27, 2024, to estimate the hydraulic conductivity (k) for the representative geological units in which the wells were screened. The shale bedrock shows a k-value of  $3.4 \times 10^{-7}$  and  $3.2 \times 10^{-8}$  m/s. The k-value for overburden is  $4.9 \times 10^{-8}$  m/s.
6. Short-term Dewatering: Pending design details, the preliminary requirements for dewatering during and after the construction period are as follows. Also, the additional flow rate may be needed because of a major precipitation event within 24 hrs. These values should be verified once detailed designed drawings are available.

| Common Underground Level                                     | P1 Level | P2 Levels |
|--------------------------------------------------------------|----------|-----------|
| Estimated Flow Rate- L/day (without safety factor)- L/day    | 8,000    | 17,000    |
| Estimated Flow Rate- L/day (with safety factor x 1.5)-L/day  | 12,000   | 25,000    |
| Additional Stormwater Removal (assumed 10 mm /24 hrs)- L/day | 60,000   | 60,000    |
| Total Dewatering Rate                                        | 72,000   | 85,000    |

7. Permanent Drainage or Foundation Drain: Following the construction of the underground structure, long-term groundwater flow to the underfloor drainage system for the building will be a function of the upward flux and drainage along the foundation wall. The estimated permanent flow rates are as below. The estimated values should be verified once detailed designed drawings are available.

| Underground Level                                            | P1 Level | P2 Levels |
|--------------------------------------------------------------|----------|-----------|
| Estimated Flow Rate- L/day (without safety factor)- L/day    | 1,000    | 7,000     |
| Estimated Flow Rate- L/day (with safety factor x 1.5)- L/day | 1,500    | 10,500    |

8. Permit Requirements:

- The expected design dewatering rates during construction for all phases are expected to be more than 50,000 L/day including additional stormwater removal. Therefore, an EASR application is required to be submitted to the MECP for short-term dewatering. An Environmental Activity Sector Registration (EASR) is required to be submitted to the Ministry of the Environment, Conservation and Parks (MECP) if the taking of groundwater

and stormwater for a temporary construction project is between 50,000 L/day and 400,000 L/ day.

- An EASR can be avoided if the daily pumping requirement is maintained below 50,000 L/day during construction.
  - Based on current groundwater conditions, permanent groundwater flow or permanent drainage is expected to be less than the water-taking limit of 50,000 L/day, therefore, a PTTW is not required permanently.
  - A discharge permit will be required from the Halton Region/Town of Oakville if private water is to be sent to the sewer system for construction dewatering and permanent drainage. Alternatively, the pumped volume can be managed on-site because of the minimal expected dewatering volume during the construction.
9. One (1) unfiltered groundwater sample was collected from monitoring well BH 24-6 on August 29, 2024, to assess the suitability for discharge of groundwater to the Halton Region sanitary and combined sewers and the Town of Oakville storm sewers.
10. Groundwater quality analysis indicated that no parameters exceeded the Halton Region sanitary and combined sewer criteria but total suspended solids(TSS), manganese and chloroform exceeded the Town of Oakville storm sewer criteria. Therefore, groundwater at the development site is not suitable for discharge into the Town of Oakville's storm sewers without pre-treatment. A Discharge permit may be required from the Town of Oakville for discharge if the pumped water is diverted to the Town's sewer system.
11. Following the completion of construction activities, all dewatering wells, well points, eductors and monitoring wells installed at various stages of this project must be decommissioned. The installation and eventual decommissioning of the wells and the dewatering system must be conducted by a licensed water well contractor following Regulation 903 of the Ontario Water Resources Act.

Should you have any questions regarding these findings, please contact the undersigned.

**DS Consultants Ltd.**

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## 1.0 INTRODUCTION

DS Consultants Limited (DS) was retained by Valery Group to complete a hydrogeological investigation for the proposed development at DUC Block 297 near 1429 Dundas Street East in Oakville, Ontario (Herein referred to as “the site”). The proposed development at the site will be comprised of a high-rise building with up to a combined two(2) levels of underground parking(P1-P2 Levels). Detailed designs were not available but a conceptual plan is available at the time of drafting this report. The established grade at 165 meters above sea level (masl) and the lowest finished floor elevation of 162 and 159 masl, for common P1 and P2 levels are assumed for the preliminary hydrogeological investigation.

This hydrogeological investigation includes an overview of the existing geological and hydrogeological conditions at the Site and the surrounding area, an assessment of the hydrogeological constraints, and impacts of the proposed development on the local groundwater, and provides an estimation of construction dewatering during the proposed development phase. If needed, the results of this investigation can be used in support of an application for a Category 3 Permit to Take Water (PTTW) or an Environmental Activity Sector Registry (EASR) for construction dewatering from the Ministry of the Environment Conservation and Parks (MECP). Construction dewatering volumes were estimated based on preliminary site plan dimensions provided to DS.

### 1.1 Purpose

The purpose of this investigation was to review and determine the need for dewatering, estimate dewatering rates, assess groundwater quality and determine the need for a Permit to Take Water (PTTW) or an Environmental Activity Sector Registry (EASR) from the Ministry of Environment, Conservation and Parks (MECP) in addition to requirements to obtain discharge permits from the Halton Region if needed. Potential impacts related to construction dewatering and associated monitoring/mitigation measures were also to be investigated.

### 1.2 Scope of Work

The scope of work for this investigation included:

- Site visits.
- Desktop review of pertinent geological and hydrogeological resources.
- Review the MECP Water Well Records and water use in the surrounding area.
- Fieldwork includes drilling of six (6) boreholes in August 2024
- Conducting single well response tests (slug tests) to determine hydraulic conductivity values across the site.

- Characterize the stratigraphy and measure the groundwater levels across the site.
- Collection and analysis of groundwater samples to quantify and characterize any contaminants that may impact future discharge applications.
- Estimation of dewatering volumes, which is to be used to predict the short-term and long-term groundwater control requirements during and after construction of the proposed building(s) on the site.
- Impact assessment as a result of potential dewatering activities and mitigation measures.

## **2.0 FIELDWORK**

- In August 2024, DS drilled six (6) boreholes (BH24-1 to 24-6) and equipped five(5) drilled boreholes with a monitoring well as part of the concurrent geotechnical and hydrogeological investigations. The boreholes were advanced to depths ranging from 6.1 to 12.6 meters below the ground surface (mbgs). Two monitoring wells were screened at a depth of 7.8 and 10.7 m below the existing ground surface(mbgs) into shale bedrock and three wells into overburden at a depth between 4.7 and 6.1 mbgs.
- All monitoring wells were developed before any use to allow for groundwater level monitoring, hydraulic conductivity testing, and to assess groundwater quality.
- Three(3) single well response tests (SWRTs) were completed by performing a rising head test (slug test) to estimate the hydraulic conductivity values of the soils at the site.
- One (1) unfiltered groundwater sample was also collected and analyzed for the parameters listed under the Halton Region sewer discharge by-law, the Town of Oakville storm sewer discharge by-law.

## **3.0 PHYSICAL SETTING**

Available topographic maps and environmental, geotechnical, and hydrogeological reports were used to develop an understanding of the physical setting of the study area. Borehole logs and the MECP WWRs were used to interpret the geological and hydrogeological conditions at the development site.

### **3.1 Physiography and Drainage**

The topography at the development site slopes towards Joshua Creek located about 350 m to the east side of the Site. Surface elevation across the site ranges from 167 to 161 masl. Drainage in the study area is controlled by streams, artificial channels, and the local topography, and may also be influenced by fill and underground utilities.

## **3.2 Geology**

The following presents a brief description of regional and development site geology based on the review of available information and development site-specific soil investigations.

### **3.2.1 Quaternary Geology**

According to the Ontario Geological Survey mapping across the region, the site lies within the South Slope physiographic region of southern Ontario and is characterized by drumlinized till plains landforms. Surficial geology at the site is mapped as clay-silt textured till derived from glaciolacustrine deposits or shale. The surficial geology map is shown in **Figure 2**.

### **3.2.2 Bedrock Geology**

According to the Ontario Geological Survey mapping across the region, the bedrock at the site is comprised of shale, limestone, dolostone, and siltstone of the Queenston Formation.

### **3.2.3 Site Geology/ Soil Conditions**

On-site subsurface soil conditions were summarized from the boreholes advanced by DS for the current investigation. Detailed subsurface conditions are presented in **Figure 5**, and the borehole logs are presented in **Appendix A**. The subsurface conditions in the boreholes are summarized in the following paragraphs.

#### **Fill Materials:**

Fill materials were found in all boreholes extending to depths ranging from 0.8 to 3.0 m. The fill material generally consisted of clayey silt to silty clay with inclusions of shale fragments and trace organics. A surficial granular fill layer, about 150mm thick, consisting of sand and gravel was encountered in BH24-3.

#### **Silty Clay Till:**

The native soils below the fill material consisted of silty clay till deposits, overlying till/shale complex or shale bedrock.

#### **Till/Shale Complex:**

Below the silty clay till deposits and above the shale bedrock, a transition unit of till/shale complex (clayey silt till mixed with highly weathered shale fragments) was encountered in two (2) boreholes, BH24-1 and BH24-2. T

#### **Shale Bedrock:**

The shale bedrock of Queenston Formation was encountered in all boreholes (BH24-1 to BH24-6) at depths ranging from 6.0 to 7.6 mbgs corresponding to elevations 159.8 to 161.3 masl.

### 3.3 Hydrogeology

The hydrogeology at the site was evaluated using the on-site monitoring wells installed by DS, and the MECP WWRs in the study area.

#### 3.3.1 Local Groundwater Use

As part of the hydrogeological investigation, DS completed a search of the MECP Water Well Records (WWRs) database (**Appendix D**). Based on the MECP WWR search, there are 48 water wells within 500 meters of the site. Two (2) wells were noted for domestic (DO) use. All other wells were noted as either monitoring (MO), test hole (TH) or not in use (NU). A water well survey is recommended within the study area to confirm the presence and use of any domestic wells. **Figure 1** shows the MECP water well location plan. A water well survey is recommended within the study area to confirm the presence and use of any domestic wells.

#### 3.3.2 Groundwater Conditions

Groundwater levels were measured in all available monitoring wells on August 27, 2024 by DS personnel. **Table 3-1** presents the groundwater levels in all monitoring wells. Groundwater levels varied between 3.1 to 5.64 mbgs, corresponding to elevations 161.3-158. masl. Based on groundwater elevations, the flow direction is expected to be southeast towards Joshua Creek. The groundwater levels are subject to seasonal fluctuations and may vary in response to changing climate conditions.

**Table 3-1: Groundwater Levels in Monitoring Wells**

| Well ID/<br>Location | Ground<br>Elevation<br>(masl) | Well<br>Depth<br>(mbgs) | Screened<br>Interval<br>(masl) | Date            | Depth to<br>Water<br>(mbgs) | Groundwater<br>Elevation<br>(masl) |
|----------------------|-------------------------------|-------------------------|--------------------------------|-----------------|-----------------------------|------------------------------------|
| BH24-1               | 166.9                         | 7.6                     | 4.6-7.6                        | August 27, 2024 | 5.64                        | 161.3                              |
| BH24-2               | 166.9                         | 4.6                     | 1.6-4.6                        | August 27, 2024 | Dry                         | n/a                                |
| BH24-3               | 167.3                         | 6.1                     | 3.1-6.1                        | August 27, 2024 | Dry                         | n/a                                |
| BH24-5               | 164.3                         | 6.1                     | 3.1-6.1                        | August 27, 2024 | 3.02                        | 161.3                              |
| BH24-6               | 161.3                         | 10.7                    | 7.7-10.7                       | August 27, 2024 | 3.33                        | 158.0                              |

#### 3.3.3 Hydraulic Conductivity

A Single Well Response Test (slug test) was completed in three wells available with sufficient water by DS on August 27, 2024, to estimate hydraulic conductivity (k) for the representative geological units in which the wells were screened. Two wells were found dry at the time of testing. The testing was completed using data loggers placed at the bottom of the monitoring wells to accurately measure the change in the hydraulic head versus time. Hydraulic conductivity (k) values were calculated using the Hvorslev method using the AquiferTest® Software. The semi-log plots for normalized drawdown versus

time are provided in **Appendix B**. The shale bedrock shows a k-value of  $3.4 \times 10^{-7}$  and  $3.2 \times 10^{-8}$  m/s. The k-value for overburden is  $4.9 \times 10^{-8}$  m/s. **Table 3-2** presents the Hydraulic Conductivity (k) values for the representative geological units.

**Table 3-2: Summary of Hydraulic Conductivity (k) Test Results**

| Well ID | Screened Interval (mbgs) | Screened Formation              | K-value (m/s)        |
|---------|--------------------------|---------------------------------|----------------------|
| BH24-1  | 4.6-7.6                  | Shale complex/shale bedrock     | $3.4 \times 10^{-7}$ |
| BH24-2  | 1.6-4.6                  | Silty clay till                 | Dry                  |
| BH24-3  | 3.1-6.1                  | Silty clay till                 | Dry                  |
| BH24-5  | 3.1-6.1                  | Silty clay till-sandy silt till | $4.9 \times 10^{-8}$ |
| BH24-6  | 7.7-10.7                 | shale bedrock                   | $3.2 \times 10^{-8}$ |

### 3.3.4 Groundwater Quality

One (1) unfiltered groundwater sample was collected from monitoring well BH 24-6 on August 29, 2024, to assess the suitability for discharge of groundwater to the Halton Region sanitary and combined sewers and the Town of Oakville storm sewers. The groundwater samples were submitted to SGS Laboratories in Lakefield, Ontario. SGS is certified by the Canadian Association of Laboratory Accreditation Inc. (CALA) and the Canadian Standard Association (CSA). The reported analytical results indicate that on parameters exceeded the Halton Region's sewer criteria, but TSS, manganese and chloroform exceeded the Town of Oakville's storm sewer criteria. **Table 3-3** present a summary of the exceeded parameters, and the certificates of analyses are provided in **Appendix C**.

**Table 3-3: Parameters in Groundwater Exceeding Halton Region Sewer Use By-Law and Town of Oakville Storm Sewer Use By-law**

| Parameter                                                                                                          | Unit | Halton Region Sanitary Sewer By-Law Criteria | Halton Region/Town of Oakville Storm Sewer By-Law Criteria | BH 24-6       |
|--------------------------------------------------------------------------------------------------------------------|------|----------------------------------------------|------------------------------------------------------------|---------------|
| Total Suspended Solids (TSS)                                                                                       | mg/L | 350                                          | 15                                                         | <u>29</u>     |
| Manganese                                                                                                          | mg/L | 5                                            | 0.05                                                       | <u>0.11</u>   |
| Chloroform                                                                                                         | mg/L | 0.04                                         | 0.002                                                      | <u>0.0052</u> |
| <u>0.00</u> - Exceeds Storm Sewer Criteria; <b>0.00(bold)</b> - Exceeds Sanitary and Combined Sewer Criteria; 0.00 |      |                                              |                                                            |               |

## 4.0 CONSTRUCTION DEWATERING

### 4.1 Estimation of Flow Rates- Proposed Building(s)

Detailed designs were not available to DS at the time of drafting this report. The established grade at 165 meters above sea level (masl) and the lowest finished floor elevation of 162 and 159 masl, for common

P1 and P2 levels are assumed for dewatering assessment. The lowest excavation depth would be 3 m below the lowest finished floor elevation of underground structures ( EL 159-156 masl) The highest groundwater elevation is 161.3 masl and hence dewatering will be required during excavation. The dewatering volume was estimated using the steady-state equation as below in **Table 4-1**. The groundwater flux is expected to be limited because of the low hydraulic conductivity of the till and underlying shale bedrock. The dewatering rates should be revised once the detailed design becomes available.

$$Q = \frac{\pi(H^2 - h^2)}{2.3 \log\left(\frac{R_0}{r_e}\right)} \quad \text{Eq.1}$$

$$R_0 = C(H - h)\sqrt{k} \quad \text{Eq.2}$$

$$r_e = \sqrt{\frac{ab}{\pi}} \quad \text{Eq.3}$$

**Table 4-1: Dewatering Flow Rates( Short-term)- Common Underground P1-P2 Levels**

| Parameter                                                                   | P1 Level             | P2 Levels            |
|-----------------------------------------------------------------------------|----------------------|----------------------|
| K -Hydraulic conductivity(geomean) (m/s)                                    | $3.4 \times 10^{-7}$ | $3.4 \times 10^{-7}$ |
| H-Distance from water level to the bottom of an aquifer (m)                 | 3.0                  | 6.0                  |
| h -Depth of water in the well while pumping (m)                             | 0.5                  | 0.5                  |
| Area (a x b) in (m)                                                         | 100x 60              | 100x 60              |
| $r_e$ —equivalent radius, where a and b excavation dimensions (m)           | 44                   | 44                   |
| $R_0$ - $r_e$ + Radius of the cone of depression(Zone of Influence-ZOI)-(m) | 48                   | 55                   |
| Estimated Flow Rate- L/day (without safety factor)- L/day                   | 8,000                | 17,000               |
| Estimated Flow Rate- L/day (with safety factor x 1.5)- L/day                | 12,000               | 25,000               |
| Additional Dewatering- Stormwater Removal<br>(assumed 10 mm /24 hrs)- L/day | 60,000               | 60,000               |

## 4.2 Total Estimation of Flow Rate (Short-Term/ Temporary Discharge)

Considering the unsealed excavation method, the estimated steady-state flow rate for building with P1 and P2 levels would be 12,000 and 25,000 L/day with a safety factor of x 1.5 These values are recommended to be verified once detailed designed drawings are available. Also, the additional flow rate may be needed because of a major precipitation event within 24 hrs.

### 4.3 Zones of Influence During Construction

The radius of influence (Ro) for the construction dewatering was calculated based on the Sichardt equation (Equation 2). Ro is the distance at which the drawdown resulting from pumping is negligible. The equation is empirical and was developed to provide representative flow rates using the steady-state flow dewatering equations as indicated above. Under steady-state conditions, the Ro of pumping will extend until boundary flow conditions are reached, and sufficient water inputs are equal to the discharge rate due to pumping. Therefore, the Sichardt equation is used to provide a representative flow rate but is not precise in determining the actual radius of influence by pumping. Based on the Sichardt equation the ZOI is approximately 4 and 9 m from the edges of the excavation for the underground parking levels P1 and P2.

### 4.4 Permanent Drainage (Long-term Discharge)

Following the construction of the underground structure, long-term groundwater flow to the underfloor drainage system for the building will be a function of the upward flux and drainage along the foundation wall. The estimated permanent flow rates are as below in **Table 4-2**.

**Table 4-2: Permanent Flow Rate or Foundation Drain- Common Underground P1-P2 Levels**

| Parameters                                                  | P1 Level             | P2 Levels            |
|-------------------------------------------------------------|----------------------|----------------------|
| K -Hydraulic conductivity (highest) (m/s)                   | $3.4 \times 10^{-7}$ | $3.4 \times 10^{-7}$ |
| H-Distance from water level to subfloor drainage(m)         | 0.5                  | 3.0                  |
| h -Depth of water in the well while pumping (m)             | 0                    | 0                    |
| Area (a x b) in (m)                                         | 100 x 60             | 100 x 60             |
| Estimated Flow Rate- L/day (without safety factor)- L/day   | 1,000                | 7,000                |
| Estimated Flow Rate- L/day (with safety factor x 1.5)-L/day | 1,500                | 10,500               |

### 4.5 Permit Requirements

#### 4.5.1 Environmental Activity and Sector Registry (EASR) /Permit to Take Water (PTTW) Application

An Environmental Activity Sector Registration (EASR) is required to be submitted to the Ministry of the Environment, Conservation and Parks (MECP) if the taking of groundwater and stormwater for a temporary construction project is between 50,000 L/day and 400,000 L/ day. The EASR application is an online registry and should be submitted to the MECP before any construction dewatering. A PTTW is required to be submitted to the MECP if the taking of groundwater and stormwater for a temporary construction project is more than 400,000 L/ day.

The expected design dewatering rates during construction for all phases are expected to be more than 50,000 L/day including additional stormwater removal. Therefore, an EASR application is required to be

submitted to the MECP for the short term. However, an EASR can be avoided if the daily pumping requirement is maintained below the water-taking limit during construction.

Furthermore, based on current groundwater conditions, permanent groundwater flow or permanent drainage is expected to be less than the water-taking limit of 50,000 L/day, therefore, a PTTW is not required permanently.

#### **4.5.2 Discharge Permits**

A discharge permit will be required from the Halton Region/Town of Oakville if private water is to be sent to the sewer system for construction dewatering and permanent drainage. Alternatively, the pumped volume can be managed on-site because of the minimal expected dewatering volume during the construction.

### **5.0 POTENTIAL IMPACTS**

The following are the predicted potential impacts due to construction dewatering:

#### **5.1 Local Groundwater Use**

Based on the MECP WWRs, there are no private water wells expected in the maximum predicted radius of Influence of about 11 from the edge of the excavation. Also, the expected dewatering volumes are minimal and therefore, it is not expected short-term or long-term impacts to private water wells occurring from the proposed short-term dewatering.

#### **5.2 Source Protection Area**

The site is located within the Halton Region Source Protection Area (SPA). Source Protection Plans contain policies aimed at protecting drinking water sources by reducing or eliminating significant threats to the source of municipal drinking water. No source of municipal water drinking water within the expected radius of influence of about 11 m from the edges of the excavation. Therefore, no impacts are anticipated on the drinking water supply within the zone of influence.

#### **5.3 Highly Vulnerable Aquifer**

The site is not located in a Highly Vulnerable Aquifer (HVA). HVAs are aquifers that are more susceptible to contamination consisting of granular material (i.e., sand & gravel, and fractured rock near the surface of the ground) as

#### **5.4 Wellhead Protection Area**

The site and the study area are not located within a municipal Wellhead Protection Area (WHPA). WHPAs are used to identify locations of potential water quantity threats. There are two types of threats: those associated with water demand and those associated with a reduction in groundwater recharge.

## **5.5 Intake Protection Zone**

The site and the study area are not located within an Intake Protection Zone (IPZ). IPZs depend on surface water for municipal water supply and include areas of land adjacent to streams and storm sewers where runoff water can quickly reach an intake.

## **5.6 Surface Water**

The nearest surface body is Joshua Creek located about 350 m away from the eastern boundary of the site, not falling within the maximum thermal radius of influence of about 9 m from the edges of the excavation. The development will be completed from low permeable silty clay to sandy silt till and shale. The horizontal and vertical groundwater movement within the till and shale is expected to be limited and locally. As such, any adverse impact is not anticipated on the nearby Joshua Creek because of dewatering activities

## **5.7 Point of Discharge and Groundwater Quality**

Groundwater quality analysis indicated that no parameters exceeded the Halton Region sanitary and combined sewer criteria but total suspended solids(TSS), manganese and chloroform exceeded the Town of Oakville storm sewer criteria. Therefore, groundwater at the development site is not suitable for discharge into the Town of Oakville's storm sewers without pre-treatment. A Discharge permit may be required from the Town of Oakville for short-term discharge if the pumped water is diverted to the Town's sewer system.

## **6.0 MONITORING AND MITIGATION**

Based on the findings of the hydrogeological investigation and associated potential impacts due to development, the following monitoring and mitigation program is provided:

- Baseline groundwater quality has been assessed and established before construction. However, groundwater quality can change based on several factors (land-use change, spills, etc.) and should be monitored during construction dewatering and after construction to ensure that water quality meets the guidelines or regulations associated with any permits from the MECP, Halton Region and Town of Oakville.
- If a groundwater dewatering system is set up at the Site, daily and weekly monitoring should be implemented to assess the groundwater conditions such as water levels, measurement of discharge flow, discharge water quality and any adverse impacts because of dewatering.
- In conformance with Regulation 903 of the Ontario Water Resources Act, the decommissioning of any dewatering system and monitoring wells should be carried out by a licensed contractor under the supervision of a licensed water well technician.

## 7.0 LIMITATIONS

This report was prepared for the sole use of the addressee to provide an assessment of the hydrogeological conditions on the property. The information presented in this report is based on information collected during the completion of the hydrogeological investigation. DS Consultants Limited was required to use and rely upon various information sources produced by other parties. The information provided in this report reflects DS' judgment considering the information available at the time of report preparation. This report may not be relied upon by any other person or entity without the written authorization of DS Consultants Ltd. The scope of services performed in the execution of this investigation may not be appropriate to satisfy the needs of other users, and any use or reuse of these documents or findings, conclusions, and recommendations represented herein is at the sole risk of said users. The conclusions drawn from the Hydrogeological report were based on information at selected observation and sampling locations. Different conditions between and beyond these locations may become apparent during future investigations or on-site work, which could not be detected or anticipated at the time of this investigation. DS Consultants Ltd. cannot be held responsible for hydrogeological conditions at the site that were not apparent from the available information.

Should you have any questions regarding these findings, please contact the undersigned.

### DS Consultants Ltd.

Prepared By:



**Pradeep Patel, M.Sc., P.Geo.**  
Hydrogeologist

Reviewed By:



**Martin Gedeon, M.Sc., P.Geo.**  
Senior Hydrogeologist



## 8.0 CONSULTANT QUALIFICATIONS

**Martin Gedeon, M.Sc., P.Geo.**, is a Professional Geoscientist (P.Geo.) with over 26 years of experience as an environmental/hydrogeological consultant in the areas of groundwater and soil monitoring, environmental site assessments, environmental due diligence, and remediation. Martin has significant experience in physical and contaminant hydrogeology across Canada and overseas and has provided hydrogeological/environmental technical support on various projects. Martin has prepared hundreds of hydrogeological reports in support of permit applications for a private sector development application, municipal dewatering operations, and provincial infrastructure projects across the province.

**Pradeep Patel, M.Sc., P.Geo.** is a hydrogeologist at DS Consultants Ltd. and has more than 15 years of experience working in the environmental industry. He participates in numerous Hydrogeological and Geotechnical investigation projects. His experience includes the preparation of construction dewatering activities and hydrogeological investigations in support of Environmental Activity and Sector Registry (EASR) and Permit to Take Water (PTTW) applications.

## 9.0 REFERENCES

Approved Source Protection Plan: CTC Source Protection Region. Prepared by: CTC Source Protection Committee. Amendment (Version 2.0). Effective March 25, 2019

Chapman, L.J., and D.F. Putnam; The Physiography of Southern Ontario, Third Edition, Ontario Geological Survey Special Volume 2; 1984, & 2007.

Freeze, R.A., and J.A. Cherry. "Groundwater." Prentice-Hall, Inc. Englewood Cliffs, NJ. 1979.

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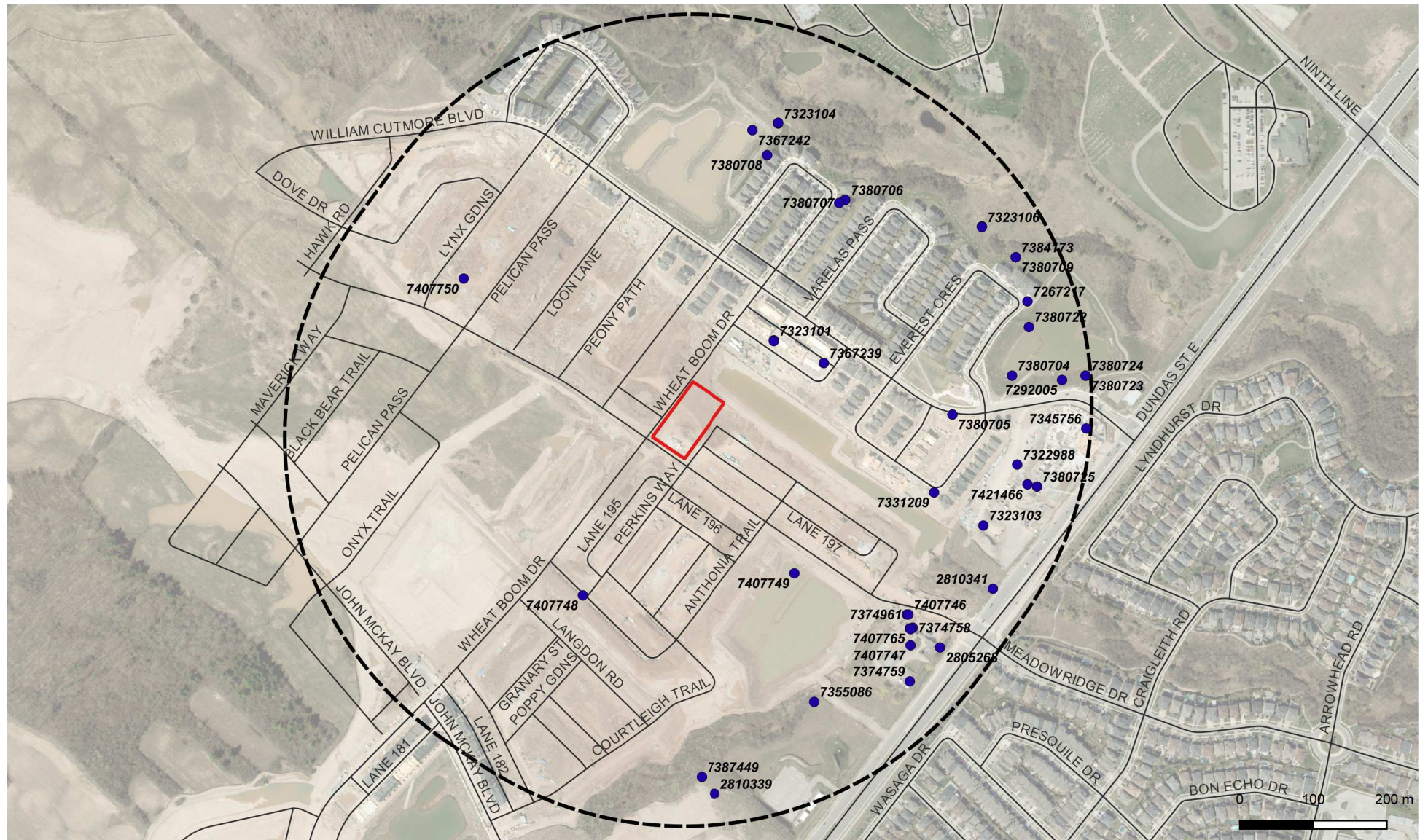
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Pat M. Cashman and Martin Preene; Groundwater Lowering in Construction- Second Edition, CRC Press.

## FIGURES



### Legend

- Property Boundary
- 500m Buffer
- Registered Water Well (MECP WWR)



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www.dsconsultants.ca

Client:

VALERY HOMES

Project:

HYDROGEOLOGICAL INVESTIGATION  
Dundas Urban Core Block(DUC) Block 297- Dundas St. E., Oakville, ON

Title:

### SITE LOCATION AND MECP WELL RECORDS



Size:  
8.5 x 11

Approved By:

P.P

Drawn By:

S.Y

Date:

October 2024

Rev:  
0

Scale:

As Shown

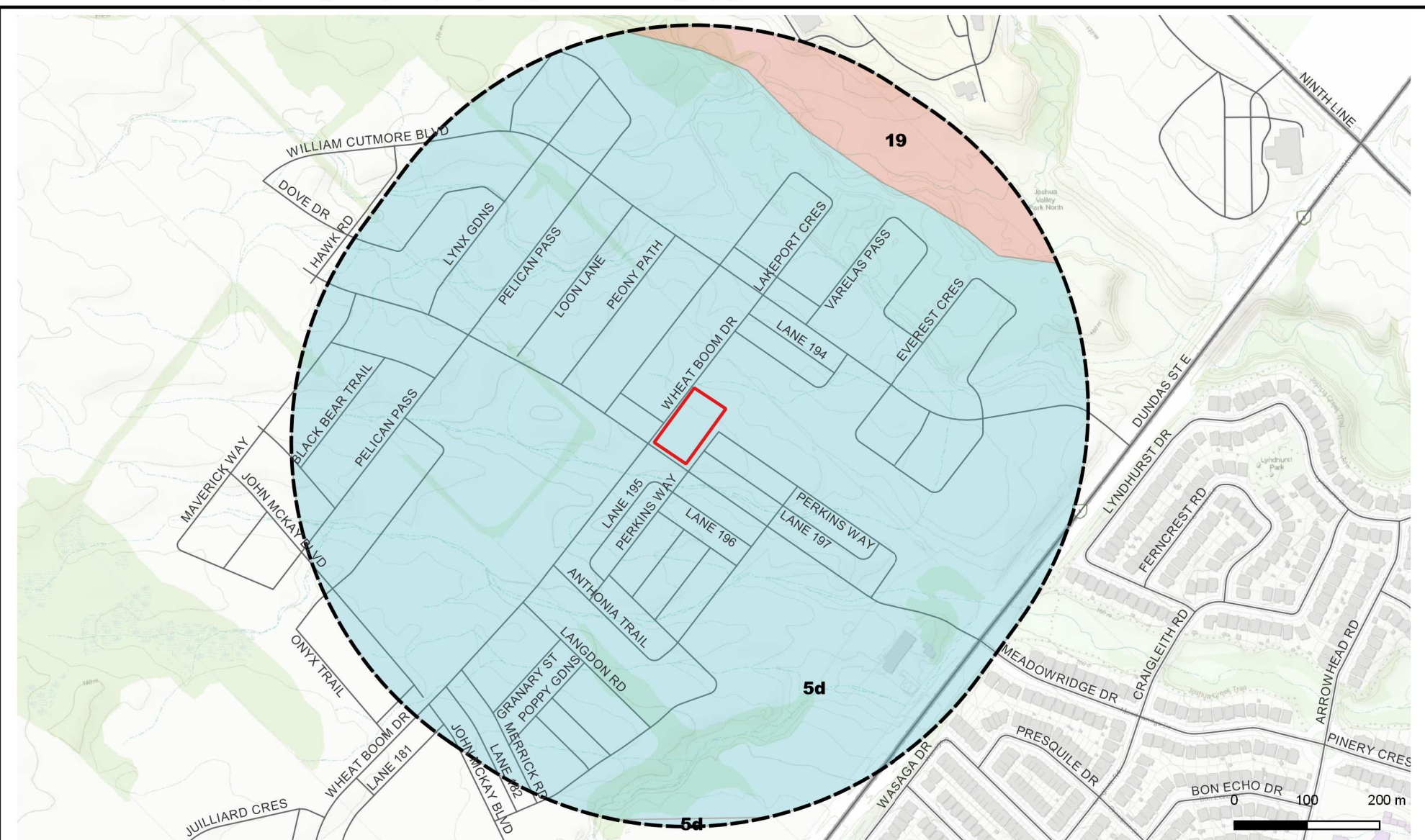
Project No.:

24-228-100

Figure No.:

1

Image/Map Source: Esri Satellite Image



### Legend

- Property Boundary
- 500m Buffer
- 19 - Modern Alluvium
- 5d - Till



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Dundas Urban Core Block(DUC) Block 297- Dundas St. E., Oakville, ON

Title:

**SURFICIAL GEOLOGY MAP**

Size:  
8.5 x 11

Rev:  
0

Approved By:

P.P

Scale:

As Shown

Image/Map Source: Esri Topo Map

Drawn By:

S.Y

Project No.:

24-228-100

Date:

October 2024

Figure No.:

**2**





# Legend

- Property Boundary
- ⊕ Borehole
- ⊗ Monitoring Well
- Cross Section



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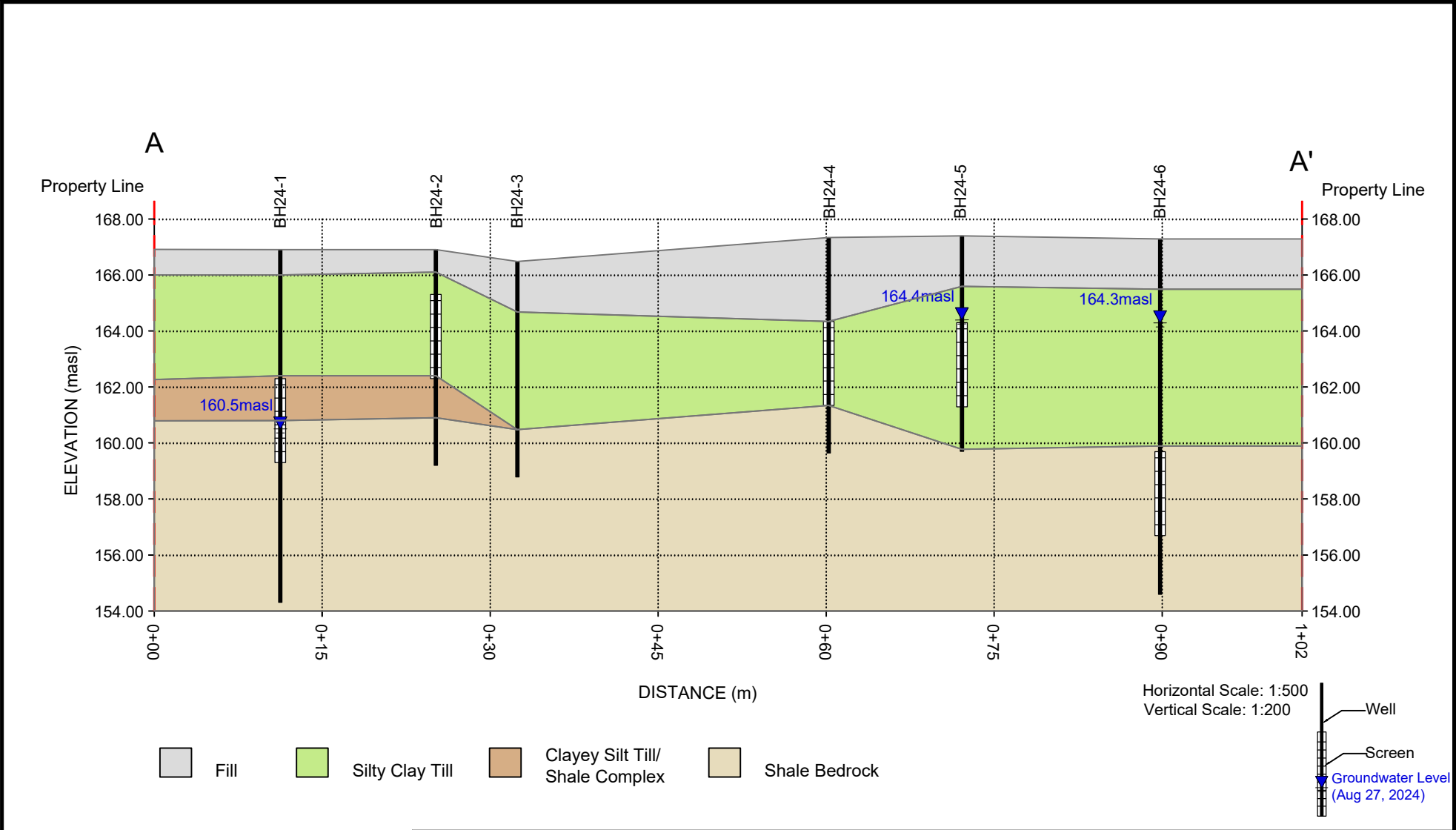
Client: **VALERY HOMES**

Project: **HYDROGEOLOGICAL INVESTIGATION  
 Dundas Urban Core Block(DUC) Block 297- Dundas St. E., Oakville, ON**

Title: **BOREHOLE AND MONITORING WELL LOCATIONS**



|                                        |                     |                            |                         |
|----------------------------------------|---------------------|----------------------------|-------------------------|
| Size:<br>8.5 x 11                      | Approved By:<br>P.P | Drawn By:<br>S.Y           | Date:<br>October 2024   |
| Rev:<br>0                              | Scale:<br>As Shown  | Project No.:<br>24-228-100 | Figure No.:<br><b>3</b> |
| Image/Map Source: Esri Satellite Image |                     |                            |                         |



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Project: HYDROGEOLOGICAL INVESTIGATION  
Dundas Urban Core Block(DUC) Block 297- Dundas St. E.,Oakville, ON

Title: **GEOLOGICAL CROSS SECTION A-A'**

Client:  
**VALERY HOMES**

|                   |                     |                           |                        |
|-------------------|---------------------|---------------------------|------------------------|
| Size:<br>8.5 x 11 | Approved By:<br>P.P | Drawn By:<br>S.Y          | Date:<br>October 2024  |
| Rev.              | Scale:<br>As Shown  | Project No:<br>24-228-100 | Figure No.<br><b>4</b> |

## **APPENDICES**

## **Appendix A: Borehole Logs**

PROJECT: Additional Geotechnical Investigation  
CLIENT: Valery Group  
PROJECT LOCATION: Block 297, Oakville, Ontario  
DATUM: Geodetic  
BH LOCATION: See Drawing 1 N 4817671.9 E 604337.1

**DRILLING DATA**  
Method: Hollow Stem Auger/Mud Rotary  
Diameter: 200mm  
Date: Aug-09-2024  
REF. NO.: 24-228-100  
ENCL NO.: 2

| SOIL PROFILE |                                                                                                                                                                                 |             | SAMPLES |      |                 | GROUND WATER CONDITIONS | ELEVATION                     | DYNAMIC CONE PENETRATION RESISTANCE PLOT |                 | PLASTIC LIMIT NATURAL MOISTURE CONTENT LIQUID LIMIT |                   | POCKET PEN. (Cu) (kPa) | NATURAL UNIT WT (kN/m <sup>3</sup> ) | REMARKS AND GRAIN SIZE DISTRIBUTION (%) |
|--------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------|------|-----------------|-------------------------|-------------------------------|------------------------------------------|-----------------|-----------------------------------------------------|-------------------|------------------------|--------------------------------------|-----------------------------------------|
| (m)          | DESCRIPTION                                                                                                                                                                     | STRATA PLOT | NUMBER  | TYPE | "N" BLOWS 0.3 m |                         |                               | 20 40 60 80 100                          | 20 40 60 80 100 | W <sub>p</sub> W W <sub>L</sub>                     | WATER CONTENT (%) |                        |                                      |                                         |
| 166.9        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      | GR SA SI CL                             |
| 0.0          | <b>FILL:</b> clayey silt, trace sand, reddish brown, moist, very stiff                                                                                                          |             | 1       | SS   | 15              |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 166.0        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 0.9          | <b>SILTY CLAY TILL:</b> sandy, trace gravel, brown to reddish brown, moist, very stiff to hard                                                                                  |             | 2       | SS   | 33              |                         | 166                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
|              |                                                                                                                                                                                 |             | 3       | SS   | 31              |                         | 165                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
|              |                                                                                                                                                                                 |             | 4       | SS   | 28              |                         | 164                           |                                          |                 |                                                     |                   |                        |                                      | 3 26 48 23                              |
|              |                                                                                                                                                                                 |             | 5       | SS   | 17              |                         | 163                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 162.4        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 4.5          | <b>CLAYEY SILT TILL/SHALE COMPLEX:</b> trace sand, reddish brown, moist, hard                                                                                                   |             | 6       | SS   | 50/75mm         |                         | 162                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
|              |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 160.8        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 160.7        | <b>SHALE BEDROCK:</b> Queenston Formation, reddish brown, weathered                                                                                                             |             | 7       | SS   | 50/75mm         |                         | 161                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 160.3        |                                                                                                                                                                                 |             | R1      | RC   |                 |                         | 160                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 6.6          | TCR=100%, SCR=93%, RQD=93%<br>Hard layers=6%, Maximum hard layer thickness=10mm                                                                                                 |             |         |      |                 |                         | W. L. 160.5 m<br>Aug 27, 2024 |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 159.8        |                                                                                                                                                                                 |             | R2      | RC   |                 |                         | 159                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 7.1          | TCR=98%, SCR=86%, RQD=83%<br>Hard layers=19%, Maximum hard layer thickness=100mm                                                                                                |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
|              | TCR=96%, SCR=88%, RQD=83%<br>Hard layers=11%, Maximum hard layer thickness=50mm                                                                                                 |             | R3      | RC   |                 |                         | 158                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 157.3        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 9.6          | TCR=93%, SCR=93%, RQD=87%<br>Hard layers=10%, Maximum hard layer thickness=130mm                                                                                                |             | R4      | RC   |                 |                         | 157                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 155.8        |                                                                                                                                                                                 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 11.1         | TCR=100%, SCR=98%, RQD=98%<br>Hard layers=18%, Maximum hard layer thickness=100mm                                                                                               |             | R5      | RC   |                 |                         | 156                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 154.3        |                                                                                                                                                                                 |             |         |      |                 |                         | 155                           |                                          |                 |                                                     |                   |                        |                                      |                                         |
| 12.6         | <b>END OF BOREHOLE:</b><br>Notes:<br>1) 50mm dia. monitoring well installed upon completion.<br>2) Water Level Readings:<br><br>Date: Water Level(mbgl):<br>August 27, 2024 6.4 |             |         |      |                 |                         |                               |                                          |                 |                                                     |                   |                        |                                      |                                         |

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 24-228-100GEO.GPJ DS GDT 24-9-5



PROJECT: Additional Geotechnical Investigation  
CLIENT: Valery Group  
PROJECT LOCATION: Block 297, Oakville, Ontario  
DATUM: Geodetic  
BH LOCATION: See Drawing 1 N 4817651 E 604368.5

DRILLING DATA  
Method: Hollow Stem Auger  
Diameter: 200mm  
Date: Aug-09-2024  
REF. NO.: 24-228-100  
ENCL NO.: 3

| SOIL PROFILE         |                                                                                                                                                                          |             | SAMPLES |      |                    | GROUND WATER<br>CONDITIONS | ELEVATION | DYNAMIC CONE PENETRATION<br>RESISTANCE PLOT                                                   |  |  |  | PLASTIC NATURAL LIQUID<br>LIMIT MOISTURE CONTENT LIMIT                  |  |  | POCKET PEN.<br>(Cu) (kPa) | NATURAL UNIT WT<br>(kN/m³) | REMARKS<br>AND<br>GRAIN SIZE<br>DISTRIBUTION<br>(%) |  |
|----------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------|------|--------------------|----------------------------|-----------|-----------------------------------------------------------------------------------------------|--|--|--|-------------------------------------------------------------------------|--|--|---------------------------|----------------------------|-----------------------------------------------------|--|
| (m)<br>ELEV<br>DEPTH | DESCRIPTION                                                                                                                                                              | STRATA PLOT | NUMBER  | TYPE | "N" BLOWS<br>0.3 m |                            |           | SHEAR STRENGTH (kPa)                                                                          |  |  |  | WATER CONTENT (%)                                                       |  |  |                           |                            |                                                     |  |
|                      |                                                                                                                                                                          |             |         |      |                    |                            |           | <div><div></div><div>20406080100</div></div>                                                  |  |  |  | <div><div>W<sub>P</sub></div><div>W</div><div>W<sub>L</sub></div></div> |  |  |                           |                            |                                                     |  |
|                      |                                                                                                                                                                          |             |         |      |                    |                            |           | <div>○ UNCONFINED + FIELD VANE &amp; Sensitivity</div> <div>● QUICK TRIAXIAL × LAB VANE</div> |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 166.9                |                                                                                                                                                                          |             |         |      |                    |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           | GR SA SI CL                |                                                     |  |
| 0.0                  | FILL: clayey silt, trace sand, reddish brown, moist, very stiff                                                                                                          |             | 1       | SS   | 20                 |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 166.1                |                                                                                                                                                                          |             |         |      |                    |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 0.8                  | SILTY CLAY TILL: sandy, trace gravel, brown to reddish brown, moist, very stiff to hard                                                                                  |             | 2       | SS   | 31                 |                            | 166       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
|                      |                                                                                                                                                                          |             | 3       | SS   | 28                 |                            | 165       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
|                      |                                                                                                                                                                          |             | 4       | SS   | 28                 |                            | 164       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
|                      |                                                                                                                                                                          |             | 5       | SS   | 15                 |                            | 163       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 162.4                |                                                                                                                                                                          |             |         |      |                    |                            | 162       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 4.5                  | CLAYEY SILT TILL/SHALE COMPLEX: trace sand, reddish brown, moist, hard                                                                                                   |             | 6       | SS   | 50/<br>30mm        |                            | 161       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 160.9                |                                                                                                                                                                          |             |         |      |                    |                            | 160       |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 6.0                  | SHALE BEDROCK: Queenston Formation, reddish brown, weathered                                                                                                             |             | 7       | SS   | 50/<br>50mm        |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 159.2                |                                                                                                                                                                          |             |         |      |                    |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |
| 7.7                  | END OF BOREHOLE:<br>Notes:<br>1) 50mm dia. monitoring well installed upon completion.<br>2) Water Level Readings:<br><br>Date: Water Level(mbgl):<br>August 27, 2024 dry |             | 8       | SS   | 50/<br>50mm        |                            |           |                                                                                               |  |  |  |                                                                         |  |  |                           |                            |                                                     |  |

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH  
NOTES

+ 3 , × 3 : Numbers refer  
to Sensitivity

○ = 3% Strain at Failure



PROJECT: Additional Geotechnical Investigation

CLIENT: Valery Group

PROJECT LOCATION: Block 297, Oakville, Ontario

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4817684.8 E 604355.2

DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Aug-12-2024

REF. NO.: 24-228-100

ENCL NO.: 4

| SOIL PROFILE |                                                                                                                                 |             | SAMPLES |      |                    | GROUND WATER<br>CONDITIONS | ELEVATION | DYNAMIC CONE PENETRATION<br>RESISTANCE PLOT |  |  |  | PLASTIC NATURAL LIQUID |   |                | POCKET PEN.<br>(Cu) (kPa) | NATURAL UNIT WT<br>(kN/m <sup>3</sup> ) | REMARKS<br>AND<br>GRAIN SIZE<br>DISTRIBUTION<br>(%) |
|--------------|---------------------------------------------------------------------------------------------------------------------------------|-------------|---------|------|--------------------|----------------------------|-----------|---------------------------------------------|--|--|--|------------------------|---|----------------|---------------------------|-----------------------------------------|-----------------------------------------------------|
| (m)          | DESCRIPTION                                                                                                                     | STRATA PLOT | NUMBER  | TYPE | "N" BLOWS<br>0.3 m |                            |           | SHEAR STRENGTH (kPa)                        |  |  |  | W <sub>p</sub>         | W | W <sub>L</sub> |                           |                                         |                                                     |
| 167.2        | <b>GRANULAR FILL:</b> sand and gravel, 150mm<br><b>FILL:</b> clayey silt, trace sand, reddish brown, moist, stiff to very stiff |             | 1       | SS   | 20                 |                            | 167       |                                             |  |  |  |                        |   |                |                           |                                         | GR SA SI CL                                         |
| 166.9        |                                                                                                                                 |             | 2       | SS   | 13                 |                            | 166       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 165.4        |                                                                                                                                 |             | 3       | SS   | 23                 |                            | 165       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 164.9        | <b>SILTY CLAY TILL:</b> some sand, trace gravel, brown to reddish brown, moist, very stiff to hard                              |             | 4       | SS   | 29                 |                            | 164       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 164.4        |                                                                                                                                 |             | 5       | SS   | 50                 |                            | 163       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 163.9        |                                                                                                                                 |             | 6       | SS   | 26                 |                            | 162       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 161.2        | <b>SHALE BEDROCK:</b> Queenston Formation, reddish brown, weathered                                                             |             | 7       | SS   | 50/<br>50mm        |                            | 161       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 159.5        |                                                                                                                                 |             | 8       | SS   | 50/<br>50mm        |                            | 160       |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |
| 157.7        | <b>END OF BOREHOLE:</b><br>Notes:<br>1) No water was encountered during drilling.                                               |             |         |      |                    |                            |           |                                             |  |  |  |                        |   |                |                           |                                         |                                                     |

GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH  
NOTES

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure



PROJECT: Additional Geotechnical Investigation

CLIENT: Valery Group

PROJECT LOCATION: Block 297, Oakville, Ontario

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4817705.9 E 604375.2

## DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Aug-12-2024

REF. NO.: 24-228-100

ENCL NO.: 5

| SOIL PROFILE         |                                                                                                                                                                                    |             | SAMPLES |      |                    | GROUND WATER<br>CONDITIONS | ELEVATION | DYNAMIC CONE PENETRATION<br>RESISTANCE PLOT |  | PLASTIC<br>LIMIT<br>W <sub>P</sub> | NATURAL<br>MOISTURE<br>CONTENT<br>W | LIQUID<br>LIMIT<br>W <sub>L</sub> | POCKET PEN.<br>(C <sub>u</sub> ) (kPa) | NATURAL UNIT WT<br>(kN/m <sup>3</sup> ) | REMARKS<br>AND<br>GRAIN SIZE<br>DISTRIBUTION<br>(%) |
|----------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------|------|--------------------|----------------------------|-----------|---------------------------------------------|--|------------------------------------|-------------------------------------|-----------------------------------|----------------------------------------|-----------------------------------------|-----------------------------------------------------|
| (m)<br>ELEV<br>DEPTH | DESCRIPTION                                                                                                                                                                        | STRATA PLOT | NUMBER  | TYPE | "N" BLOWS<br>0.3 m |                            |           | SHEAR STRENGTH (kPa)                        |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 167.3                |                                                                                                                                                                                    |             |         |      |                    |                            |           | 20 40 60 80 100                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 0.0                  | <b>FILL:</b> clayey silt, trace sand,<br>reddish brown, moist, stiff to very<br>stiff                                                                                              |             | 1       | SS   | 25                 |                            | 167       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 1                    |                                                                                                                                                                                    |             | 2       | SS   | 13                 |                            | 166       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 2                    | trace organics at 1.8m                                                                                                                                                             |             | 3       | SS   | 11                 |                            | 165       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
|                      |                                                                                                                                                                                    |             | 4       | SS   | 12                 |                            | 164       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 164.3                | <b>SILTY CLAY TILL:</b> some sand,<br>trace gravel, brown to reddish<br>brown, moist, hard                                                                                         |             | 5       | SS   | 32                 |                            | 163       |                                             |  |                                    |                                     |                                   |                                        |                                         | 1 14 58 27                                          |
| 3.0                  |                                                                                                                                                                                    |             | 6       | SS   | 50/<br>50mm        |                            | 162       |                                             |  |                                    |                                     |                                   |                                        |                                         | auger grinding                                      |
|                      | greyish brown at 4.6m                                                                                                                                                              |             |         |      |                    |                            | 161       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 161.3                | <b>SHALE BEDROCK:</b> Queenston<br>Formation, reddish brown,<br>weathered                                                                                                          |             | 7       | SS   | 50/<br>50mm        |                            | 160       |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 6.0                  |                                                                                                                                                                                    |             | 8       | SS   | 50/<br>75mm        |                            |           |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 159.6                | <b>END OF BOREHOLE:</b><br>Notes:<br>1) 50mm dia. monitoring well<br>installed upon completion.<br>2) Water Level Readings:<br><br>Date: Water Level(mbgl):<br>August 27, 2024 dry |             |         |      |                    |                            |           |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |
| 7.7                  |                                                                                                                                                                                    |             |         |      |                    |                            |           |                                             |  |                                    |                                     |                                   |                                        |                                         |                                                     |

## GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH  
NOTES+ 3 , × 3 : Numbers refer  
to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 24-228-100GEO.GPJ DS.GDT 24-9-5



PROJECT: Additional Geotechnical Investigation

CLIENT: Valery Group

PROJECT LOCATION: Block 297, Oakville, Ontario

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4817725.4 E 604378.3

## DRILLING DATA

Method: Hollow Stem Auger

Diameter: 200mm

Date: Aug-13-2024

REF. NO.: 24-228-100

ENCL NO.: 6

| SOIL PROFILE  |                                                                                                                                                                          |             | SAMPLES |      |                    | GROUND WATER<br>CONDITIONS | ELEVATION               | DYNAMIC CONE PENETRATION<br>RESISTANCE PLOT |  |  |  |  | POCKET PEN.<br>(Cu) (kPa) | NATURAL UNIT WT<br>(kN/m <sup>3</sup> ) | REMARKS<br>AND<br>GRAIN SIZE<br>DISTRIBUTION<br>(%) |
|---------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------|---------|------|--------------------|----------------------------|-------------------------|---------------------------------------------|--|--|--|--|---------------------------|-----------------------------------------|-----------------------------------------------------|
| (m)           | DESCRIPTION                                                                                                                                                              | STRATA PLOT | NUMBER  | TYPE | "N" BLOWS<br>0.3 m |                            |                         | SHEAR STRENGTH (kPa)                        |  |  |  |  |                           |                                         |                                                     |
| 167.4         |                                                                                                                                                                          |             |         |      |                    |                            |                         | 20 40 60 80 100                             |  |  |  |  |                           |                                         |                                                     |
| ELEV<br>DEPTH |                                                                                                                                                                          |             |         |      |                    |                            |                         | 20 40 60 80 100                             |  |  |  |  |                           |                                         |                                                     |
| 167.4         |                                                                                                                                                                          |             |         |      |                    |                            |                         | 20 40 60 80 100                             |  |  |  |  |                           |                                         |                                                     |
| 0.0           | FILL: clayey silt, trace sand, some gravels, reddish brown, moist, stiff to very stiff                                                                                   |             | 1       | SS   | 12                 |                            | 167                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 1             |                                                                                                                                                                          |             | 2       | SS   | 18                 |                            | 166                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 165.6         |                                                                                                                                                                          |             | 3       | SS   | 15                 |                            | 165                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 1.8           | SILTY CLAY TILL: sandy, trace gravel, brown to reddish brown, moist, very stiff                                                                                          |             | 4       | SS   | 28                 |                            | 165                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 2             |                                                                                                                                                                          |             | 5       | SS   | 27                 |                            | 164.4 m<br>Aug 27, 2024 |                                             |  |  |  |  |                           |                                         |                                                     |
| 3             |                                                                                                                                                                          |             |         |      |                    |                            |                         |                                             |  |  |  |  |                           |                                         |                                                     |
| 4             |                                                                                                                                                                          |             |         |      |                    |                            |                         |                                             |  |  |  |  |                           |                                         |                                                     |
| 5             | greyish brown at 4.6m                                                                                                                                                    |             | 6       | AS   | 26                 |                            | 163                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 6             |                                                                                                                                                                          |             |         |      |                    |                            | 162                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 7             | grey at 6.1m                                                                                                                                                             |             | 7       | SS   | 25                 |                            | 161                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 159.8         |                                                                                                                                                                          |             |         |      |                    |                            | 160                     |                                             |  |  |  |  |                           |                                         |                                                     |
| 159.8         | SHALE BEDROCK: Queenston Formation, reddish brown, weathered                                                                                                             |             | 8       | CG   | 50/75mm            |                            |                         |                                             |  |  |  |  |                           |                                         |                                                     |
| 7.7           | END OF BOREHOLE:<br>Notes:<br>1) 50mm dia. monitoring well installed upon completion.<br>2) Water Level Readings:<br><br>Date: Water Level(mbgl):<br>August 27, 2024 3.0 |             |         |      |                    |                            |                         |                                             |  |  |  |  |                           |                                         |                                                     |

## GROUNDWATER ELEVATIONS

Measurement 1st 2nd 3rd 4th

GRAPH  
NOTES

+ 3, × 3: Numbers refer to Sensitivity

○ = 3% Strain at Failure

PROJECT: Additional Geotechnical Investigation

CLIENT: Valery Group

PROJECT LOCATION: Block 297, Oakville, Ontario

DATUM: Geodetic

BH LOCATION: See Drawing 1 N 4817709.3 E 604408.1

**DRILLING DATA**

Method: Hollow Stem Auger/Mud Rotary

Diameter: 200mm

Date: Aug-13-2024

REF. NO.: 24-228-100

ENCL NO.: 7

| SOIL PROFILE  |                                                                                                    |                                                                                   | SAMPLES |      |                    | GROUND WATER<br>CONDITIONS | ELEVATION | DYNAMIC CONE PENETRATION<br>RESISTANCE PLOT |                                             |    |    | PLASTIC<br>LIMIT<br>W <sub>P</sub> | NATURAL<br>MOISTURE<br>CONTENT<br>W | LIQUID<br>LIMIT<br>W <sub>L</sub> | POCKET PEN<br>(C <sub>u</sub> ) (kPa) | NATURAL UNIT WT<br>(kN/m <sup>3</sup> ) | REMARKS<br>AND<br>GRAIN SIZE<br>DISTRIBUTION<br>(%) |                   |    |     |
|---------------|----------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|---------|------|--------------------|----------------------------|-----------|---------------------------------------------|---------------------------------------------|----|----|------------------------------------|-------------------------------------|-----------------------------------|---------------------------------------|-----------------------------------------|-----------------------------------------------------|-------------------|----|-----|
| (m)           | DESCRIPTION                                                                                        | STRATA PLOT                                                                       | NUMBER  | TYPE | "N" BLOWS<br>0.3 m |                            |           | SHEAR STRENGTH (kPa)                        |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     | WATER CONTENT (%) |    |     |
| ELEV<br>DEPTH |                                                                                                    |                                                                                   |         |      |                    |                            |           | ○ UNCONFINED<br>● QUICK TRIAXIAL            | + FIELD VANE<br>& Sensitivity<br>× LAB VANE | 20 | 40 |                                    |                                     |                                   |                                       |                                         |                                                     | 60                | 80 | 100 |
| 167.3         |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         | GR SA SI CL                                         |                   |    |     |
| 0.0           | <b>FILL:</b> clayey silt, trace sand, some gravels, reddish brown, moist, firm to very stiff       |  | 1       | SS   | 7                  |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   | 2       | SS   | 20                 |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
| 165.5         |                                                                                                    |                                                                                   | 3       | SS   | 21                 |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
| 1.8           | <b>SILTY CLAY TILL:</b> some sand, trace gravel, brown to reddish brown, moist, very stiff to hard |  |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   | 4       | SS   | 35                 |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   | 5       | SS   | 28                 |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      |                    |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |
|               |                                                                                                    |                                                                                   |         |      | </                 |                            |           |                                             |                                             |    |    |                                    |                                     |                                   |                                       |                                         |                                                     |                   |    |     |

W. L. 164.3 m  
Aug 27, 2024

**GROUNDWATER ELEVATIONS**

Measurement 1st 2nd 3rd 4th

**GRAPH NOTES**

+ 3 , × 3 : Numbers refer to Sensitivity

○ = 3% Strain at Failure

DS SOIL LOG-2021-FINAL 24-228-100GEO.GPJ DS GDT 24-9-5

## **Appendix B: Hydraulic Conductivity Analysis**

|                                                                                                                                                                                                                                                        |  |                                 |                                     |                          |  |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|---------------------------------|-------------------------------------|--------------------------|--|
|                                                                                                                                                                                                                                                        |  |                                 | <b>Slug Test Analysis Report</b>    |                          |  |
|                                                                                                                                                                                                                                                        |  |                                 | Project: Hydrogeology Investigation |                          |  |
|                                                                                                                                                                                                                                                        |  |                                 | Number: 24-228-100                  |                          |  |
|                                                                                                                                                                                                                                                        |  |                                 | Client: Valery Homes                |                          |  |
| Location: Block 297, Oakville, ON                                                                                                                                                                                                                      |  | Slug Test: BH/MW 24-1           |                                     | Test Well: BH/MW 24-1    |  |
| Test Conducted by:                                                                                                                                                                                                                                     |  |                                 |                                     | Test Date: 10/1/2024     |  |
| Analysis Performed by: PP                                                                                                                                                                                                                              |  | Hvorslev                        |                                     | Analysis Date: 10/1/2024 |  |
| Aquifer Thickness: 1.95 m                                                                                                                                                                                                                              |  |                                 |                                     |                          |  |
| <div><div></div><div><div>Time [s]</div><div><div>0</div><div>600</div><div>1200</div><div>1800</div><div>2400</div><div>3000</div></div><div><div>10</div><div>1</div><div>0</div><div>0</div></div><div><div>h/h<sub>0</sub></div></div></div></div> |  |                                 |                                     |                          |  |
| Calculation using Hvorslev                                                                                                                                                                                                                             |  |                                 |                                     |                          |  |
| Observation Well                                                                                                                                                                                                                                       |  | Hydraulic Conductivity<br>[m/s] |                                     |                          |  |
| BH/MW 24-1                                                                                                                                                                                                                                             |  | 3.37 × 10 <sup>-7</sup>         |                                     |                          |  |
|                                                                                                                                                                                                                                                        |  |                                 |                                     |                          |  |

|                                       |  |                                     |  |                          |  |
|---------------------------------------|--|-------------------------------------|--|--------------------------|--|
|                                       |  | Slug Test Analysis Report           |  |                          |  |
|                                       |  | Project: Hydrogeology Investigation |  |                          |  |
|                                       |  | Number: 24-228-100                  |  |                          |  |
|                                       |  | Client: Valery Homes                |  |                          |  |
| Location: Block 297, Oakville, ON     |  | Slug Test: BH/MW 24-5               |  | Test Well: BH/MW 24-5    |  |
| Test Conducted by:                    |  |                                     |  | Test Date: 10/1/2024     |  |
| Analysis Performed by: PP             |  | Hvorslev                            |  | Analysis Date: 10/1/2024 |  |
| Aquifer Thickness: 3.09 m             |  |                                     |  |                          |  |
| <div><p>Time [s]</p><p>h/h0</p></div> |  |                                     |  |                          |  |
| Calculation using Hvorslev            |  |                                     |  |                          |  |
| Observation Well                      |  | Hydraulic Conductivity [m/s]        |  |                          |  |
| BH/MW 24-5                            |  | $4.87 \times 10^{-8}$               |  |                          |  |
|                                       |  |                                     |  |                          |  |

|                                                                                                                                                                                                                                                                                                                                                                                               |      | Slug Test Analysis Report           |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------|-------------------------------------|--|--------------------------|--|----------|------|---|-----|------|-----|------|------|------|-----|------|------|------|-----|
|                                                                                                                                                                                                                                                                                                                                                                                               |      | Project: Hydrogeology Investigation |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
|                                                                                                                                                                                                                                                                                                                                                                                               |      | Number: 24-228-100                  |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
|                                                                                                                                                                                                                                                                                                                                                                                               |      | Client: Valery Homes                |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Location: Block 297, Oakville, ON                                                                                                                                                                                                                                                                                                                                                             |      | Slug Test: BH/MW 24-6               |  | Test Well: BH/MW 24-6    |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Test Conducted by:                                                                                                                                                                                                                                                                                                                                                                            |      |                                     |  | Test Date: 10/1/2024     |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Analysis Performed by: PP                                                                                                                                                                                                                                                                                                                                                                     |      | Hvorslev                            |  | Analysis Date: 10/1/2024 |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Aquifer Thickness: 7.38 m                                                                                                                                                                                                                                                                                                                                                                     |      |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| <div><p>Time [s]</p><table border="1"><caption>Approximate data points from the graph</caption><thead><tr><th>Time [s]</th><th>h/h0</th></tr></thead><tbody><tr><td>0</td><td>1.0</td></tr><tr><td>1000</td><td>1.0</td></tr><tr><td>2000</td><td>0.95</td></tr><tr><td>3000</td><td>0.9</td></tr><tr><td>4000</td><td>0.85</td></tr><tr><td>5000</td><td>0.8</td></tr></tbody></table></div> |      |                                     |  |                          |  | Time [s] | h/h0 | 0 | 1.0 | 1000 | 1.0 | 2000 | 0.95 | 3000 | 0.9 | 4000 | 0.85 | 5000 | 0.8 |
| Time [s]                                                                                                                                                                                                                                                                                                                                                                                      | h/h0 |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 0                                                                                                                                                                                                                                                                                                                                                                                             | 1.0  |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 1000                                                                                                                                                                                                                                                                                                                                                                                          | 1.0  |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 2000                                                                                                                                                                                                                                                                                                                                                                                          | 0.95 |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 3000                                                                                                                                                                                                                                                                                                                                                                                          | 0.9  |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 4000                                                                                                                                                                                                                                                                                                                                                                                          | 0.85 |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| 5000                                                                                                                                                                                                                                                                                                                                                                                          | 0.8  |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Calculation using Hvorslev                                                                                                                                                                                                                                                                                                                                                                    |      |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| Observation Well                                                                                                                                                                                                                                                                                                                                                                              |      | Hydraulic Conductivity [m/s]        |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
| BH/MW 24-6                                                                                                                                                                                                                                                                                                                                                                                    |      | $3.18 \times 10^{-8}$               |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |
|                                                                                                                                                                                                                                                                                                                                                                                               |      |                                     |  |                          |  |          |      |   |     |      |     |      |      |      |     |      |      |      |     |

**Appendix C: Groundwater Quality  
Certificate of Analysis**



## FINAL REPORT

CA40200-AUG24 R1

24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

Prepared for

**DS Consultants**

## First Page

### CLIENT DETAILS

Client DS Consultants

Address 6221 Highway 7 Unit 16  
Vaughan, Ontario  
L4H 0K8, Canada

Contact Pradeep Patel

Telephone 647-332-3482

Facsimile 905-264-2685

Email ppatel@dsconsultants.ca

Project 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

Order Number

Samples Ground Water (1)

### LABORATORY DETAILS

Project Specialist Maarit Wolfe, Hon.B.Sc

Laboratory SGS Canada Inc.

Address 185 Concession St., Lakefield ON, K0L 2H0

Telephone 705-652-2000

Facsimile 705-652-6365

Email Maarit.Wolfe@sgs.com

SGS Reference CA40200-AUG24

Received 08/29/2024

Approved 09/06/2024

Report Number CA40200-AUG24 R1

Date Reported 09/06/2024

### COMMENTS

RL - SGS Reporting Limit

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 036246

### SIGNATORIES

Maarit Wolfe, Hon.B.Sc





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# FINAL REPORT

CA40200-AUG24 R1

**Client:** DS Consultants

**Project:** 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

**Project Manager:** Pradeep Patel

**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter                              | Units     | RL  | L1 | Result |
|----------------------------------------|-----------|-----|----|--------|
| <b>General Chemistry</b>               |           |     |    |        |
| Carbonaceous Biochemical Oxygen Demand | mg/L      | 2   |    | < 4 †  |
| Biochemical Oxygen Demand (BOD5)       | mg/L      | 2   | 15 | < 4 †  |
| Total Suspended Solids                 | mg/L      | 2   | 15 | 73     |
| Total Kjeldahl Nitrogen                | as N mg/L | 0.5 |    | 2.0    |

## Metals and Inorganics

|                    |      |          |       |          |
|--------------------|------|----------|-------|----------|
| Cyanide (total)    | mg/L | 0.01     | 0.02  | < 0.01   |
| Fluoride           | mg/L | 0.06     |       | 0.51     |
| Sulphate           | mg/L | 2        |       | 1300     |
| Aluminum (total)   | mg/L | 0.001    |       | 0.939    |
| Antimony (total)   | mg/L | 0.0009   |       | < 0.0009 |
| Arsenic (total)    | mg/L | 0.0002   | 0.02  | 0.0043   |
| Beryllium (total)  | mg/L | 0.000007 |       | 0.000050 |
| Cadmium (total)    | mg/L | 0.000003 | 0.008 | 0.000059 |
| Chromium (total)   | mg/L | 0.00008  | 0.08  | 0.00130  |
| Cobalt (total)     | mg/L | 0.000004 |       | 0.00507  |
| Copper (total)     | mg/L | 0.001    | 0.04  | 0.003    |
| Iron (total)       | mg/L | 0.007    |       | 1.18     |
| Lead (total)       | mg/L | 0.00009  | 0.12  | 0.00069  |
| Manganese (total)  | mg/L | 0.00001  | 0.05  | 0.208    |
| Molybdenum (total) | mg/L | 0.0004   |       | 0.0104   |
| Nickel (total)     | mg/L | 0.0001   | 0.08  | 0.0044   |



FINAL REPORT

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**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9  
**Sample Name** BH24-6  
**Sample Matrix** Ground Water  
**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter                         | Units     | RL      | L1    | Result    |
|-----------------------------------|-----------|---------|-------|-----------|
| Metals and Inorganics (continued) |           |         |       |           |
| Phosphorus (total)                | mg/L      | 0.003   | 0.4   | 0.039     |
| Selenium (total)                  | mg/L      | 0.00004 | 0.02  | 0.00127   |
| Silver (total)                    | mg/L      | 0.00005 | 0.12  | < 0.00005 |
| Tin (total)                       | mg/L      | 0.00006 |       | 0.00480   |
| Titanium (total)                  | mg/L      | 0.0001  |       | 0.0074    |
| Zinc (total)                      | mg/L      | 0.002   | 0.04  | 0.037     |
| Microbiology                      |           |         |       |           |
| E. Coli                           | cfu/100mL | 0       | 200   | < 2 †     |
| Nonylphenol and Ethoxylates       |           |         |       |           |
| Nonylphenol                       | mg/L      | 0.001   | 0.001 | < 0.001   |
| Nonylphenol Ethoxylates           | mg/L      | 0.01    | 0.01  | < 0.01    |
| Oil and Grease                    |           |         |       |           |
| Oil & Grease (total)              | mg/L      | 2       |       | < 2       |
| Oil & Grease (animal/vegetable)   | mg/L      | 4       |       | < 4       |
| Oil & Grease (mineral/synthetic)  | mg/L      | 4       |       | < 4       |



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MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter                                | Units   | RL      | L1      | Result    |
|------------------------------------------|---------|---------|---------|-----------|
| <b>Organochlorine Pests (OCs)</b>        |         |         |         |           |
| Hexachlorobenzene                        | mg/L    | 0.00001 | 0.00004 | < 0.00001 |
| <b>Other (ORP)</b>                       |         |         |         |           |
| pH                                       | No unit | 0.05    | 8.5     | 7.54      |
| Chromium VI                              | mg/L    | 0.0002  | 0.04    | < 0.0002  |
| Mercury (total)                          | mg/L    | 0.00001 | 0.0004  | < 0.00001 |
| <b>PAHs</b>                              |         |         |         |           |
| Benzo(b+j)fluoranthene                   | mg/L    | 0.0001  |         | < 0.0001  |
| <b>PCBs</b>                              |         |         |         |           |
| Polychlorinated Biphenyls (PCBs) - Total | mg/L    | 0.0001  | 0.0004  | < 0.0001  |
| <b>Pesticides</b>                        |         |         |         |           |
| Aldrin + Dieldrin                        | mg/L    | 0.00002 | 0.00008 | < 0.00002 |
| Chlordane (total)                        | mg/L    | 0.00002 | 0.04    | < 0.001 ↑ |
| DDT+Metabolites                          | mg/L    | 0.00004 |         | < 0.00004 |
| op-DDT                                   | mg/L    | 0.00002 |         | < 0.00002 |
| pp-DDD                                   | mg/L    | 0.00002 |         | < 0.00002 |
| pp-DDE                                   | mg/L    | 0.00001 |         | < 0.00001 |
| pp-DDT                                   | mg/L    | 0.00002 |         | < 0.00002 |
| o,p-DDD                                  | mg/L    | 0.00002 |         | < 0.00002 |
| o,p-DDE                                  | mg/L    | 0.00001 |         | < 0.00001 |
| Mirex                                    | mg/L    | 0.001   | 0.04    | < 0.001   |
| Hexachlorocyclohexane                    | mg/L    | 0.001   | 0.04    | < 0.001   |



# FINAL REPORT

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**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter | Units | RL | L1 | Result |
|-----------|-------|----|----|--------|
|-----------|-------|----|----|--------|

## Phenols

|                |      |       |       |       |
|----------------|------|-------|-------|-------|
| 4AAP-Phenolics | mg/L | 0.002 | 0.008 | 0.003 |
|----------------|------|-------|-------|-------|

## SVOCs

|                            |      |        |        |          |
|----------------------------|------|--------|--------|----------|
| PAHs (Total)               | mg/L |        | 0.002  | < 0.001  |
| Perylene                   | mg/L | 0.0005 |        | < 0.0005 |
| di-n-Butyl Phthalate       | mg/L | 0.002  | 0.015  | < 0.002  |
| Bis(2-ethylhexyl)phthalate | mg/L | 0.002  | 0.0088 | < 0.002  |
| 3,3-Dichlorobenzidine      | mg/L | 0.0005 | 0.0008 | < 0.0005 |
| Pentachlorophenol          | mg/L | 0.0005 | 0.002  | < 0.0005 |

## SVOCs - PAHs

|                         |      |        |  |          |
|-------------------------|------|--------|--|----------|
| Naphthalene             | mg/L | 0.0005 |  | < 0.0005 |
| 7Hdibenzo(c,g)carbazole | mg/L | 0.0001 |  | < 0.0001 |
| Anthracene              | mg/L | 0.0001 |  | < 0.0001 |
| Benzo(a)anthracene      | mg/L | 0.0001 |  | < 0.0001 |
| Benzo(a)pyrene          | mg/L | 0.0001 |  | < 0.0001 |
| Benzo(e)pyrene          | mg/L | 0.0001 |  | < 0.0001 |
| Benzo(ghi)perylene      | mg/L | 0.0002 |  | < 0.0002 |
| Benzo(k)fluoranthene    | mg/L | 0.0001 |  | < 0.0001 |
| Chrysene                | mg/L | 0.0001 |  | < 0.0001 |
| Dibenzo(a,h)anthracene  | mg/L | 0.0001 |  | < 0.0001 |
| Dibenzo(a,i)pyrene      | mg/L | 0.0001 |  | < 0.0001 |
| Dibenzo(a,j)acridine    | mg/L | 0.0001 |  | < 0.0001 |



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MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter                | Units | RL     | L1 | Result   |
|--------------------------|-------|--------|----|----------|
| SVOCs - PAHs (continued) |       |        |    |          |
| Fluoranthene             | mg/L  | 0.0001 |    | < 0.0001 |
| Indeno(1,2,3-cd)pyrene   | mg/L  | 0.0002 |    | < 0.0002 |
| Phenanthrene             | mg/L  | 0.0001 |    | < 0.0001 |
| Pyrene                   | mg/L  | 0.0001 |    | < 0.0001 |

## VOCs

|                                         |      |        |        |          |
|-----------------------------------------|------|--------|--------|----------|
| Chloroform                              | mg/L | 0.0005 | 0.002  | 0.0052   |
| 1,2-Dichlorobenzene                     | mg/L | 0.0005 | 0.0056 | < 0.0005 |
| 1,4-Dichlorobenzene                     | mg/L | 0.0005 | 0.0068 | < 0.0005 |
| cis-1,2-Dichloroethylene                | mg/L | 0.0005 | 0.0056 | < 0.0005 |
| trans-1,3-Dichloropropene               | mg/L | 0.0005 | 0.0056 | < 0.0005 |
| Methylene Chloride                      | mg/L | 0.0005 | 0.0052 | < 0.0005 |
| Tetrachloroethylene (perchloroethylene) | mg/L | 0.0005 | 0.0044 | < 0.0005 |
| Trichloroethylene                       | mg/L | 0.0005 | 0.0076 | < 0.0005 |
| 1,1,2,2-Tetrachloroethane               | mg/L | 0.0005 | 0.017  | < 0.0005 |



FINAL REPORT

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**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9  
**Sample Name** BH24-6  
**Sample Matrix** Ground Water  
**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Oakville Sewer Use By Law - Storm Sewer Discharge - BL\_2009\_031

| Parameter      | Units | RL     | L1    | Result   |
|----------------|-------|--------|-------|----------|
| VOCs - BTEX    |       |        |       |          |
| Benzene        | mg/L  | 0.0005 | 0.002 | < 0.0005 |
| Ethylbenzene   | mg/L  | 0.0005 | 0.002 | < 0.0005 |
| Toluene        | mg/L  | 0.0005 | 0.002 | < 0.0005 |
| m-p-xylene     | mg/L  | 0.0005 |       | < 0.0005 |
| o-xylene       | mg/L  | 0.0005 |       | < 0.0005 |
| Xylene (total) | mg/L  | 0.0005 |       | < 0.0005 |



EXCEEDANCE SUMMARY

|           |        |       |        |                                                                                                     |
|-----------|--------|-------|--------|-----------------------------------------------------------------------------------------------------|
|           |        |       |        | SANSEW / WATER<br>/ - - Oakville Sewer<br>Use By Law -<br>Storm Sewer<br>Discharge -<br>BL_2009_031 |
| Parameter | Method | Units | Result | L1                                                                                                  |

BH24-6

|                        |                   |      |        |       |
|------------------------|-------------------|------|--------|-------|
| Chloroform             | EPA 5030B/8260C   | mg/L | 0.0052 | 0.002 |
| Total Suspended Solids | SM 2540D          | mg/L | 73     | 15    |
| Manganese              | SM 3030/EPA 200.8 | mg/L | 0.208  | 0.05  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Anions by discrete analyzer  
Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

| Parameter | QC batch<br>Reference | Units | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|-------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |       |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |       |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Sulphate  | DIO5001-SEP24         | mg/L  | 2  | <2              | ND        | 20        | 107                      | 80                     | 120  | 107                      | 75                     | 125  |

Biochemical Oxygen Demand  
Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

| Parameter                              | QC batch<br>Reference | Units           | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------------------------|-----------------------|-----------------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                        |                       |                 |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                        |                       |                 |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Carbonaceous Biochemical Oxygen Demand | BOD0061-AUG24         | (CBOD5)<br>mg/L | 2  | < 2             | 4         | 30        | 97                       | 70                     | 130  | 96                       | 70                     | 130  |
| Biochemical Oxygen Demand (BOD5)       | BOD0062-AUG24         | mg/L            | 2  | < 2             | 3         | 30        | 99                       | 70                     | 130  | 123                      | 70                     | 130  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Cyanide by SFA  
Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

| Parameter       | QC batch<br>Reference | Units | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------------|-----------------------|-------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                 |                       |       |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                 |                       |       |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Cyanide (total) | SKA0004-SEP24         | mg/L  | 0.01 | <0.01           | ND        | 10        | 94                       | 90                     | 110  | NV                       | 75                     | 125  |

Fluoride by Specific Ion Electrode  
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

| Parameter | QC batch<br>Reference | Units | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|-------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |       |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |       |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Fluoride  | EWL0683-AUG24         | mg/L  | 0.06 | <0.06           | 7         | 10        | 101                      | 90                     | 110  | 105                      | 75                     | 125  |

Hexavalent Chromium by SFA  
Method: EPA218.6/EPA3060A | Internal ref.: ME-CA-IENVISKA-LAK-AN-012

| Parameter   | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|             |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|             |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Chromium VI | SKA0005-SEP24         | mg/L  | 0.0002 | <0.0002         | ND        | 20        | 99                       | 80                     | 120  | NV                       | 75                     | 125  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Mercury by CVAAS  
Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

| Parameter       | QC batch<br>Reference | Units | RL      | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------------|-----------------------|-------|---------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                 |                       |       |         |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                 |                       |       |         |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Mercury (total) | EHG0067-AUG24         | mg/L  | 0.00001 | < 0.00001       | ND        | 20        | 102                      | 80                     | 120  | 70                       | 70                     | 130  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Metals in aqueous samples - ICP-MS  
Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-ENVISPE-LAK-AN-006

| Parameter          | QC batch<br>Reference | Units | RL       | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|--------------------|-----------------------|-------|----------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                    |                       |       |          |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                    |                       |       |          |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Silver (total)     | EMS0342-AUG24         | mg/L  | 0.00005  | <0.00005        | ND        | 20        | 100                      | 90                     | 110  | 93                       | 70                     | 130  |
| Aluminum (total)   | EMS0342-AUG24         | mg/L  | 0.001    | <0.001          | ND        | 20        | 104                      | 90                     | 110  | 99                       | 70                     | 130  |
| Arsenic (total)    | EMS0342-AUG24         | mg/L  | 0.0002   | <0.0002         | ND        | 20        | 99                       | 90                     | 110  | 103                      | 70                     | 130  |
| Beryllium (total)  | EMS0342-AUG24         | mg/L  | 0.000007 | <0.000007       | ND        | 20        | 103                      | 90                     | 110  | 97                       | 70                     | 130  |
| Cadmium (total)    | EMS0342-AUG24         | mg/L  | 0.000003 | <0.000003       | 3         | 20        | 97                       | 90                     | 110  | 101                      | 70                     | 130  |
| Cobalt (total)     | EMS0342-AUG24         | mg/L  | 0.000004 | <0.000004       | 2         | 20        | 101                      | 90                     | 110  | 104                      | 70                     | 130  |
| Chromium (total)   | EMS0342-AUG24         | mg/L  | 0.00008  | <0.00008        | 0         | 20        | 100                      | 90                     | 110  | 104                      | 70                     | 130  |
| Copper (total)     | EMS0342-AUG24         | mg/L  | 0.001    | <0.001          | ND        | 20        | 99                       | 90                     | 110  | 103                      | 70                     | 130  |
| Iron (total)       | EMS0342-AUG24         | mg/L  | 0.007    | <0.007          | 0         | 20        | 103                      | 90                     | 110  | 100                      | 70                     | 130  |
| Manganese (total)  | EMS0342-AUG24         | mg/L  | 0.00001  | <0.00001        | 1         | 20        | 101                      | 90                     | 110  | 99                       | 70                     | 130  |
| Molybdenum (total) | EMS0342-AUG24         | mg/L  | 0.0004   | <0.0004         | ND        | 20        | 101                      | 90                     | 110  | 108                      | 70                     | 130  |
| Nickel (total)     | EMS0342-AUG24         | mg/L  | 0.0001   | <0.0001         | 7         | 20        | 101                      | 90                     | 110  | 106                      | 70                     | 130  |
| Lead (total)       | EMS0342-AUG24         | mg/L  | 0.00009  | <0.00009        | 5         | 20        | 97                       | 90                     | 110  | 102                      | 70                     | 130  |
| Phosphorus (total) | EMS0342-AUG24         | mg/L  | 0.003    | <0.003          | 7         | 20        | 98                       | 90                     | 110  | NV                       | 70                     | 130  |
| Antimony (total)   | EMS0342-AUG24         | mg/L  | 0.0009   | <0.0009         | ND        | 20        | 102                      | 90                     | 110  | 109                      | 70                     | 130  |
| Selenium (total)   | EMS0342-AUG24         | mg/L  | 0.00004  | <0.00004        | 18        | 20        | 99                       | 90                     | 110  | 92                       | 70                     | 130  |
| Tin (total)        | EMS0342-AUG24         | mg/L  | 0.00006  | <0.00006        | ND        | 20        | 103                      | 90                     | 110  | NV                       | 70                     | 130  |
| Titanium (total)   | EMS0342-AUG24         | mg/L  | 0.0001   | <0.0001         | 9         | 20        | 103                      | 90                     | 110  | NV                       | 70                     | 130  |
| Zinc (total)       | EMS0342-AUG24         | mg/L  | 0.002    | <0.002          | 0         | 20        | 103                      | 90                     | 110  | 71                       | 70                     | 130  |



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CA40200-AUG24 R1

QC SUMMARY

Microbiology  
Method: SM 9222D | Internal ref.: ME-CA-IENVIMIC-LAK-AN-006

| Parameter | QC batch<br>Reference | Units     | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|-----------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |           |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |           |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| E. Coli   | BAC9502-AUG24         | cfu/100mL | -  | ACCEPTED        | ACCEPTED  |           |                          |                        |      |                          |                        |      |
|           |                       |           |    |                 | D         |           |                          |                        |      |                          |                        |      |

Nonylphenol and Ethoxylates  
Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

| Parameter   | QC batch<br>Reference | Units | RL    | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-------------|-----------------------|-------|-------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|             |                       |       |       |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|             |                       |       |       |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Nonylphenol | GCM0008-SEP24         | mg/L  | 0.001 | <0.001          |           |           | 94                       | 55                     | 120  |                          |                        |      |

Oil & Grease  
Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter            | QC batch<br>Reference | Units | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------|-----------------------|-------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                      |                       |       |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                      |                       |       |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Oil & Grease (total) | GCM0039-SEP24         | mg/L  | 2  | <2              | NSS       | 20        | 106                      | 75                     | 125  |                          |                        |      |



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CA40200-AUG24 R1

QC SUMMARY

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter                        | QC batch Reference | Units | RL | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|----------------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                                  |                    |       |    |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                                  |                    |       |    |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Oil & Grease (animal/vegetable)  | GCM0039-SEP24      | mg/L  | 4  | < 4          | NSS       | 20     | NA                 | 70                  | 130  |                     |                     |      |
| Oil & Grease (mineral/synthetic) | GCM0039-SEP24      | mg/L  | 4  | < 4          | NSS       | 20     | NA                 | 70                  | 130  |                     |                     |      |

Pesticides

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-018

| Parameter             | QC batch Reference | Units | RL      | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|-----------------------|--------------------|-------|---------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                       |                    |       |         |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                       |                    |       |         |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Hexachlorobenzene     | GCM0063-SEP24      | mg/L  | 0.00001 | < 0.00001    | NSS       | 30     | 91                 | 50                  | 140  | 88                  | 50                  | 140  |
| Hexachlorocyclohexane | GCM0063-SEP24      | mg/L  | 0.001   | < 0.001      | NSS       | 30     | 95                 | 50                  | 140  | 93                  | 50                  | 140  |
| Mirex                 | GCM0063-SEP24      | mg/L  | 0.001   | < 0.001      | NSS       | 30     | 95                 | 50                  | 140  | 83                  | 50                  | 140  |
| o,p-DDD               | GCM0063-SEP24      | mg/L  | 0.00002 | < 0.00002    | NSS       | 30     | 97                 | 50                  | 140  | 93                  | 50                  | 140  |
| o,p-DDE               | GCM0063-SEP24      | mg/L  | 0.00001 | < 0.00001    | NSS       | 30     | 97                 | 50                  | 140  | 97                  | 50                  | 140  |
| op-DDT                | GCM0063-SEP24      | mg/L  | 0.00002 | < 0.00002    | NSS       | 30     | 98                 | 50                  | 140  | 96                  | 50                  | 140  |
| pp-DDD                | GCM0063-SEP24      | mg/L  | 0.00002 | < 0.00002    | NSS       | 30     | 99                 | 50                  | 140  | 102                 | 50                  | 140  |
| pp-DDE                | GCM0063-SEP24      | mg/L  | 0.00001 | < 0.00001    | NSS       | 30     | 97                 | 50                  | 140  | 92                  | 50                  | 140  |
| pp-DDT                | GCM0063-SEP24      | mg/L  | 0.00002 | < 0.00002    | NSS       | 30     | 102                | 50                  | 140  | 105                 | 50                  | 140  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

pH  
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

| Parameter | QC batch<br>Reference | Units   | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|---------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |         |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |         |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| pH        | EWL0675-AUG24         | No unit | 0.05 | NA              | 0         |           | 100                      |                        |      | NA                       |                        |      |

Phenols by SFA  
Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

| Parameter      | QC batch<br>Reference | Units | RL    | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------|-----------------------|-------|-------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                |                       |       |       |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                |                       |       |       |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 4AAP-Phenolics | SKA0002-SEP24         | mg/L  | 0.002 | <0.002          | 7         | 10        | 100                      | 80                     | 120  | 106                      | 75                     | 125  |

Polychlorinated Biphenyls  
Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

| Parameter                                   | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|---------------------------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                             |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                             |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Polychlorinated Biphenyls (PCBs) -<br>Total | GCM0009-SEP24         | mg/L  | 0.0001 | <0.0001         | NSS       | 30        | 91                       | 60                     | 140  | NSS                      | 60                     | 140  |



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CA40200-AUG24 R1

QC SUMMARY

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter                  | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                            |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                            |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 3,3-Dichlorobenzidine      | GCM0035-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 107                      | 30                     | 130  | NSS                      | 30                     | 130  |
| 7Hdibenzo(c,g)carbazole    | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 89                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Anthracene                 | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 88                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(a)anthracene         | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 93                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(a)pyrene             | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 93                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(b+j)fluoranthene     | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(e)pyrene             | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 89                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(ghi)perylene         | GCM0037-SEP24         | mg/L  | 0.0002 | < 0.0002        | NSS       | 30        | 96                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(k)fluoranthene       | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 100                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Bis(2-ethylhexyl)phthalate | GCM0037-SEP24         | mg/L  | 0.002  | < 0.002         | NSS       | 30        | 102                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Chrysene                   | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 95                       | 50                     | 140  | NSS                      | 50                     | 140  |
| di-n-Butyl Phthalate       | GCM0037-SEP24         | mg/L  | 0.002  | < 0.002         | NSS       | 30        | 102                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,h)anthracene     | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,i)pyrene         | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 83                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,j)acridine       | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 88                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Fluoranthene               | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 95                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Indeno(1,2,3-cd)pyrene     | GCM0037-SEP24         | mg/L  | 0.0002 | < 0.0002        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Naphthalene                | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 77                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Pentachlorophenol          | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 101                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Perylene                   | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 103                      | 50                     | 140  | NSS                      | 50                     | 140  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Semi-Volatile Organics (continued)

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter    | QC batch Reference | Units | RL     | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|--------------|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|              |                    |       |        |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|              |                    |       |        |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Phenanthrene | GCM0037-SEP24      | mg/L  | 0.0001 | < 0.0001     | NSS       | 30     | 90                 | 50                  | 140  | NSS                 | 50                  | 140  |
| Pyrene       | GCM0037-SEP24      | mg/L  | 0.0001 | < 0.0001     | NSS       | 30     | 97                 | 50                  | 140  | NSS                 | 50                  | 140  |

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

| Parameter              | QC batch Reference | Units | RL | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                        |                    |       |    |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                        |                    |       |    |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Total Suspended Solids | EWL0664-AUG24      | mg/L  | 2  | < 2          | 4         | 10     | 97                 | 90                  | 110  | NA                  |                     |      |

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

| Parameter               | QC batch Reference | Units     | RL  | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|-------------------------|--------------------|-----------|-----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                         |                    |           |     |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                         |                    |           |     |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Total Kjeldahl Nitrogen | SKA0017-SEP24      | as N mg/L | 0.5 | <0.5         | 3         | 10     | 97                 | 90                  | 110  | 106                 | 75                  | 125  |



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QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

| Parameter                                  | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|--------------------------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                            |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                            |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 1,1,2,2-Tetrachloroethane                  | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 101                      | 60                     | 130  | 103                      | 50                     | 140  |
| 1,2-Dichlorobenzene                        | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 100                      | 60                     | 130  | 111                      | 50                     | 140  |
| 1,4-Dichlorobenzene                        | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 110                      | 50                     | 140  |
| Benzene                                    | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 113                      | 50                     | 140  |
| Chloroform                                 | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 110                      | 50                     | 140  |
| cis-1,2-Dichloroethylene                   | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 109                      | 50                     | 140  |
| Ethylbenzene                               | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 112                      | 50                     | 140  |
| m-p-xylene                                 | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 114                      | 50                     | 140  |
| Methylene Chloride                         | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 111                      | 50                     | 140  |
| o-xylene                                   | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 97                       | 60                     | 130  | 111                      | 50                     | 140  |
| Tetrachloroethylene<br>(perchloroethylene) | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 114                      | 50                     | 140  |
| Toluene                                    | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 111                      | 50                     | 140  |
| trans-1,3-Dichloropropene                  | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 96                       | 60                     | 130  | 102                      | 50                     | 140  |
| Trichloroethylene                          | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 95                       | 60                     | 130  | 109                      | 50                     | 140  |



# FINAL REPORT

CA40200-AUG24 R1

## QC SUMMARY

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**Method Blank:** a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

**Duplicate:** Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

**LCS/Spike Blank:** Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

**Matrix Spike:** A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

**Reference Material:** a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

**RL:** Reporting limit

**RPD:** Relative percent difference

**AC:** Acceptance criteria

**Multielement Scan Qualifier:** as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

**Duplicate Qualifier:** for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

**Matrix Spike Qualifier:** for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

## LEGEND

## FOOTNOTES

**NSS** Insufficient sample for analysis.

**RL** Reporting Limit.

↑ Reporting limit raised.

↓ Reporting limit lowered.

**NA** The sample was not analysed for this analyte

**ND** Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

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This report supersedes all previous versions.

-- End of Analytical Report --

## Request for Laboratory Services and CHAIN OF CUSTODY

No. 036246

Page 1 of 1

## Laboratory Information Section - Lab use only

Received By: Amel  
Received Date: 08/29/24 (mm/dd/yy)  
Received Time: 12:00 (hr:min)Received By (signature): Amel  
Custody Seal Present: Yes ☒ No ☐  
Custody Seal Intact: Yes ☒ No ☐Cooling Agent Present: Yes ☒ No ☐ Type: ICE  
Temperature Upon Receipt (°C): 9.3LAB LIMS # CA40200-Ayga

## REPORT INFORMATION

## INVOICE INFORMATION

Company: PS Consultants Ltd  
Contact: Pradeep Patel  
Address: 6221 Hwy 7, Unit 6  
Phone: 905-264-9393  
Fax:   
Email: Pradeep@psconsultants.caCompany: Accounting  
Contact:   
Address:   
Phone:   
Fax:   
Email: 

## REGULATIONS

☐ O.Reg 153/04 ☐ O.Reg 406/19  
☐ Table 1 ☐ Res/Park ☐ Soil Texture: ☐ Reg 347/558 (3 Day min TAT)  
☐ Table 2 ☐ Ind/Com ☐ Coarse ☐ PW/OO ☐ MMER  
☐ Table 3 ☐ Agr/Other ☐ Medium/Fine ☐ CCME ☐ Other: Municipality: Halton  
☐ Table  Appx.  ☐ MISA  
Soil Volume ☐ <350m3 ☐ >350m3 ☐ ODWS Not Reportable \*See note

## RECORD OF SITE CONDITION (RSC)

☐ YES ☐ NOSewer By-Law: ☒ Sanitary ☒ Storm  
Halton  
Catville

## ANALYSIS REQUESTED

Quotation #: 24-228-100  
Project #: 24-228-100  
TURNAROUND TIME (TAT) REQUIRED before Dr. Catville  
☒ Regular TAT (5-7 days)  
RUSH TAT (Additional Charges May Apply): ☐ 1 Day ☐ 2 Days ☐ 3 Days ☐ 4 Days  
PLEASE CONFIRM RUSH FEASIBILITY WITH SGS REPRESENTATIVE PRIOR TO SUBMISSION  
Specify Due Date:   
\*NOTE: DRINKING (POTABLE) WATER SAMPLES FOR HUMAN CONSUMPTION MUST BE SUBMITTED WITH SGS DRINKING WATER CHAIN OF CUSTODY

| SAMPLE IDENTIFICATION | DATE SAMPLED  | TIME SAMPLED        | # OF BOTTLES | MATRIX    | Field Filtered (Y/N) |      |     |     |     |      |                        |      |      |                     |
|-----------------------|---------------|---------------------|--------------|-----------|----------------------|------|-----|-----|-----|------|------------------------|------|------|---------------------|
|                       |               |                     |              |           | M & I                | SVOC | PCB | PHC | VOC | Pest | Other (please specify) | SPLP | TCLP | COMMENTS:           |
| 1                     | <u>Bu24-6</u> | <u>Aug 29, 2024</u> | <u>18</u>    | <u>GU</u> | <u>N</u>             |      |     |     |     |      |                        |      |      | <u>Not filtered</u> |
| 2                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 3                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 4                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 5                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 6                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 7                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 8                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 9                     |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 10                    |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 11                    |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |
| 12                    |               |                     |              |           |                      |      |     |     |     |      |                        |      |      |                     |

## Observations/Comments/Special Instructions

## Sampled By (NAME):

Ken Kim

## Signature:

KenDate: Aug 29, 2024

(mm/dd/yy)

Pink Copy - Client

## Relinquished By (NAME):

Ken Kim

## Signature:

KenDate: Aug 29, 2024

(mm/dd/yy)

Yellow &amp; White Copy - SGS

Revision # 1.7  
Date of Issue: 07/June/2023Note: Submission of samples to SGS is considered an acknowledgment that you have been provided direction on sample collection, handling and transportation of samples. (2) Submission of samples to SGS is considered an authorization for completion of work. Signatures may appear on this form or be retained on file in the contract, or in an alternative format (e.g. shipping documents). (3) Results may be sent by email to an unlimited number of addresses for no additional cost. Fax is available upon request. This document is issued by the Company under its General Conditions of Service accessible at [http://www.sgs.com/terms\\_and\\_conditions.htm](http://www.sgs.com/terms_and_conditions.htm). (Printed copies are available upon request.) Attention is drawn to the limitation of liability, indemnification and jurisdiction issues defined therein.



## FINAL REPORT

CA40200-AUG24 R1

24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

Prepared for

**DS Consultants**

## First Page

### CLIENT DETAILS

Client DS Consultants

Address 6221 Highway 7 Unit 16  
Vaughan, Ontario  
L4H 0K8, Canada

Contact Pradeep Patel

Telephone 647-332-3482

Facsimile 905-264-2685

Email ppatel@dsconsultants.ca

Project 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

Order Number

Samples Ground Water (1)

### LABORATORY DETAILS

Project Specialist Maarit Wolfe, Hon.B.Sc

Laboratory SGS Canada Inc.

Address 185 Concession St., Lakefield ON, K0L 2H0

Telephone 705-652-2000

Facsimile 705-652-6365

Email Maarit.Wolfe@sgs.com

SGS Reference CA40200-AUG24

Received 08/29/2024

Approved 09/06/2024

Report Number CA40200-AUG24 R1

Date Reported 09/06/2024

### COMMENTS

RL - SGS Reporting Limit

Temperature of Sample upon Receipt: 9 degrees C

Cooling Agent Present: Yes

Custody Seal Present: Yes

Chain of Custody Number: 036246

### SIGNATORIES

Maarit Wolfe, Hon.B.Sc





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# FINAL REPORT

CA40200-AUG24 R1

**Client:** DS Consultants

**Project:** 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

**Project Manager:** Pradeep Patel

**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03

L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

## General Chemistry

|                                        |           |     |     |  |       |
|----------------------------------------|-----------|-----|-----|--|-------|
| Carbonaceous Biochemical Oxygen Demand | mg/L      | 2   |     |  | < 4 ↑ |
| Biochemical Oxygen Demand (BOD5)       | mg/L      | 2   | 300 |  | < 4 ↑ |
| Total Suspended Solids                 | mg/L      | 2   | 350 |  | 73    |
| Total Kjeldahl Nitrogen                | as N mg/L | 0.5 | 100 |  | 2.0   |

## Metals and Inorganics

|                    |      |          |      |  |          |
|--------------------|------|----------|------|--|----------|
| Cyanide (total)    | mg/L | 0.01     | 2    |  | < 0.01   |
| Fluoride           | mg/L | 0.06     | 10   |  | 0.51     |
| Sulphate           | mg/L | 2        | 1500 |  | 1300     |
| Aluminum (total)   | mg/L | 0.001    | 50   |  | 0.939    |
| Antimony (total)   | mg/L | 0.0009   | 5    |  | < 0.0009 |
| Arsenic (total)    | mg/L | 0.0002   | 1    |  | 0.0043   |
| Beryllium (total)  | mg/L | 0.000007 | 5    |  | 0.000050 |
| Cadmium (total)    | mg/L | 0.000003 | 1    |  | 0.000059 |
| Chromium (total)   | mg/L | 0.00008  | 3    |  | 0.00130  |
| Cobalt (total)     | mg/L | 0.000004 | 5    |  | 0.00507  |
| Copper (total)     | mg/L | 0.001    | 3    |  | 0.003    |
| Iron (total)       | mg/L | 0.007    | 50   |  | 1.18     |
| Lead (total)       | mg/L | 0.00009  | 3    |  | 0.00069  |
| Manganese (total)  | mg/L | 0.00001  | 5    |  | 0.208    |
| Molybdenum (total) | mg/L | 0.0004   | 5    |  | 0.0104   |



# FINAL REPORT

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**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03

L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

## Metals and Inorganics (continued)

|                    |      |         |    |  |           |
|--------------------|------|---------|----|--|-----------|
| Nickel (total)     | mg/L | 0.0001  | 3  |  | 0.0044    |
| Phosphorus (total) | mg/L | 0.003   | 10 |  | 0.039     |
| Selenium (total)   | mg/L | 0.00004 | 5  |  | 0.00127   |
| Silver (total)     | mg/L | 0.00005 | 5  |  | < 0.00005 |
| Tin (total)        | mg/L | 0.00006 | 5  |  | 0.00480   |
| Titanium (total)   | mg/L | 0.0001  | 5  |  | 0.0074    |
| Zinc (total)       | mg/L | 0.002   | 3  |  | 0.037     |

## Microbiology

|         |           |   |  |     |       |
|---------|-----------|---|--|-----|-------|
| E. Coli | cfu/100mL | 0 |  | 200 | < 2 † |
|---------|-----------|---|--|-----|-------|

## Nonylphenol and Ethoxylates

|                         |      |       |  |  |         |
|-------------------------|------|-------|--|--|---------|
| Nonylphenol             | mg/L | 0.001 |  |  | < 0.001 |
| Nonylphenol Ethoxylates | mg/L | 0.01  |  |  | < 0.01  |

## Oil and Grease

|                                  |      |   |     |  |     |
|----------------------------------|------|---|-----|--|-----|
| Oil & Grease (total)             | mg/L | 2 |     |  | < 2 |
| Oil & Grease (animal/vegetable)  | mg/L | 4 | 150 |  | < 4 |
| Oil & Grease (mineral/synthetic) | mg/L | 4 | 15  |  | < 4 |



# FINAL REPORT

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**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03

L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

## Organochlorine Pests (OCs)

|                   |      |         |  |  |           |
|-------------------|------|---------|--|--|-----------|
| Hexachlorobenzene | mg/L | 0.00001 |  |  | < 0.00001 |
|-------------------|------|---------|--|--|-----------|

## Other (ORP)

|                 |         |         |      |     |           |
|-----------------|---------|---------|------|-----|-----------|
| pH              | No unit | 0.05    | 10   | 8.5 | 7.54      |
| Chromium VI     | mg/L    | 0.0002  |      |     | < 0.0002  |
| Mercury (total) | mg/L    | 0.00001 | 0.05 |     | < 0.00001 |

## PAHs

|                        |      |        |  |  |          |
|------------------------|------|--------|--|--|----------|
| Benzo(b+j)fluoranthene | mg/L | 0.0001 |  |  | < 0.0001 |
|------------------------|------|--------|--|--|----------|

## PCBs

|                                          |      |        |  |  |          |
|------------------------------------------|------|--------|--|--|----------|
| Polychlorinated Biphenyls (PCBs) - Total | mg/L | 0.0001 |  |  | < 0.0001 |
|------------------------------------------|------|--------|--|--|----------|

## Pesticides

|                       |      |         |  |  |           |
|-----------------------|------|---------|--|--|-----------|
| Aldrin + Dieldrin     | mg/L | 0.00002 |  |  | < 0.00002 |
| Chlordane (total)     | mg/L | 0.00002 |  |  | < 0.001†  |
| DDT+Metabolites       | mg/L | 0.00004 |  |  | < 0.00004 |
| op-DDT                | mg/L | 0.00002 |  |  | < 0.00002 |
| pp-DDD                | mg/L | 0.00002 |  |  | < 0.00002 |
| pp-DDE                | mg/L | 0.00001 |  |  | < 0.00001 |
| pp-DDT                | mg/L | 0.00002 |  |  | < 0.00002 |
| o,p-DDD               | mg/L | 0.00002 |  |  | < 0.00002 |
| o,p-DDE               | mg/L | 0.00001 |  |  | < 0.00001 |
| Mirex                 | mg/L | 0.001   |  |  | < 0.001   |
| Hexachlorocyclohexane | mg/L | 0.001   |  |  | < 0.001   |



# FINAL REPORT

CA40200-AUG24 R1

**Client:** DS Consultants

**Project:** 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville

**Project Manager:** Pradeep Patel

**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03

L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

## Phenols

|                |      |       |   |  |       |
|----------------|------|-------|---|--|-------|
| 4AAP-Phenolics | mg/L | 0.002 | 1 |  | 0.003 |
|----------------|------|-------|---|--|-------|

## SVOCs

|                            |      |        |  |  |          |
|----------------------------|------|--------|--|--|----------|
| PAHs (Total)               | mg/L |        |  |  | < 0.001  |
| Perylene                   | mg/L | 0.0005 |  |  | < 0.0005 |
| di-n-Butyl Phthalate       | mg/L | 0.002  |  |  | < 0.002  |
| Bis(2-ethylhexyl)phthalate | mg/L | 0.002  |  |  | < 0.002  |
| 3,3-Dichlorobenzidine      | mg/L | 0.0005 |  |  | < 0.0005 |
| Pentachlorophenol          | mg/L | 0.0005 |  |  | < 0.0005 |

## SVOCs - PAHs

|                         |      |        |      |  |          |
|-------------------------|------|--------|------|--|----------|
| Naphthalene             | mg/L | 0.0005 | 0.14 |  | < 0.0005 |
| 7Hdibenzo(c,g)carbazole | mg/L | 0.0001 |      |  | < 0.0001 |
| Anthracene              | mg/L | 0.0001 |      |  | < 0.0001 |
| Benzo(a)anthracene      | mg/L | 0.0001 |      |  | < 0.0001 |
| Benzo(a)pyrene          | mg/L | 0.0001 |      |  | < 0.0001 |
| Benzo(e)pyrene          | mg/L | 0.0001 |      |  | < 0.0001 |
| Benzo(ghi)perylene      | mg/L | 0.0002 |      |  | < 0.0002 |
| Benzo(k)fluoranthene    | mg/L | 0.0001 |      |  | < 0.0001 |
| Chrysene                | mg/L | 0.0001 |      |  | < 0.0001 |
| Dibenzo(a,h)anthracene  | mg/L | 0.0001 |      |  | < 0.0001 |
| Dibenzo(a,i)pyrene      | mg/L | 0.0001 |      |  | < 0.0001 |
| Dibenzo(a,j)acridine    | mg/L | 0.0001 |      |  | < 0.0001 |



# FINAL REPORT

CA40200-AUG24 R1

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MATRIX: WATER

**Sample Number** 9

**Sample Name** BH24-6

**Sample Matrix** Ground Water

**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03

L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter | Units | RL | L1 | L2 | Result |
|-----------|-------|----|----|----|--------|
|-----------|-------|----|----|----|--------|

## SVOCs - PAHs (continued)

|                        |      |        |  |  |          |
|------------------------|------|--------|--|--|----------|
| Fluoranthene           | mg/L | 0.0001 |  |  | < 0.0001 |
| Indeno(1,2,3-cd)pyrene | mg/L | 0.0002 |  |  | < 0.0002 |
| Phenanthrene           | mg/L | 0.0001 |  |  | < 0.0001 |
| Pyrene                 | mg/L | 0.0001 |  |  | < 0.0001 |

## VOCs

|                                         |      |        |      |  |          |
|-----------------------------------------|------|--------|------|--|----------|
| Chloroform                              | mg/L | 0.0005 | 0.04 |  | 0.0052   |
| 1,2-Dichlorobenzene                     | mg/L | 0.0005 |      |  | < 0.0005 |
| 1,4-Dichlorobenzene                     | mg/L | 0.0005 | 0.08 |  | < 0.0005 |
| cis-1,2-Dichloroethylene                | mg/L | 0.0005 |      |  | < 0.0005 |
| trans-1,3-Dichloropropene               | mg/L | 0.0005 |      |  | < 0.0005 |
| Methylene Chloride                      | mg/L | 0.0005 | 2    |  | < 0.0005 |
| Tetrachloroethylene (perchloroethylene) | mg/L | 0.0005 | 1    |  | < 0.0005 |
| Trichloroethylene                       | mg/L | 0.0005 | 0.4  |  | < 0.0005 |
| 1,1,2,2-Tetrachloroethane               | mg/L | 0.0005 |      |  | < 0.0005 |



FINAL REPORT

CA40200-AUG24 R1

**Client:** DS Consultants  
**Project:** 24-228-100, Meadow Ridge & Wheat Boom Dr, Oakville  
**Project Manager:** Pradeep Patel  
**Samplers:** Ken Kim

MATRIX: WATER

**Sample Number** 9  
**Sample Name** BH24-6  
**Sample Matrix** Ground Water  
**Sample Date** 29/08/2022

L1 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Sanitary and Combined Sewer Discharge - BL\_2\_03  
L2 = SANSEW / WATER / - - Halton Sewer Use ByLaw - Storm Sewer Discharge - BL\_2\_03

| Parameter      | Units | RL     | L1    | L2 | Result   |
|----------------|-------|--------|-------|----|----------|
| VOCs - BTEX    |       |        |       |    |          |
| Benzene        | mg/L  | 0.0005 | 0.01  |    | < 0.0005 |
| Ethylbenzene   | mg/L  | 0.0005 | 0.16  |    | < 0.0005 |
| Toluene        | mg/L  | 0.0005 | 0.016 |    | < 0.0005 |
| m-p-xylene     | mg/L  | 0.0005 |       |    | < 0.0005 |
| o-xylene       | mg/L  | 0.0005 |       |    | < 0.0005 |
| Xylene (total) | mg/L  | 0.0005 |       |    | < 0.0005 |

## EXCEEDANCE SUMMARY

---

No exceedances are present above the regulatory limit(s) indicated



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Anions by discrete analyzer  
Method: US EPA 375.4 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-026

| Parameter | QC batch Reference | Units | RL | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|-----------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|           |                    |       |    |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|           |                    |       |    |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Sulphate  | DIO5001-SEP24      | mg/L  | 2  | <2           | ND        | 20     | 107                | 80                  | 120  | 107                 | 75                  | 125  |

Biochemical Oxygen Demand  
Method: SM 5210 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-007

| Parameter                              | QC batch Reference | Units           | RL | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|----------------------------------------|--------------------|-----------------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                                        |                    |                 |    |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                                        |                    |                 |    |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Carbonaceous Biochemical Oxygen Demand | BOD0061-AUG24      | (CBOD5)<br>mg/L | 2  | < 2          | 4         | 30     | 97                 | 70                  | 130  | 96                  | 70                  | 130  |
| Biochemical Oxygen Demand (BOD5)       | BOD0062-AUG24      | mg/L            | 2  | < 2          | 3         | 30     | 99                 | 70                  | 130  | 123                 | 70                  | 130  |



FINAL REPORT

CA40200-AUG24 R1

QC SUMMARY

Cyanide by SFA  
Method: SM 4500 | Internal ref.: ME-CA-IENVISFA-LAK-AN-005

| Parameter       | QC batch<br>Reference | Units | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------------|-----------------------|-------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                 |                       |       |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                 |                       |       |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Cyanide (total) | SKA0004-SEP24         | mg/L  | 0.01 | <0.01           | ND        | 10        | 94                       | 90                     | 110  | NV                       | 75                     | 125  |

Fluoride by Specific Ion Electrode  
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-014

| Parameter | QC batch<br>Reference | Units | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|-------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |       |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |       |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Fluoride  | EWL0683-AUG24         | mg/L  | 0.06 | <0.06           | 7         | 10        | 101                      | 90                     | 110  | 105                      | 75                     | 125  |

Hexavalent Chromium by SFA  
Method: EPA218.6/EPA3060A | Internal ref.: ME-CA-IENVISKA-LAK-AN-012

| Parameter   | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|             |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|             |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Chromium VI | SKA0005-SEP24         | mg/L  | 0.0002 | <0.0002         | ND        | 20        | 99                       | 80                     | 120  | NV                       | 75                     | 125  |



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QC SUMMARY

Mercury by CVAAS  
Method: EPA 7471A/SM 3112B | Internal ref.: ME-CA-IENVISPE-LAK-AN-004

| Parameter       | QC batch<br>Reference | Units | RL      | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------------|-----------------------|-------|---------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                 |                       |       |         |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                 |                       |       |         |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Mercury (total) | EHG0067-AUG24         | mg/L  | 0.00001 | < 0.00001       | ND        | 20        | 102                      | 80                     | 120  | 70                       | 70                     | 130  |



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QC SUMMARY

Metals in aqueous samples - ICP-MS  
Method: SM 3030/EPA 200.8 | Internal ref.: ME-CA-ENVISPE-LAK-AN-006

| Parameter          | QC batch<br>Reference | Units | RL       | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|--------------------|-----------------------|-------|----------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                    |                       |       |          |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                    |                       |       |          |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Silver (total)     | EMS0342-AUG24         | mg/L  | 0.00005  | <0.00005        | ND        | 20        | 100                      | 90                     | 110  | 93                       | 70                     | 130  |
| Aluminum (total)   | EMS0342-AUG24         | mg/L  | 0.001    | <0.001          | ND        | 20        | 104                      | 90                     | 110  | 99                       | 70                     | 130  |
| Arsenic (total)    | EMS0342-AUG24         | mg/L  | 0.0002   | <0.0002         | ND        | 20        | 99                       | 90                     | 110  | 103                      | 70                     | 130  |
| Beryllium (total)  | EMS0342-AUG24         | mg/L  | 0.000007 | <0.000007       | ND        | 20        | 103                      | 90                     | 110  | 97                       | 70                     | 130  |
| Cadmium (total)    | EMS0342-AUG24         | mg/L  | 0.000003 | <0.000003       | 3         | 20        | 97                       | 90                     | 110  | 101                      | 70                     | 130  |
| Cobalt (total)     | EMS0342-AUG24         | mg/L  | 0.000004 | <0.000004       | 2         | 20        | 101                      | 90                     | 110  | 104                      | 70                     | 130  |
| Chromium (total)   | EMS0342-AUG24         | mg/L  | 0.00008  | <0.00008        | 0         | 20        | 100                      | 90                     | 110  | 104                      | 70                     | 130  |
| Copper (total)     | EMS0342-AUG24         | mg/L  | 0.001    | <0.001          | ND        | 20        | 99                       | 90                     | 110  | 103                      | 70                     | 130  |
| Iron (total)       | EMS0342-AUG24         | mg/L  | 0.007    | <0.007          | 0         | 20        | 103                      | 90                     | 110  | 100                      | 70                     | 130  |
| Manganese (total)  | EMS0342-AUG24         | mg/L  | 0.00001  | <0.00001        | 1         | 20        | 101                      | 90                     | 110  | 99                       | 70                     | 130  |
| Molybdenum (total) | EMS0342-AUG24         | mg/L  | 0.0004   | <0.0004         | ND        | 20        | 101                      | 90                     | 110  | 108                      | 70                     | 130  |
| Nickel (total)     | EMS0342-AUG24         | mg/L  | 0.0001   | <0.0001         | 7         | 20        | 101                      | 90                     | 110  | 106                      | 70                     | 130  |
| Lead (total)       | EMS0342-AUG24         | mg/L  | 0.00009  | <0.00009        | 5         | 20        | 97                       | 90                     | 110  | 102                      | 70                     | 130  |
| Phosphorus (total) | EMS0342-AUG24         | mg/L  | 0.003    | <0.003          | 7         | 20        | 98                       | 90                     | 110  | NV                       | 70                     | 130  |
| Antimony (total)   | EMS0342-AUG24         | mg/L  | 0.0009   | <0.0009         | ND        | 20        | 102                      | 90                     | 110  | 109                      | 70                     | 130  |
| Selenium (total)   | EMS0342-AUG24         | mg/L  | 0.00004  | <0.00004        | 18        | 20        | 99                       | 90                     | 110  | 92                       | 70                     | 130  |
| Tin (total)        | EMS0342-AUG24         | mg/L  | 0.00006  | <0.00006        | ND        | 20        | 103                      | 90                     | 110  | NV                       | 70                     | 130  |
| Titanium (total)   | EMS0342-AUG24         | mg/L  | 0.0001   | <0.0001         | 9         | 20        | 103                      | 90                     | 110  | NV                       | 70                     | 130  |
| Zinc (total)       | EMS0342-AUG24         | mg/L  | 0.002    | <0.002          | 0         | 20        | 103                      | 90                     | 110  | 71                       | 70                     | 130  |



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CA40200-AUG24 R1

QC SUMMARY

Microbiology  
Method: SM 9222D | Internal ref.: ME-CA-IENVIMIC-LAK-AN-006

| Parameter | QC batch<br>Reference | Units     | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|-----------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |           |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |           |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| E. Coli   | BAC9502-AUG24         | cfu/100mL | -  | ACCEPTED        | ACCEPTED  |           |                          |                        |      |                          |                        |      |
|           |                       |           |    |                 | D         |           |                          |                        |      |                          |                        |      |

Nonylphenol and Ethoxylates  
Method: ASTM D7065-06 | Internal ref.: ME-CA-IENVIGC-LAK-AN-015

| Parameter   | QC batch<br>Reference | Units | RL    | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-------------|-----------------------|-------|-------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|             |                       |       |       |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|             |                       |       |       |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Nonylphenol | GCM0008-SEP24         | mg/L  | 0.001 | <0.001          |           |           | 94                       | 55                     | 120  |                          |                        |      |

Oil & Grease  
Method: MOE E3401 | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter            | QC batch<br>Reference | Units | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------|-----------------------|-------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                      |                       |       |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                      |                       |       |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Oil & Grease (total) | GCM0039-SEP24         | mg/L  | 2  | <2              | NSS       | 20        | 106                      | 75                     | 125  |                          |                        |      |



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QC SUMMARY

Oil & Grease-AV/MS

Method: MOE E3401/SM 5520F | Internal ref.: ME-CA-IENVIGC-LAK-AN-019

| Parameter                        | QC batch<br>Reference | Units | RL | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------------------|-----------------------|-------|----|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                  |                       |       |    |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                  |                       |       |    |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Oil & Grease (animal/vegetable)  | GCM0039-SEP24         | mg/L  | 4  | < 4             | NSS       | 20        | NA                       | 70                     | 130  |                          |                        |      |
| Oil & Grease (mineral/synthetic) | GCM0039-SEP24         | mg/L  | 4  | < 4             | NSS       | 20        | NA                       | 70                     | 130  |                          |                        |      |

Pesticides

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-018

| Parameter             | QC batch<br>Reference | Units | RL      | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------------------|-----------------------|-------|---------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                       |                       |       |         |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                       |                       |       |         |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Hexachlorobenzene     | GCM0063-SEP24         | mg/L  | 0.00001 | < 0.00001       | NSS       | 30        | 91                       | 50                     | 140  | 88                       | 50                     | 140  |
| Hexachlorocyclohexane | GCM0063-SEP24         | mg/L  | 0.001   | < 0.001         | NSS       | 30        | 95                       | 50                     | 140  | 93                       | 50                     | 140  |
| Mirex                 | GCM0063-SEP24         | mg/L  | 0.001   | < 0.001         | NSS       | 30        | 95                       | 50                     | 140  | 83                       | 50                     | 140  |
| o,p-DDD               | GCM0063-SEP24         | mg/L  | 0.00002 | < 0.00002       | NSS       | 30        | 97                       | 50                     | 140  | 93                       | 50                     | 140  |
| o,p-DDE               | GCM0063-SEP24         | mg/L  | 0.00001 | < 0.00001       | NSS       | 30        | 97                       | 50                     | 140  | 97                       | 50                     | 140  |
| op-DDT                | GCM0063-SEP24         | mg/L  | 0.00002 | < 0.00002       | NSS       | 30        | 98                       | 50                     | 140  | 96                       | 50                     | 140  |
| pp-DDD                | GCM0063-SEP24         | mg/L  | 0.00002 | < 0.00002       | NSS       | 30        | 99                       | 50                     | 140  | 102                      | 50                     | 140  |
| pp-DDE                | GCM0063-SEP24         | mg/L  | 0.00001 | < 0.00001       | NSS       | 30        | 97                       | 50                     | 140  | 92                       | 50                     | 140  |
| pp-DDT                | GCM0063-SEP24         | mg/L  | 0.00002 | < 0.00002       | NSS       | 30        | 102                      | 50                     | 140  | 105                      | 50                     | 140  |



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CA40200-AUG24 R1

QC SUMMARY

pH  
Method: SM 4500 | Internal ref.: ME-CA-IENVIEWL-LAK-AN-006

| Parameter | QC batch<br>Reference | Units   | RL   | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|-----------|-----------------------|---------|------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|           |                       |         |      |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|           |                       |         |      |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| pH        | EWL0675-AUG24         | No unit | 0.05 | NA              | 0         |           | 100                      |                        |      | NA                       |                        |      |

Phenols by SFA  
Method: SM 5530B-D | Internal ref.: ME-CA-IENVISFA-LAK-AN-006

| Parameter      | QC batch<br>Reference | Units | RL    | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------|-----------------------|-------|-------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                |                       |       |       |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                |                       |       |       |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 4AAP-Phenolics | SKA0002-SEP24         | mg/L  | 0.002 | <0.002          | 7         | 10        | 100                      | 80                     | 120  | 106                      | 75                     | 125  |

Polychlorinated Biphenyls  
Method: MOE E3400/EPA 8082A | Internal ref.: ME-CA-IENVIGC-LAK-AN-001

| Parameter                                   | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|---------------------------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                             |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                             |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| Polychlorinated Biphenyls (PCBs) -<br>Total | GCM0009-SEP24         | mg/L  | 0.0001 | <0.0001         | NSS       | 30        | 91                       | 60                     | 140  | NSS                      | 60                     | 140  |



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CA40200-AUG24 R1

QC SUMMARY

Semi-Volatile Organics

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter                  | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|----------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                            |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                            |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 3,3-Dichlorobenzidine      | GCM0035-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 107                      | 30                     | 130  | NSS                      | 30                     | 130  |
| 7Hdibenzo(c,g)carbazole    | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 89                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Anthracene                 | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 88                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(a)anthracene         | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 93                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(a)pyrene             | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 93                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(b+j)fluoranthene     | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(e)pyrene             | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 89                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(ghi)perylene         | GCM0037-SEP24         | mg/L  | 0.0002 | < 0.0002        | NSS       | 30        | 96                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Benzo(k)fluoranthene       | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 100                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Bis(2-ethylhexyl)phthalate | GCM0037-SEP24         | mg/L  | 0.002  | < 0.002         | NSS       | 30        | 102                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Chrysene                   | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 95                       | 50                     | 140  | NSS                      | 50                     | 140  |
| di-n-Butyl Phthalate       | GCM0037-SEP24         | mg/L  | 0.002  | < 0.002         | NSS       | 30        | 102                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,h)anthracene     | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,i)pyrene         | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 83                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Dibenzo(a,j)acridine       | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 88                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Fluoranthene               | GCM0037-SEP24         | mg/L  | 0.0001 | < 0.0001        | NSS       | 30        | 95                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Indeno(1,2,3-cd)pyrene     | GCM0037-SEP24         | mg/L  | 0.0002 | < 0.0002        | NSS       | 30        | 97                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Naphthalene                | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 77                       | 50                     | 140  | NSS                      | 50                     | 140  |
| Pentachlorophenol          | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 101                      | 50                     | 140  | NSS                      | 50                     | 140  |
| Perylene                   | GCM0037-SEP24         | mg/L  | 0.0005 | < 0.0005        | NSS       | 30        | 103                      | 50                     | 140  | NSS                      | 50                     | 140  |



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CA40200-AUG24 R1

QC SUMMARY

Semi-Volatile Organics (continued)

Method: EPA 3510C/8270D | Internal ref.: ME-CA-IENVIGC-LAK-AN-005

| Parameter    | QC batch Reference | Units | RL     | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|--------------|--------------------|-------|--------|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|              |                    |       |        |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|              |                    |       |        |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Phenanthrene | GCM0037-SEP24      | mg/L  | 0.0001 | < 0.0001     | NSS       | 30     | 90                 | 50                  | 140  | NSS                 | 50                  | 140  |
| Pyrene       | GCM0037-SEP24      | mg/L  | 0.0001 | < 0.0001     | NSS       | 30     | 97                 | 50                  | 140  | NSS                 | 50                  | 140  |

Suspended Solids

Method: SM 2540D | Internal ref.: ME-CA-IENVIEWL-LAK-AN-004

| Parameter              | QC batch Reference | Units | RL | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|------------------------|--------------------|-------|----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                        |                    |       |    |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                        |                    |       |    |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Total Suspended Solids | EWL0664-AUG24      | mg/L  | 2  | < 2          | 4         | 10     | 97                 | 90                  | 110  | NA                  |                     |      |

Total Nitrogen

Method: SM 4500-N C/4500-NO3- F | Internal ref.: ME-CA-IENVISFA-LAK-AN-002

| Parameter               | QC batch Reference | Units     | RL  | Method Blank | Duplicate |        | LCS/Spike Blank    |                     |      | Matrix Spike / Ref. |                     |      |
|-------------------------|--------------------|-----------|-----|--------------|-----------|--------|--------------------|---------------------|------|---------------------|---------------------|------|
|                         |                    |           |     |              | RPD       | AC (%) | Spike Recovery (%) | Recovery Limits (%) |      | Spike Recovery (%)  | Recovery Limits (%) |      |
|                         |                    |           |     |              |           |        |                    | Low                 | High |                     | Low                 | High |
| Total Kjeldahl Nitrogen | SKA0017-SEP24      | as N mg/L | 0.5 | <0.5         | 3         | 10     | 97                 | 90                  | 110  | 106                 | 75                  | 125  |



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QC SUMMARY

Volatile Organics

Method: EPA 5030B/8260C | Internal ref.: ME-CA-ENVIGC-LAK-AN-004

| Parameter                                  | QC batch<br>Reference | Units | RL     | Method<br>Blank | Duplicate |           | LCS/Spike Blank          |                        |      | Matrix Spike / Ref.      |                        |      |
|--------------------------------------------|-----------------------|-------|--------|-----------------|-----------|-----------|--------------------------|------------------------|------|--------------------------|------------------------|------|
|                                            |                       |       |        |                 | RPD       | AC<br>(%) | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      | Spike<br>Recovery<br>(%) | Recovery Limits<br>(%) |      |
|                                            |                       |       |        |                 |           |           |                          | Low                    | High |                          | Low                    | High |
| 1,1,2,2-Tetrachloroethane                  | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 101                      | 60                     | 130  | 103                      | 50                     | 140  |
| 1,2-Dichlorobenzene                        | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 100                      | 60                     | 130  | 111                      | 50                     | 140  |
| 1,4-Dichlorobenzene                        | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 110                      | 50                     | 140  |
| Benzene                                    | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 113                      | 50                     | 140  |
| Chloroform                                 | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 110                      | 50                     | 140  |
| cis-1,2-Dichloroethylene                   | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 109                      | 50                     | 140  |
| Ethylbenzene                               | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 112                      | 50                     | 140  |
| m-p-xylene                                 | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 114                      | 50                     | 140  |
| Methylene Chloride                         | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 111                      | 50                     | 140  |
| o-xylene                                   | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 97                       | 60                     | 130  | 111                      | 50                     | 140  |
| Tetrachloroethylene<br>(perchloroethylene) | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 98                       | 60                     | 130  | 114                      | 50                     | 140  |
| Toluene                                    | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 99                       | 60                     | 130  | 111                      | 50                     | 140  |
| trans-1,3-Dichloropropene                  | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 96                       | 60                     | 130  | 102                      | 50                     | 140  |
| Trichloroethylene                          | GCM0023-SEP24         | mg/L  | 0.0005 | <0.0005         | ND        | 30        | 95                       | 60                     | 130  | 109                      | 50                     | 140  |



# FINAL REPORT

CA40200-AUG24 R1

## QC SUMMARY

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**Method Blank:** a blank matrix that is carried through the entire analytical procedure. Used to assess laboratory contamination.

**Duplicate:** Paired analysis of a separate portion of the same sample that is carried through the entire analytical procedure. Used to evaluate measurement precision.

**LCS/Spike Blank:** Laboratory control sample or spike blank refer to a blank matrix to which a known amount of analyte has been added. Used to evaluate analyte recovery and laboratory accuracy without sample matrix effects.

**Matrix Spike:** A sample to which a known amount of the analyte of interest has been added. Used to evaluate laboratory accuracy with sample matrix effects.

**Reference Material:** a material or substance matrix matched to the samples that contains a known amount of the analyte of interest. A reference material may be used in place of a matrix spike.

**RL:** Reporting limit

**RPD:** Relative percent difference

**AC:** Acceptance criteria

**Multielement Scan Qualifier:** as the number of analytes in a scan increases, so does the chance of a limit exceedance by random chance as opposed to a real method problem. Thus, in multielement scans, for the LCS and matrix spike, up to 10% of the analytes may exceed the quoted limits by up to 10% absolute and the spike is considered acceptable.

**Duplicate Qualifier:** for duplicates as the measured result approaches the RL, the uncertainty associated with the value increases dramatically, thus duplicate acceptance limits apply only where the average of the two duplicates is greater than five times the RL.

**Matrix Spike Qualifier:** for matrix spikes, as the concentration of the native analyte increases, the uncertainty of the matrix spike recovery increases. Thus, the matrix spike acceptance limits apply only when the concentration of the matrix spike is greater than or equal to the concentration of the native analyte.

## LEGEND

## FOOTNOTES

**NSS** Insufficient sample for analysis.

**RL** Reporting Limit.

↑ Reporting limit raised.

↓ Reporting limit lowered.

**NA** The sample was not analysed for this analyte

**ND** Non Detect

Results relate only to the sample tested.

Data reported represent the sample as submitted to SGS. Solid samples expressed on a dry weight basis.

"Temperature Upon Receipt" is representative of the whole shipment and may not reflect the temperature of individual samples.

Analysis conducted on samples submitted pursuant to or as part of Reg. 153/04, are in accordance to the "Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act and Excess Soil Quality" published by the Ministry and dated March 9, 2004 as amended.

SGS provides criteria information (such as regulatory or guideline limits and summary of limit exceedances) as a service. Every attempt is made to ensure the criteria information in this report is accurate and current, however, it is not guaranteed. Comparison to the most current criteria is the responsibility of the client and SGS assumes no responsibility for the accuracy of the criteria levels indicated.

SGS Canada Inc. statement of conformity decision rule does not consider uncertainty when analytical results are compared to a specified standard or regulation.

This document is issued, on the Client's behalf, by the Company under its General Conditions of Service available on request and accessible at [http://www.sgs.com/terms\\_and\\_conditions.htm](http://www.sgs.com/terms_and_conditions.htm).

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This report supersedes all previous versions.

-- End of Analytical Report --

## Request for Laboratory Services and CHAIN OF CUSTODY

No. 036246

Page 1 of 1

## Laboratory Information Section - Lab use only

Received By: Amel  
Received Date: 08/29/24 (mm/dd/yy)  
Received Time: 12:00 (hr:min)Received By (signature): Amel  
Custody Seal Present: Yes ☒ No ☐  
Custody Seal Intact: Yes ☒ No ☐Cooling Agent Present: Yes ☒ No ☐ Type: ICE  
Temperature Upon Receipt (°C): 9.3LAB LIMS # CA40200-Ayga

## REPORT INFORMATION

## INVOICE INFORMATION

Company: PS Consultants Ltd

(same as Report Information)

Contact: Pradeep PatelCompany: AccountingAddress: 6221 Hwy 7, Unit 6Address: Phone: 905-264-9393Address: Fax: Phone: Email: Pradeep@psconsultants.caEmail: ca

REGULATIONS

☐ O.Reg 153/04☐ O.Reg 406/19

Other Regulations:

Sewer By-Law:

☐ Table 1☐ Res/Park☐ Soil Texture:☐ Reg 347/558 (3 Day min TAT)☒ Sanitary☐ Table 2☐ Ind/Com☐ Coarse☐ PW/QO☐ MMER☒ Storm☐ Table 3☐ Agr/Other☐ Medium/Fine☐ CCME☐ Other:☒ Municipally:☐ Table☐ Appx.☐ MISA☐ ODWS Not Reportable \*See note☐ MISA☒ HaltonSoil Volume ☐ <350m3 ☐ >350m3

Corkville

Corkville

Corkville

Field Filtered (Y/N)

Metals &amp; Inorganics

Full Metals Suite

ICP Metals only

PAHs only

SVOCs

PCBs

F1-F4 + BTEX

F1-F4 only

VOCs

BTEX only

Pesticides

Organochlorine or specify other

Sewer Use:

Specify pkg:

Water Characterization Pkg

General ☐ Extended ☐

SPLP

TCLP

Specify

Specify

Specify

Specify

Specify

COMMENTS:

1 Bu24-6Aug 29, 2024Aug 18Gu NField Filtered (Y/N)Metals & InorganicsFull Metals SuiteICP Metals onlyPAHs onlySVOCsPCBsF1-F4 + BTEXF1-F4 onlyVOCsBTEX onlyPesticidesOrganochlorine or specify otherSewer Use:Specify pkg:Water Characterization PkgGeneral ☐ Extended ☐SPLPTCLPSpecifySpecifySpecifySpecifySpecifySpecify

Non-filtered

Observations/Comments/Special Instructions

Sampled By (NAME): Ken KimSignature: Ken KimDate: Aug 29, 2024

(mm/dd/yy)

Pink Copy - Client

Yellow &amp; White Copy - SGS

Relinquished by (NAME): Ken KimSignature: Ken KimDate: Aug 29, 2024

(mm/dd/yy)

Note: Submission of samples to SGS is considered authorization for completion of work. Signatures may appear on this form or be retained on file in the contract, or in an alternative format (e.g. shipping documents). (3) Results may be sent by email to an unlimited number of addresses for no additional cost. Fax is available upon request. This document is issued by the Company under its General Conditions of Service accessible at [http://www.sgs.com/terms\\_and\\_conditions.htm](http://www.sgs.com/terms_and_conditions.htm). (Printed copies are available upon request.) Attention is drawn to the limitation of liability, indemnification and jurisdiction issues defined therein.

## **Appendix D: MECP Water Wells Records**

**Table: MECP Water Wells Records**  
**Location: Block 297, Oakville, ON**

| TOWNSHIP C                   | E      | N       | DATE CNTR       | CASING | WATER | PUMP TEST | WELL USE | SCREEN  | WELL    | FORMATION                                                             |
|------------------------------|--------|---------|-----------------|--------|-------|-----------|----------|---------|---------|-----------------------------------------------------------------------|
| OAKVILLE TOWN                | 604489 | 4817801 | 2018-06<br>7472 | 2      |       |           | MO       | 0015 10 | 7323102 | RED TILL CLAY SILT 0025                                               |
| OAKVILLE TOWN                | 604820 | 4817632 | 2018-11<br>7523 | 39.3   |       |           |          |         | 7322988 |                                                                       |
| OAKVILLE TOWN                | 604489 | 4817800 | 2018-06<br>7472 | 2      |       |           | MO       | 0046 5  | 7323101 | RED TILL CLAY SILT 0030 RED SAND SILT GRVL 0037<br>RED SHLE HARD 0051 |
| OAKVILLE TOWN                | 604772 | 4817956 | 2018-06<br>7472 | 2      |       |           | MO       | 0025 10 | 7323105 | RED TILL CLAY SILT 0030 RED SAND SILT GRVL 0035                       |
| OAKVILLE TOWN                | 604495 | 4818096 | 2018-06<br>7472 | 2      |       |           | MO       | 0045 5  | 7323104 | RED TILL CLAY SILT 0030 RED SAND SILT GRVL 0045<br>RED SHLE HARD 0050 |
| OAKVILLE TOWN                | 604774 | 4817549 | 2018-06<br>7472 | 2      |       |           | MO       | 0040 10 | 7323103 | RED TILL CLAY SILT 0025 RED SHLE HARD 0050                            |
| OAKVILLE TOWN                | 604495 | 4818097 | 2018-06<br>7472 | 2      |       |           | MO       | 0035 10 | 7323100 | RED TILL CLAY SILT 0030 RED SAND SILT GRVL 0044<br>RED SHLE HARD 0045 |
| OAKVILLE TOWN                | 604408 | 4817184 | 2005-08<br>6809 | 2      |       |           |          | 0020 5  | 2810339 | BLCK LOAM 0001 BRWN TILL 0010 RED SHLE 0025                           |
| OAKVILLE TOWN                | 604787 | 4817463 | 2005-08<br>6809 | 2      |       |           |          | 0013 5  | 2810341 | BLCK LOAM 0001 BRWN TILL 0007 RED SHLE 0018                           |
| OAKVILLE TOWN                | 604881 | 4817747 | 2017-06<br>6875 | 2.04   |       |           | MO       | 0025 10 | 7292005 |                                                                       |
| OAKVILLE TOWN                | 604834 | 4817854 | 2015-01<br>6607 |        |       |           |          |         | 7267217 |                                                                       |
| OAKVILLE TOWN                | 604914 | 4817681 | 2019-10<br>7523 | 36     |       | ///:      |          |         | 7345756 |                                                                       |
| OAKVILLE TOWN                | 604678 | 4817410 | 2020-11<br>7644 |        |       |           |          |         | 7374758 |                                                                       |
| OAKVILLE TOWN                | 604772 | 4817955 | 2018-06<br>7472 | 2      |       |           | MO       | 0046 5  | 7323106 | RED TILL CLAY SILT 0030 RED SAND SILT GRVL 0040<br>RED SHLE HARD 0051 |
| OAKVILLE TOWN                | 604674 | 4817337 | 2020-11<br>7644 |        |       |           |          |         | 7374759 |                                                                       |
| OAKVILLE TOWN                | 604544 | 4817309 | 6946            |        |       |           |          |         | 7355086 |                                                                       |
| OAKVILLE TOWN                | 604670 | 4817428 | 2020-11<br>7644 |        |       |           |          |         | 7374961 |                                                                       |
| OAKVILLE TOWN DS<br>N 01 007 | 604913 | 4817753 | 2020-07<br>7523 | 2      |       | ///:      |          |         | 7380724 |                                                                       |
| OAKVILLE TOWN DS<br>N 01 007 | 604913 | 4817753 | 2020-07<br>7523 | 2      |       | ///:      |          |         | 7380723 |                                                                       |
| OAKVILLE TOWN DS<br>N 01 007 | 604834 | 4817605 | 2022-06<br>7472 | 2      |       | ///:      | MO       | 0025 10 | 7421466 | BRWN FILL LOOS 0005 GREY CLAY TILL PCKD 0035                          |

|                              |        |         |                 |      |  |        |    |  |         |    |
|------------------------------|--------|---------|-----------------|------|--|--------|----|--|---------|----|
| OAKVILLE TOWN DS<br>N 01 007 | 604818 | 4817914 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7384173 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604586 | 4817992 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380727 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604732 | 4817700 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380726 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604586 | 4817992 | 2020-07<br>7523 | 5.07 |  | ///:   |    |  | 7380706 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604818 | 4817914 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380274 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604460 | 4818087 | 2020-08<br>7523 | 2    |  | ///:   | MO |  | 7367242 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604847 | 4817602 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380725 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604836 | 4817819 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380722 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604460 | 4818087 | 2020-08<br>7523 | 2    |  | ///:   | MO |  | 7367240 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604557 | 4817770 | 2020-08<br>7523 | 2    |  | ///:   |    |  | 7367239 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604813 | 4817753 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380704 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604557 | 4817770 | 2020-08<br>7523 | 2    |  | 11///: |    |  | 7367238 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604578 | 4817988 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380707 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604480 | 4818053 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380708 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604818 | 4817914 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380709 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604818 | 4817914 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380710 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604847 | 4817602 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380711 |    |
| OAKVILLE TOWN DS<br>N 01 007 | 604707 | 4817594 | 2019-03<br>7523 | 36   |  | ///:   |    |  | 7331209 | 20 |
| OAKVILLE TOWN DS<br>N 01 007 | 604732 | 4817700 | 2020-07<br>7523 | 2    |  | ///:   |    |  | 7380705 |    |
| OAKVILLE TOWN DS<br>N 01 008 | 604228 | 4817454 | 2021-11<br>7523 | 2    |  | ///:   | MO |  | 7407748 |    |
| OAKVILLE TOWN DS<br>N 01 008 | 604674 | 4817409 | 2021-10<br>7523 | 2    |  | ///:   | MO |  | 7407765 |    |
| OAKVILLE TOWN DS<br>N 01 008 | 604675 | 4817408 | 2021-10<br>7523 | 6.25 |  | 13///: | DO |  | 7407764 |    |
| OAKVILLE TOWN DS<br>N 01 008 | 604517 | 4817484 | 2021-11<br>7523 | 2    |  | ///:   | MO |  | 7407749 |    |

|                              |        |         |                 |       |                    |       |       |  |         |                                                               |
|------------------------------|--------|---------|-----------------|-------|--------------------|-------|-------|--|---------|---------------------------------------------------------------|
| OAKVILLE TOWN DS<br>N 01 008 | 604675 | 4817386 | 2021-11<br>7523 | 2     |                    | ///:  | MO    |  | 7407747 |                                                               |
| OAKVILLE TOWN DS<br>N 01 008 | 604672 | 4817428 | 2021-11<br>7523 | 2     |                    | ///:  | MO    |  | 7407746 |                                                               |
| OAKVILLE TOWN DS<br>N 01 008 | 604715 | 4817383 | 1978-04<br>3637 | 30 24 | FR 0010<br>FR 0019 | 5///: | ST DO |  | 2805268 | BRWN LOAM 0001 BRWN CLAY PCKD 0009 RED SHLE<br>VERY HARD 0020 |
| OAKVILLE TOWN DS<br>N 01 008 | 604066 | 4817885 | 2021-11<br>7523 | 2     |                    | ///:  | MO    |  | 7407750 |                                                               |
| OAKVILLE TOWN DS<br>N 01 009 | 604390 | 4817207 | 2021-05<br>7523 | 2     |                    | ///:  | MO    |  | 7387449 |                                                               |