

# 1258 Rebecca Street, Oakville

# **Functional Servicing Report**

January 2023

## **Submitted by:**

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**Project Number: 2480** 

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## **SUBMISSION HISTORY**

Submission	Date	In Support Of	Distributed To
1 <sup>st</sup>	April 2022	Zoning By-law Amendment	Town of Oakville,
		Application	Conservation Halton
Draft 2 <sup>nd</sup>	November	Zoning By-law Amendment	Town of Oakville,
	2022	Application	Conservation Halton
2 <sup>nd</sup>	January 2023	Zoning By-law Amendment	Town of Oakville,
		Application	Conservation Halton



#### 1.0 INTRODUCTION

SCS Consulting Group Ltd. has been retained by Halton Region to prepare a Functional Servicing Report for a proposed assisted living development located at Rebecca Street and Warminster Drive in the Town of Oakville.

#### 1.1 Purpose of the Report

The Functional Servicing and Stormwater Management (SWM) Report has been prepared in support of a Zoning By-law Amendment (ZBA) application for the proposed development. The Site Plan is provided in **Appendix A**.

The purpose of this report is to demonstrate that the proposed development can be graded and serviced in accordance with the Town of Oakville, Halton Region, Conservation Halton, Ontario Building Code (OBC), and the Ministry of Environment, Conservation and Parks (MECP) design criteria.

#### 1.2 Study Area

The existing site is comprised of vacant open space located within the Fourteen Mile Creek watershed in the Town of Oakville. As shown on **Figure 1.1**, the study area is bound by:

- Rebecca Street to the north;
- Patricia-Picknell Elementary School to the south;
- Single-family residential area to the east; and
- Oakville Public Library and Paramedic Services Station to the west.

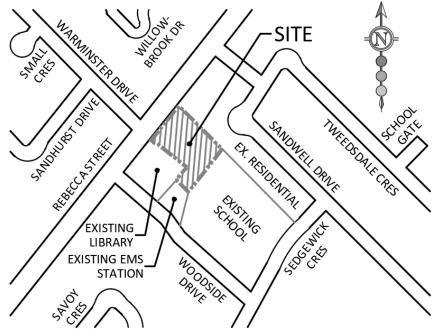


Figure 1.1: Site Location Plan

The proposed development is approximately 0.66 ha in size and consists of three single detached lots fronting onto Rebecca Street and fourteen single storey semi-detached units. The semi-detached units will serve as an affordable independent living community for seniors.

Each of the proposed single detached lots will have independent access onto Rebecca Street. These lots are intended to be sold as serviced lots and will be developed by others.

The independent living community is proposed to include a private laneway with access from Rebecca Street. Pedestrian connections to the neighbouring library will also be provided. The semi-detached units will be constructed as slab-on-grade and will not have basements.

Please refer to the Site Plan in **Appendix A** to view the proposed site layout.

## 1.3 Background Servicing Information

In preparation of the preliminary servicing and SWM strategies, the following design guidelines and standards were used:

- Town of Oakville, Development Engineering Procedures and Guidelines Manual;
- Development Engineering Procedures and Guidelines Manual Addendum #1 (January 2017);
- North Oakville Sustainable Development Checklist & User Guide Subdivision and Site Level Design, prepared by the Town of Oakville (May 2008);
- Conservation Halton Policies and Guidelines for the Administration of Ontario Regulation 162/06 (November 2020);
- Conservation Halton Guidelines for Stormwater Management Engineering Submissions (May 2021);
- Halton Region, Water and Wastewater Linear Design Manual, version 4.0 (April 2019);
- Ministry of Environment, Conservation and Parks (MECP) Stormwater Management Planning and Design Manual (March 2003); and
- Ministry of Transportation (MTO) Drainage Management Manual (1997).

The preliminary site servicing and SWM strategies in this report are based on the following reports:

- Preliminary Geotechnical Investigation, prepared by WSP (February 2021); and
- Proposed Halton Region Paramedic Services Station No. 15 Stormwater Management Report, prepared by MGM Consulting Inc. (August 2017).

The preliminary site servicing and SWM strategies are also based on the following approved Engineering Drawings:

Woodside Drive − Storm Drainage Area Plan No. R-358-00-03, prepared by Trafalgar Engineering Ltd., dated March 2001;



- Woodside Drive − Rebecca to Sta. 0+320 No. 946P1, prepared by Trafalgar Engineering Ltd., dated March 2001;
- Rebecca Street Watermain Replacement Drawing No. PR-1452, prepared by Marshall Macklin Monaghan Ltd., dated July 1993;
- Rebecca Street –Plan & Profile Showing Proposed Storm Sewer from Third Line Road to Fourteen Mile Creek Drawing No. 2, prepared by Franklin McArthur Associates Ltd., dated February 1958; and
- Utility Investigation, prepared by R&B Locating, dated December 2020.

The above listed drawings have been included in Appendix B.

#### 2.0 STORM SERVICING

#### 2.1 Existing Storm Sewer System

As indicated in the utility investigation prepared by R&B Locating and the record drawings (**Appendix B**), the sizes and locations of the existing municipal storm sewers surrounding the site are:

- An 1800 mm diameter concrete storm sewer on Rebecca Street flowing northeast; and
- A 375 mm diameter PVC storm sewer on Woodside Drive flowing southeast.

The existing lands drain southwest via overland flow to the neighbouring Patricia-Picknell Elementary School grounds, where the flows are captured by an existing ditch inlet catchbasin and conveyed to the existing 375 mm diameter storm sewer on Woodside Drive. Please refer to **Section 3.2** for further discussion of the existing drainage.

As presented in the Town of Oakville Stormwater Management Master Plan, the existing 1800 mm diameter sewer on Rebecca Street is surcharged in the 5 year storm event to an elevation above the pipe obvert but below the manhole rim elevation. Based on the Town's Construction Projects web page, there are no works planned in the near future to upgrade the existing storm sewer system. A figure showing the results of the Town's capacity assessment is included in **Appendix D**.

The design of the Woodside Drive sewer accounted for 0.33 ha of drainage from 1258 Rebecca Street, as shown in the drainage plan prepared by Trafalgar Engineering Ltd. (**Appendix B**), with a flow of 42.4 L/s. However, based on the site survey, the entire site area of 0.66 ha plus 0.04 ha of external area currently drains to the Woodside Drive sewer. The Existing Woodside Drive Design Sheet is included in **Appendix D**. The analysis shows that the downstream sewers on Woodside Drive and Sedgewick Drive (EX.MH4 to EX.HW) are surcharged at 102-120% of the pipe capacities during the 5 year storm event under existing conditions.

#### 2.2 Proposed Storm Sewer System

The storm sewer system (minor system) for the proposed development will be designed for the 5 year return storm per the Town of Oakville standards. The storm sewer system will be designed in accordance with the Town of Oakville, Ontario Building Code and MECP guidelines, including the following:

Minor System Conveyance: 5 Year
 Major System Conveyance: 100 Year
 Minimum Pipe Size: 300 mm diameter

Minimum Slope: 0.30%

Minimum / Maximum Velocity: 0.75 m/s - 4.0 m/s

Minimum Pipe Cover: 1.20 m (frost cover)



The rainfall intensity will be determined using the values from Table 3.1 of the Town of Oakville Development Engineering Procedures and Guidelines Manual dated January 2011 as shown in **Table 2.2**:

**Table 2.2 – Rainfall Intensity Parameters** 

Return Period Storm	А	В	С
2 Year	725	4.8	0.808
5 Year	1170	5.8	0.843
10 Year	1400	5.8	0.848
25 Year	1680	5.6	0.851
50 Year	1960	5.8	0.861
100 Year	2150	5.7	0.861

The preliminary storm sewer layout is shown on **Figure 2.1**. Flows captured from the independent living community are proposed to be conveyed to the existing 375 mm diameter Woodside Drive storm sewer. The proposed storm service connection for the independent living community will be routed through the neighbouring Paramedic Services Station property, which is owned by Halton Region. An easement through the neighbouring property will be required to allow for maintenance of the sewer. The proposed service connection will have sufficient depth to service the proposed development.

The installation of the storm connection through the Paramedic Services site was agreed to during a meeting on April 11, 2022 between Halton Region's Paramedic Services Logistics and Housing Action teams. The minutes from that meeting are included in **Appendix D**.

Stormwater from the front yards of the three single family lots is proposed to drain via overland flow to the Rebecca Street right-of-way. Stormwater from the remaining area of the single family lots is proposed to drain via overland flow to the private storm sewer system within the independent living community and ultimately outlet to Woodside Drive. The proposed storm drainage is shown on **Figure 3.2**.

The allowable release rate to the Woodside Drive storm sewer will be 42.4 L/s based on the existing drainage area accounted for in the drainage plan prepared by Trafalgar Engineering Ltd. The Proposed Woodside Drive Design Sheet is included in **Appendix D**. The analysis shows that the proposed development will reduce the existing surcharging between EX.MH4 and EX.HW to 98-116% of the pipe capacities during the 5 year storm event. Please refer to **Section 3.3** for further discussion of the allowable release rate.

The front yards of the single-family lots are proposed to drain uncontrolled to the Rebecca Street right-of-way at a rate of 49.9 L/s in the 100 year storm. This flow corresponds to 1.0% of the existing 1800 mm diameter sewer capacity, and is only a marginal increase in flow. Therefore, the impact on the existing surcharged condition will be minimal. Please refer to the Proposed Rebecca Street Design Sheet in **Appendix D** for further details.

#### 3.0 STORMWATER MANAGEMENT

#### 3.1 Stormwater Runoff Control Criteria

The following stormwater runoff control criteria have been established based on the greatest requirements of each of the design guidelines and standards listed in **Section 1.3**. The stormwater runoff criteria are summarized below in **Table 3.1**.

**Table 3.1: Stormwater Runoff Control Criteria** 

Criteria	Control Measure	
Quantity Control	Control proposed peak flows to existing peak flows for the 2 through 100 year storm events. Where runoff is conveyed to an existing storm sewer, limit the maximum peak flow to the existing 5 year storm event peak flow (Town of Oakville).	
Quality Control	MECP Enhanced Level Protection (80% TSS Removal).	
Erosion Control	Detention/retention of the 25 mm rainfall runoff for a minimum of 24 hours. For smaller sites, demonstrate that the use of pipe storage, infiltration, evapotranspiration, and on-site re-use of runoff has been applied to the extent feasible to reduce erosion potential (Conservation Halton).	
Water Budget	Replicate/maintain as closely as possible existing hydrologic conditions by maintaining a balance between infiltration, runoff and evapotranspiration and minimize negative impacts to groundwater (Conservation Halton).	

#### 3.2 Existing Drainage

Drainage from Catchment 101 and External Catchment EXT-1 (0.66 ha and 0.04 ha respectively, **Figure 3.1**) drain southwest via overland flow to an existing ditch at the southwest corner of the site. Flow in the existing ditch is captured via an existing ditch inlet catchbasin (DICB) which is connected to the existing 375 mm diameter storm sewer on Woodside Drive and outlets to the Sedgewick Forest and ultimately to Lake Ontario. Flows up to the 100 year storm event from Catchment EXT-2 flow southeast to the Woodside Drive sewer system via an existing storm sewer. Flows greater than the 100 year storm event from Catchment EXT-2 (0.41ha, **Figure 3.1**) drain southeast via overland flow to the existing ditch at the southwest corner of the site.

#### 3.3 Allowable Release Rate

The allowable release rate for the proposed development has been established based on controlling the proposed peak flows to existing peak flows for the 2 through 100 year storm events however, where runoff is conveyed to an existing storm sewer, the maximum peak flow is limited to the existing 5 year storm event peak flow. However, as outlined within

**Section 3.2**, the Woodside Drive storm sewer system was designed with a total drainage area of 0.33 ha. Therefore, the allowable release rate to the Woodside Drive storm sewer will be 42.4 L/s based on the existing drainage area accounted for in the Woodside Drive Reconstruction Storm Drainage Area Plan prepared by Trafalgar Engineering Ltd (March 2001), refer to **Appendix B**.

The rational method was used to determine the target release rate from the site based on Intensity-Duration-Frequency (IDF) rainfall curves from the Town of Oakville Design Standards. Supporting calculations are provided in **Appendix E**.

#### 3.4 Stormwater Best Management Practices Selection

In accordance with the Ministry of Environment Stormwater Management Planning and Design Manual (2003), a review of stormwater management best practices was completed using a treatment train approach, which evaluated lot level, conveyance system and end-of-pipe alternatives. The potential best management practices were evaluated based on the stormwater management objectives listed in **Table 3.1**.

The following study area characteristics were taken into consideration:

- The existing site is mostly undeveloped open space with some existing paved areas:
- Based on the Geotechnical investigation, study area soils consist of 50 − 130 mm layers of topsoil over fill materials extending to depths of 0.8 m to 1.5m.
   The fill materials are overlain by native silty clay till extending to depths ranging from 1.9m to 2.6 m., which is underlain by shale bedrock;
- → Within the installed site wells, groundwater was observed at depths ranging between 1.82 m to 2.77 m below existing grade; and
- The proposed site plan development is approximately 0.66 ha and consists of three single detached lots fronting onto Rebecca Street, fourteen single storey semi-detached units and a proposed laneway.

The following are examples of lot-level, conveyance and end-of-pipe controls that will be evaluated for use in the proposed development. While evaluating the following controls, cost, feasibility, groundwater and grading constraints will be taken into consideration.

#### **Lot-Level Controls**

Lot-level controls are at-source measures that reduce runoff prior to stormwater entering the conveyance system, such as:

- Increased topsoil depth;
- Roof leaders to grassed areas;
- At-source storage (i.e. rooftop or parking lot storage);
- Pervious pavements;



Infiltration trenches/soak-away pits.

#### **Conveyance Controls**

Conveyance controls provide treatment of stormwater during the transport of runoff from individual lots to the receiving watercourse or end-of-pipe facility. Examples of conveyance controls include:

- Grassed Swales;
- Pervious pipe system.

#### **End-of-Pipe Controls**

End-of-pipe stormwater management facilities receive stormwater flows from a conveyance system (i.e., storm sewers or ditches) and provide treatment of stormwater prior to discharging flows to the receiving watercourse. Typical end-of-pipe controls include:

- Wet ponds;
- Wetlands;
- Dry ponds;
- Infiltration basins; and
- Underground storage.

A comprehensive assessment of LID practices will be provided in support of the Site Plan Application. The development consists of a private road, three single detached lots and fourteen single storey semi-detached units. It is noted that the site has high groundwater levels and the opportunity for infiltration based LIDs are limited. However, a large portion of the private road consists of permeable pavers, therefore infiltration opportunities within the permeable pavers will be explored at the Site Plan Application stage in addition to grassed swales within the single detached lots and increased topsoil depth.

At the detailed design stage, a water balance evaluation will be incorporated into the detailed stormwater management report that discusses the selection of LIDs in accordance with the Town of Oakville Engineering Design Criteria and Conservation Halton guidelines, and quantifies the proposed rainwater retention volume.

#### 3.5 Proposed Storm Drainage

The proposed major and minor system flow patterns and drainage areas are shown on **Figure 3.2**. As illustrated, runoff from the proposed development will be conveyed to the existing Woodside Drive storm sewer. Major and minor system flows Catchments 201, 202 and EXT-1 (0.42 ha, 0.11 ha and 0.04 ha, respectively, **Figure 3.2**) will be captured and conveyed to the existing Woodside Drive storm sewer via proposed internal storm sewer system. Major and minor system flows from Catchment 204 (0.02 ha, Figure 3.2) will be conveyed southwest, uncontrolled to Woodside Drive. Major and minor system flows from Catchment 203 (0.11 ha, Figure 3.2) will be conveyed north, uncontrolled to Rebecca Street.

#### 3.5.1 Quantity Control

Quantity control for the proposed development will be required to control proposed runoff back to the allowable release rates to the existing Woodside Drive storm sewer. The allowable release rate for the proposed development, as identified in **Section 3.3**, is to be achieved by utilizing an orifice plate and providing on-site storage of stormwater. Preliminary calculations have been completed and approximately 187.4m³ of storage is required to control the 100 year storm event, refer to calculations in **Appendix E**. This is proposed to be achieved through underground storage in the form of a, 0.9 m x 1.8 m box culvert. Details will be provided at the Site Plan application stage.

Due to grading constraints, it is not feasible to provide quantity controls for flows being conveyed to Rebecca Street (Catchment 203, **Figure 3.2**). It is important to note that the existing sewer on Rebecca Street is currently surcharging during a 5 year storm event. The additional flows from Catchment 203 (0.11 ha, **Figure 3.2**) represent 1.0% of the sewer's capacity in the 100-year storm and therefore, will not have a significant impact on the existing surcharge conditions.

#### 3.5.2 Quality Control

Quality control for the proposed development will be required to be provided on-site. This will be achieved through a combination of on-site LID's and a manufactured treatment device.

Quality control for runoff from the proposed development, Catchments 201 and 202 (**Figure 3.2**) will be provided by a treatment train of Best Management (BMP) techniques which could include additional topsoil depth on all grassed areas, permeable pavers, and grassed swale with an end-of-pipe manufactured treatment device, i.e. Jellyfish Unit JF4-2-1 model or approved equivalent. The manufactured treatment device has been sized to achieve Enhanced level quality control (80% TSS removal) as requested by the Town of Oakville (correspondence provided in **Appendix B**).

#### 3.5.3 Erosion Control

As mentioned within **Section 3.1**, detention/retention of the 25 mm rainfall runoff for a minimum of 24 hours is required. However, for smaller sites, demonstrate that the use of pipe storage, infiltration, and evapotranspiration, and on-site re-use of runoff has been applied to the extent feasible to reduce erosion potential. As the proposed site is 0.66 ha, detention/retention of the 25 mm storm event would be challenging. Every extent possible to detain/retain the 25 mm storm event will be investigated and detailed at the site plan application stage via on-site storage within the proposed superpipe and infiltration within the permeable pavers.



#### 3.5.4 Water Balance

Where feasible, measures to minimize impacts on the water budget will be incorporated into the proposed development design.

As noted in **Section 2.1**, the minimum criteria is to maintain existing hydrology function. Proposed BMP's will be fully explored at site plan application stage and a water balance will be completed to determine the existing, proposed and proposed with mitigation infiltration values. As mentioned within **Section 3.4**, potential preliminary BMP's include infiltration within the permeable pavers, increased topsoil depth and grassed swales.

#### 4.0 SANITARY SERVICING

#### 4.1 Existing Sanitary Sewer System

As indicated in the utility investigation prepared by R&B Locating (**Appendix B**), the sizes and locations of the existing sanitary sewers surrounding the site are:

- A 525 mm diameter vitrified clay sanitary sewer on Rebecca Street flowing northeast;
- A 1350 mm diameter concrete sanitary sewer on Woodside Drive flowing south; and
- A 200 mm diameter PVC sanitary sewer on Woodside Drive flowing south.

The subject site previously had a church building which has now been demolished, but was serviced from the existing 525 mm diameter sewer on Rebecca Street, as shown in the record drawings. Based on the Town of Oakville design criteria, the church would have generated a peak flow of approximately 0.48 L/s. The sanitary flow calculations are included in **Appendix F**.

#### 4.2 Proposed Sanitary Sewer System

The proposed sanitary sewer system for the subject development is illustrated on **Figure 2.1**. The independent living community is proposed to be serviced from the existing 525 mm sanitary sewer on Rebecca Street via a new control manhole at the property line. The three single family lots will also be provided with individual service connections to the 525 mm sanitary sewer per Halton Region standards. The proposed service connections will have approximately 2.5 m of cover at the property line, which is sufficient to service the development.

The sanitary sewers within the site will have slopes ranging between 0.5% and 2% (typically) and will be provided at 2.5 m to 1.5 m deep. The sanitary sewer system will be designed in accordance with the Halton Region and MECP criteria, including but not limited to:

- Residential Sanitary Generation Rate: 275 L/cap/day
- Residential Population Density:
  - 55 persons/ha (Single-family)
  - 100 persons/ha (Semi-detached)
- Peaking Factor: Modified Harmon's Equation (Min = 2.0)
- Infiltration Rate: 0.286 L/s/ha
- Minimum Pipe Size: 200 mm diameter
- Minimum Velocity: 0.6 m/s
- Maximum Velocity: 3.0 m/s

Based on the design criteria, the proposed site is expected to generate a flow of 0.96 L/s. The net increase in sanitary flow from the development is 0.47 L/s. This increase in flow corresponds to 0.2% of the existing 525 mm sewer capacity. The proposed flow rate is only marginally higher than the existing condition, and therefore the impact on the existing downstream system will be minimal.

Please refer to the sanitary flow calculations in **Appendix F** for further details.

#### 5.0 WATER SUPPLY AND DISTRIBUTION

#### 5.1 Existing Water Distribution

As indicated in the record drawings (**Appendix B**), the following existing watermains surround the site:

- A 600 mm diameter concrete watermain on the northwest side of Rebecca Street;
- A 150 mm diameter PVC watermain on the southeast side of Rebecca Street; and
- A 150 mm diameter watermain on the west side of Woodside Drive.

There are existing hydrants located on Rebecca Street approximately 20 m west and 63 m northeast of the subject site. A hydrant flow test was completed on October 26, 2022 by Ontario Clean Water Agency (OCWA) to confirm the available flow and pressure in the existing water distribution system. The results of the hydrant flow test are included in **Appendix G**.

#### 5.2 Proposed Water System

The subject development is proposed to be serviced from the existing 150 mm watermain on the southeast side of Rebecca Street. The three single family lots will be provided with individual service connections and water meters per Halton Region standards. The independent living community will be provided with a private water distribution system, with individual meters for each unit. The preliminary watermain layout is shown on **Figure 2.1**.

The proposed private water distribution system will be designed in accordance with Halton Region and MECP criteria, including but not limited to the following:

- Average Daily Demand: 0.275 m³ per capita
- Residential Population Density:
  - 100 persons/ha (semi-detached)
  - 55 persons/ha (single family)
- Peaking Factors:
  - O Maximum Day = 2.25
  - O Maximum Hour = 4.00
- Minimum Pipe Size: 150 mm diameter
- Minimum Pipe Cover: 1.70 m
- Maximum Hydrant Spacing: 150 m (Residential)

Water demand and Fire Underwriters Survey (FUS) calculations can be found in **Appendix G**. The demands for each scenario analysed can be found in **Table 5.1** below.



**Table 5.1: Water Demands and Required Pressure Ranges** 

Scenario	Water Demand	Required Pressure Range
Average Day	0.18 L/s	350 – 550 kPa (Preferred)
Maximum Day	0.40 L/s	275 – 700 kPa (Required)
Maximum Hour	0.71 L/s	
Fire Flow	6,000 L/min	≥ 140 kPa
Fire Flow + Maximum Day	6,024 L/min	

Based on the results of the hydrant flow test, the pressure available in the existing water distribution system was calculated for each water demand scenario. The results are summarized in **Table 5.2** below.

**Table 5.2: Available Water Pressures** 

Scenario	Available Pressure
Average Day	444.0 kPa
Maximum Day	444.0 kPa
Maximum Hour	444.0 kPa
Fire Flow	427.0 kPa
Fire Flow + Maximum Day	426.9 kPa

As shown in the table above, the Average Day, Maximum Day and Maximum Hour demands can be provided within the Town's preferred pressure range of 350-550 kPa. The Fire Flow + Maximum Day demand can be provided at a pressure above the Town's minimum 140 kPa requirement.

Please refer to the calculations in **Appendix G** for further details.

#### 6.0 GRADING

#### 6.1 Existing Grading Conditions

The existing site is relatively flat, with slopes ranging from 1.0 - 3.0% on average. There is an existing ditch in the southeast section of the site which drains south to the existing Patricia-Picknell Elementary School grounds. The ground surface elevations range from 88.90 in the northwest corner of the site to 87.75 in the south corner of the site.

#### **6.2** Proposed Grading Concept

In general, the proposed development has been graded in a manner which satisfies the Town of Oakville lot and road grading criteria, creates the required depth for the sanitary sewer, as well as provision of an efficient earthworks program, including:

Minimum Road Grade: 0.5%Maximum Road Grade: 6.0%Minimum Lot Grade: 2%

►→ Maximum Lot Grade: 5%

Minimum Driveway Grade: 2%Maximum Driveway Grade: 8%

Minimize the need for retaining walls

Minimize the volume of earth to be moved and minimize cut/fill differentials

Minimize the need for rear lot catchbasins

Achieve the stormwater management objectives required for the proposed development.

A preliminary grading plan is provided on **Figure 6.1**. Details will be provided at the site plan application stage.

At the detailed design stage, the preliminary grading shown on **Figure 6.1** will be subject to a more in-depth analysis in an attempt to balance the cut and fill volumes and minimize slopes and retaining walls.

#### 7.0 EROSION AND SEDIMENT CONTROL DURING CONSTRUCTION

Erosion and sediment control measures will be designed at the detailed design stage. These measures may include temporary sediment control fencing, a construction access driveway, check dams and temporary sediment control facilities where required. These measures will be designed and constructed as per the "Erosion and Sediment Control Guide for Urban Construction" document (TRCA, 2019).

The detailed erosion and sediment control plan will be approved by the Town of Oakville prior to any site alteration being undertaken. The plan will address phasing, inspection and monitoring aspects of erosion and sediment control. All reasonable measures will be taken to ensure sediment loading to the adjacent properties and storm sewers is minimized both during and following construction.

#### 8.0 SUMMARY

This Functional Servicing Report has outlined the means by which:

- The proposed development can be serviced from the existing municipal services (i.e. storm, sanitary and water) within the Rebecca Street and Woodside Drive rights-of way;
- The stormwater management criteria can be achieved; and
- The proposed development can be graded in a manner which satisfies the Town of Oakville grading criteria and the stormwater management requirements for this development.

Respectfully Submitted:

**SCS Consulting Group Ltd.** 

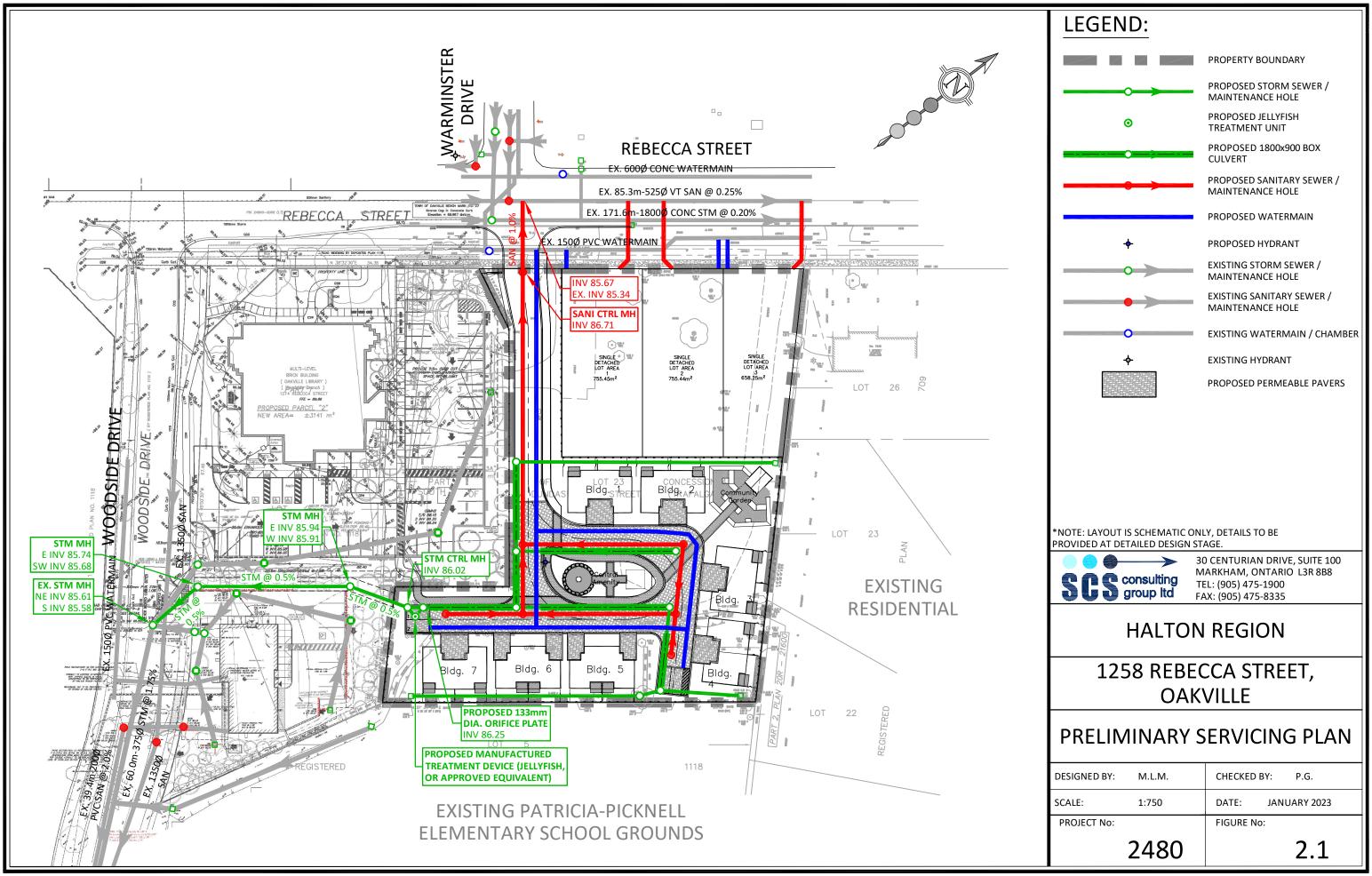
Rebecca Bar, E.I.T.

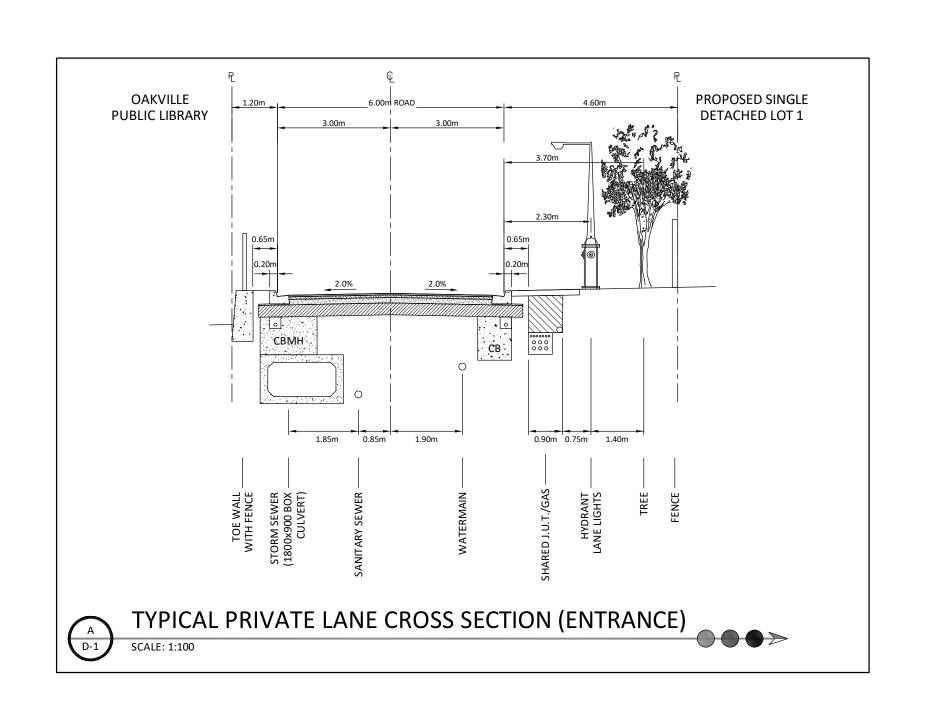
Plebeer Bar

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Jan. 24/23

Paige Turchet, P.Eng. pturchet@scsconsultinggroup.com





LEGEND:

\*NOTE: LAYOUT IS SCHEMATIC ONLY, DETAILS TO BE PROVIDED AT DETAILED DESIGN STAGE.



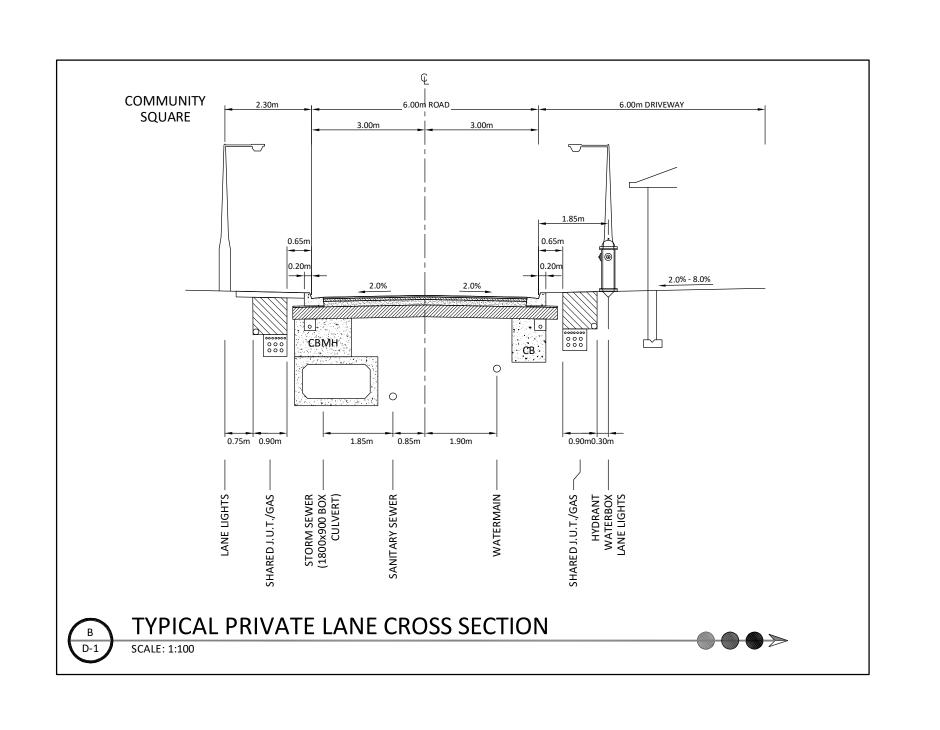
30 CENTURIAN DRIVE, SUITE 100 MARKHAM, ONTARIO L3R 8B8 TEL: (905) 475-1900 FAX: (905) 475-8335

# **HALTON REGION**

# 1258 REBECCA STREET, OAKVILLE

# PRELIMINARY LANEWAY CROSS-SECTIONS

DESIGNED BY:	M.L.M.	CHECKED BY: P.G.
SCALE:	1:100	DATE: JANUARY 2023
PROJECT No:		FIGURE No:
	2480	2.2



LEGEND:

\*NOTE: LAYOUT IS SCHEMATIC ONLY, DETAILS TO BE PROVIDED AT DETAILED DESIGN STAGE.



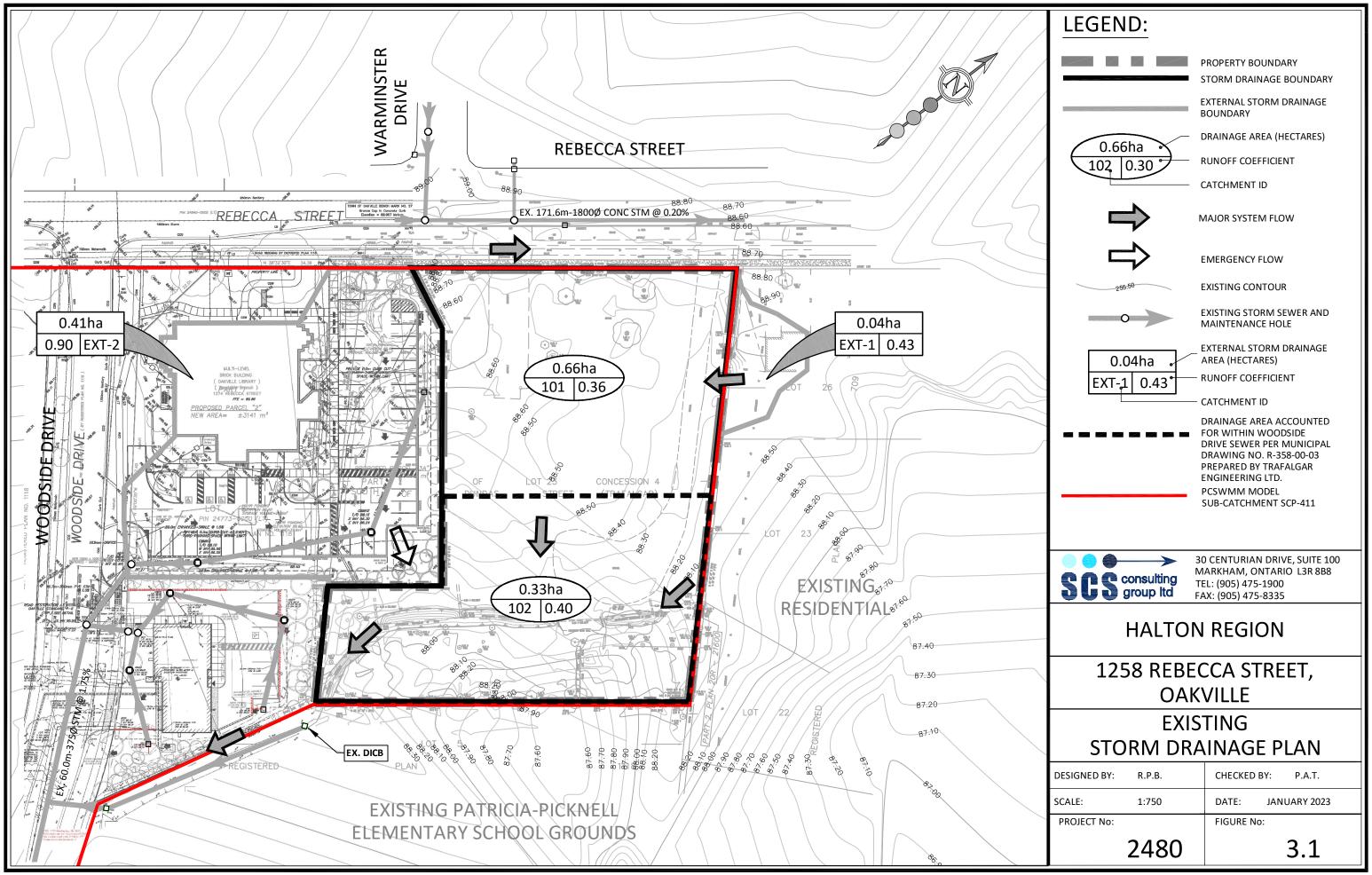
30 CENTURIAN DRIVE, SUITE 100 MARKHAM, ONTARIO L3R 8B8 TEL: (905) 475-1900 FAX: (905) 475-8335

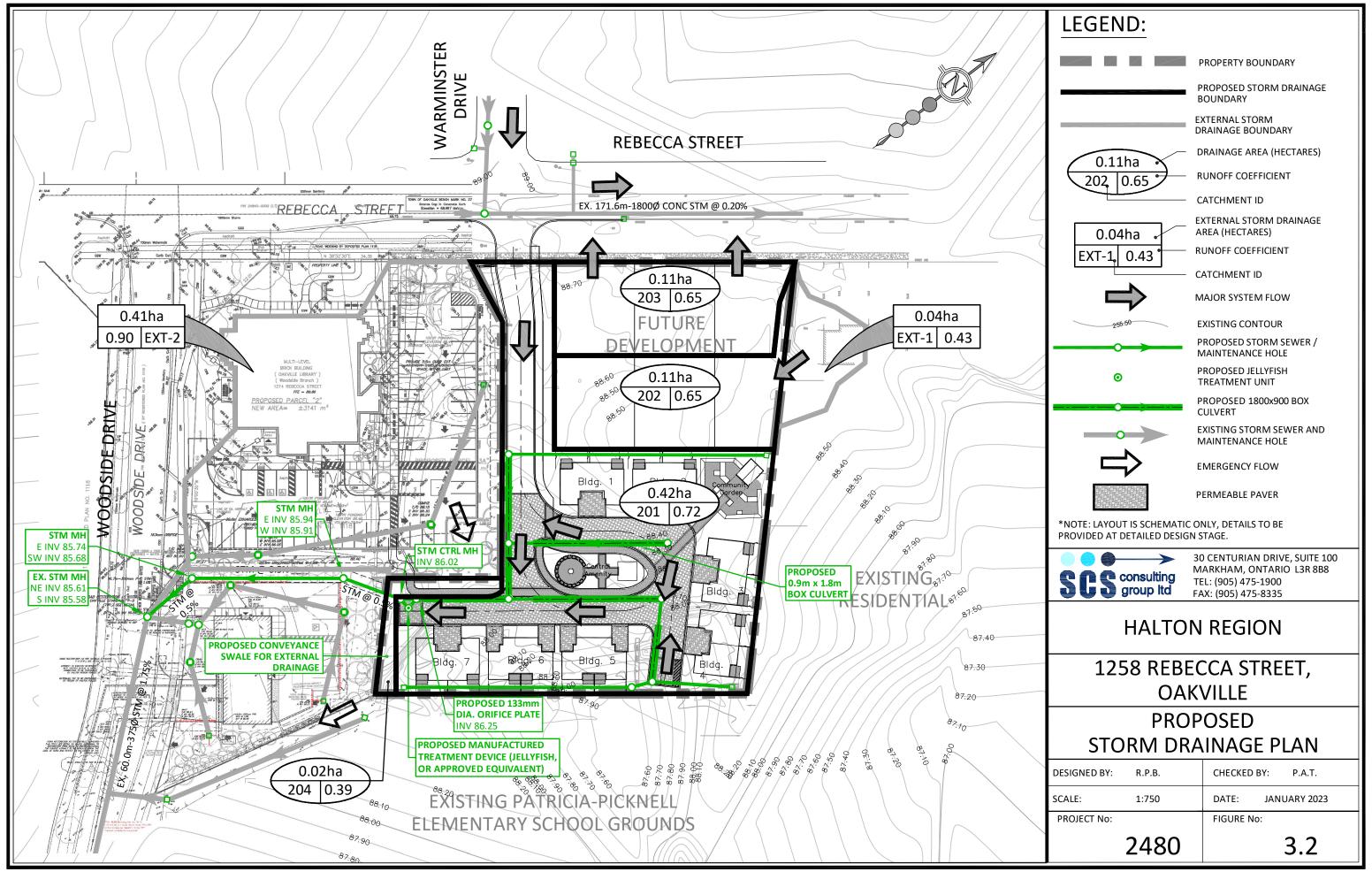
# **HALTON REGION**

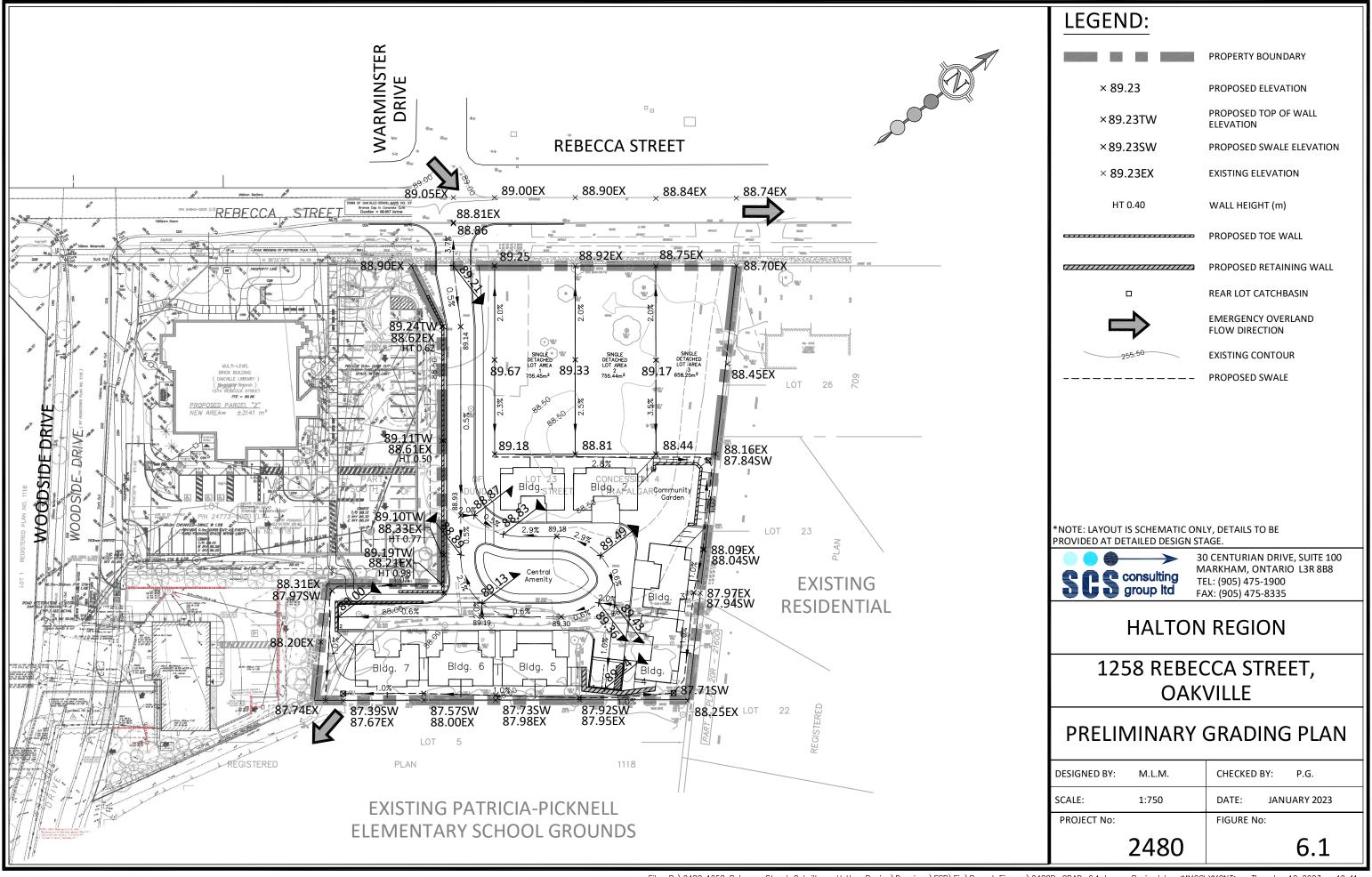
# 1258 REBECCA STREET, OAKVILLE

# PRELIMINARY LANEWAY CROSS-SECTIONS

DESIGNED BY:	M.L.M.	CHECKED BY: P.G.
SCALE:	1:100	DATE: JANUARY 2023
PROJECT No:		FIGURE No:
	2480	2.3



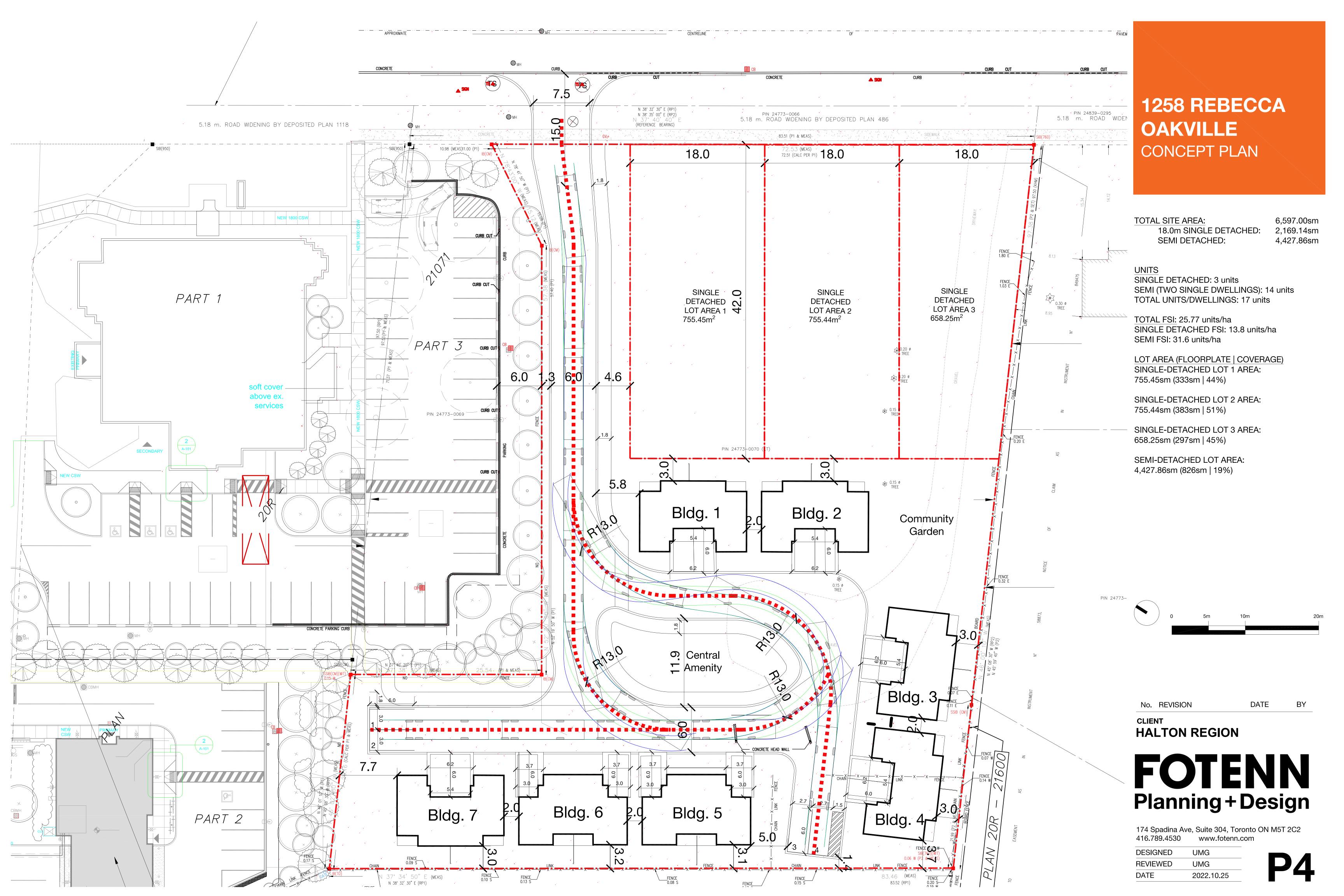




## **APPENDIX A**

# **SITE PLAN**

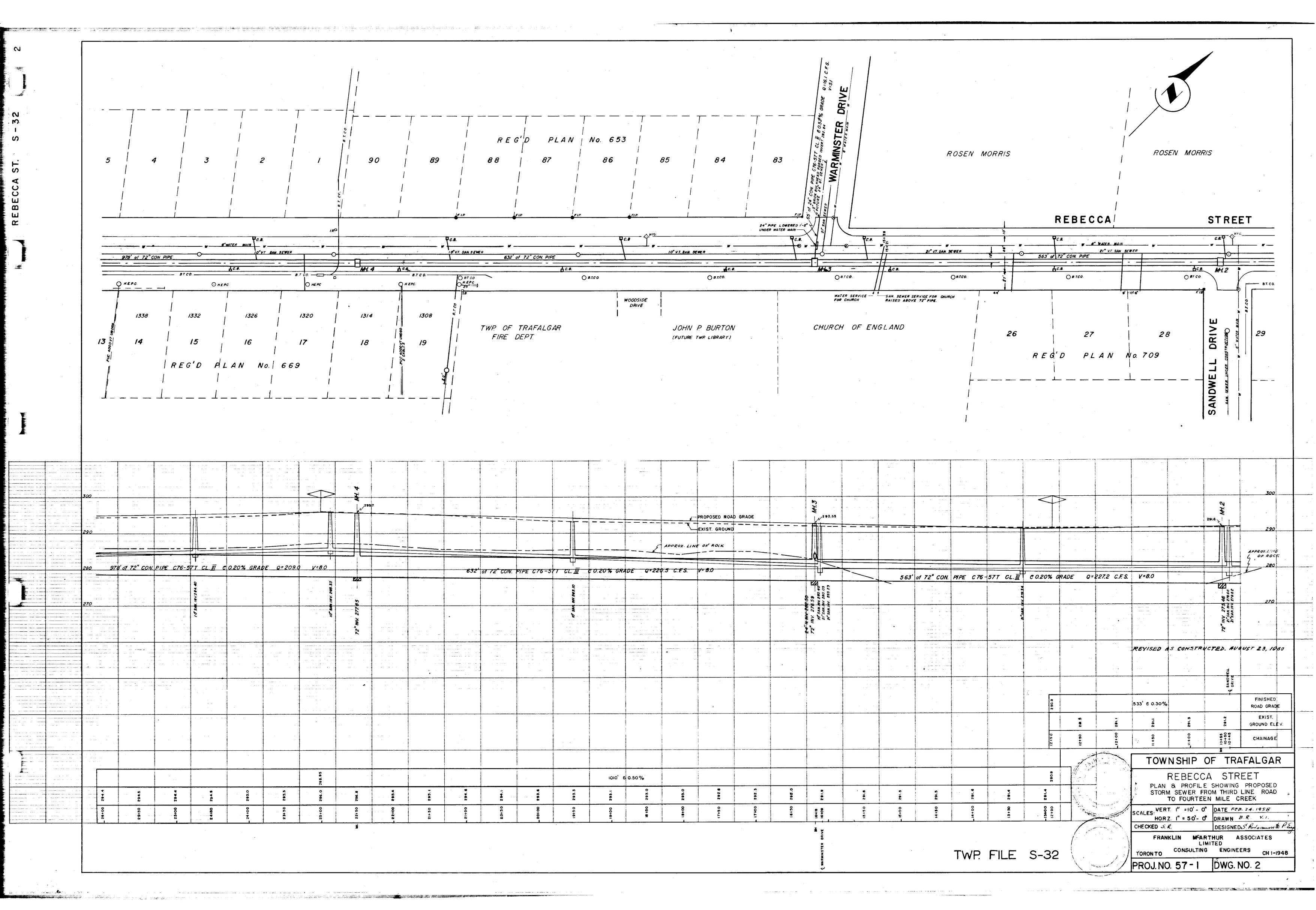


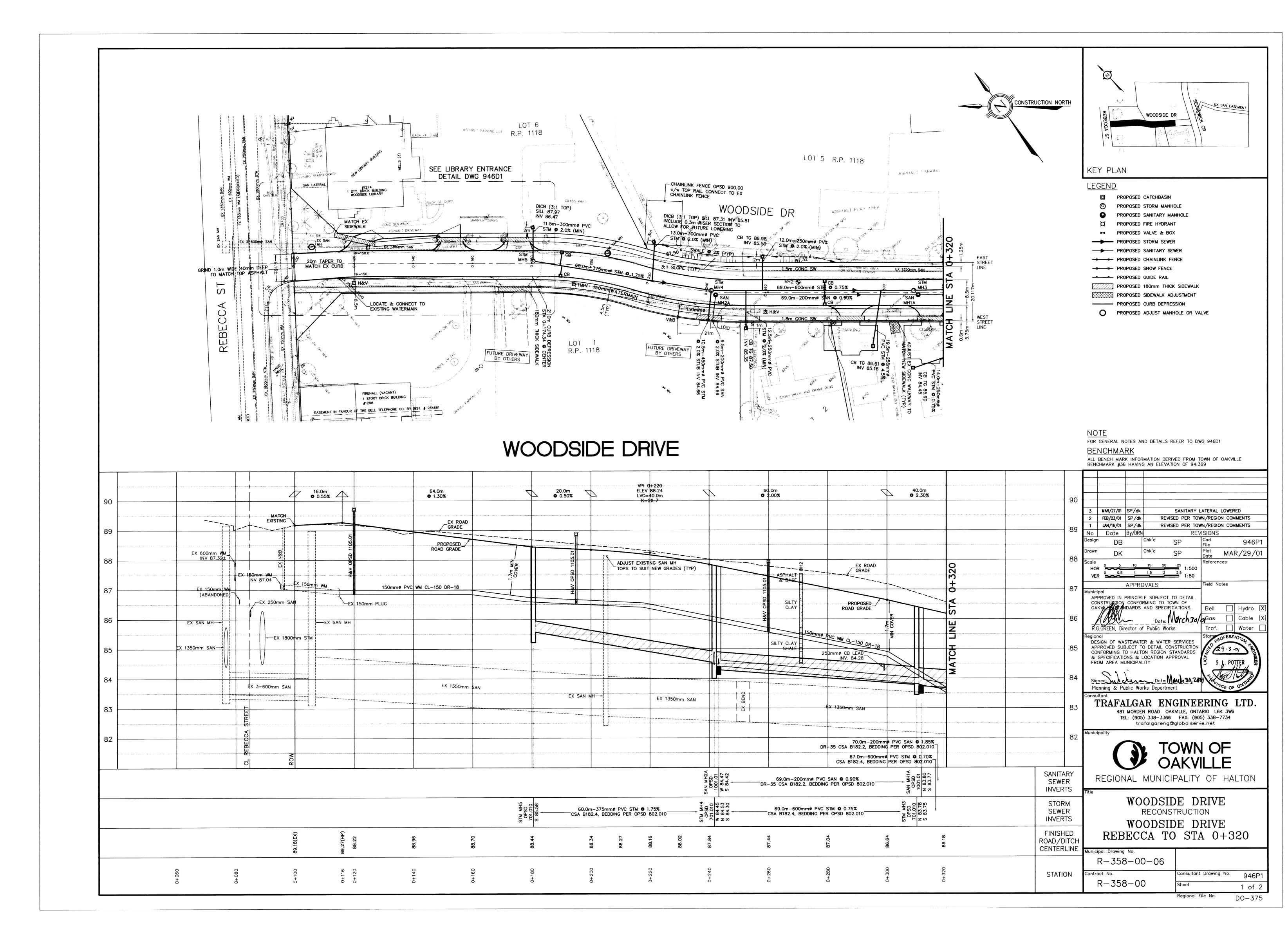


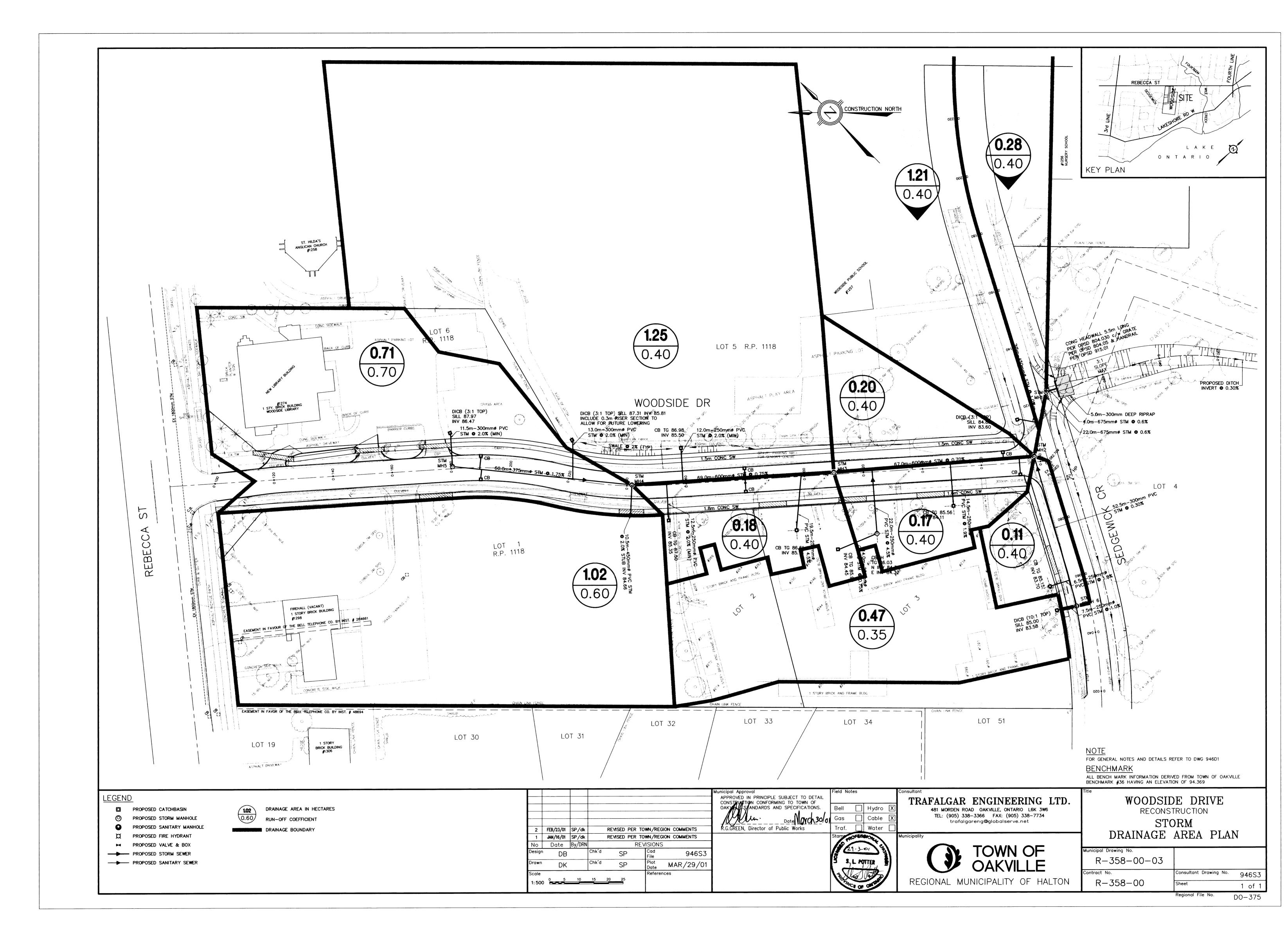
## **APPENDIX B**

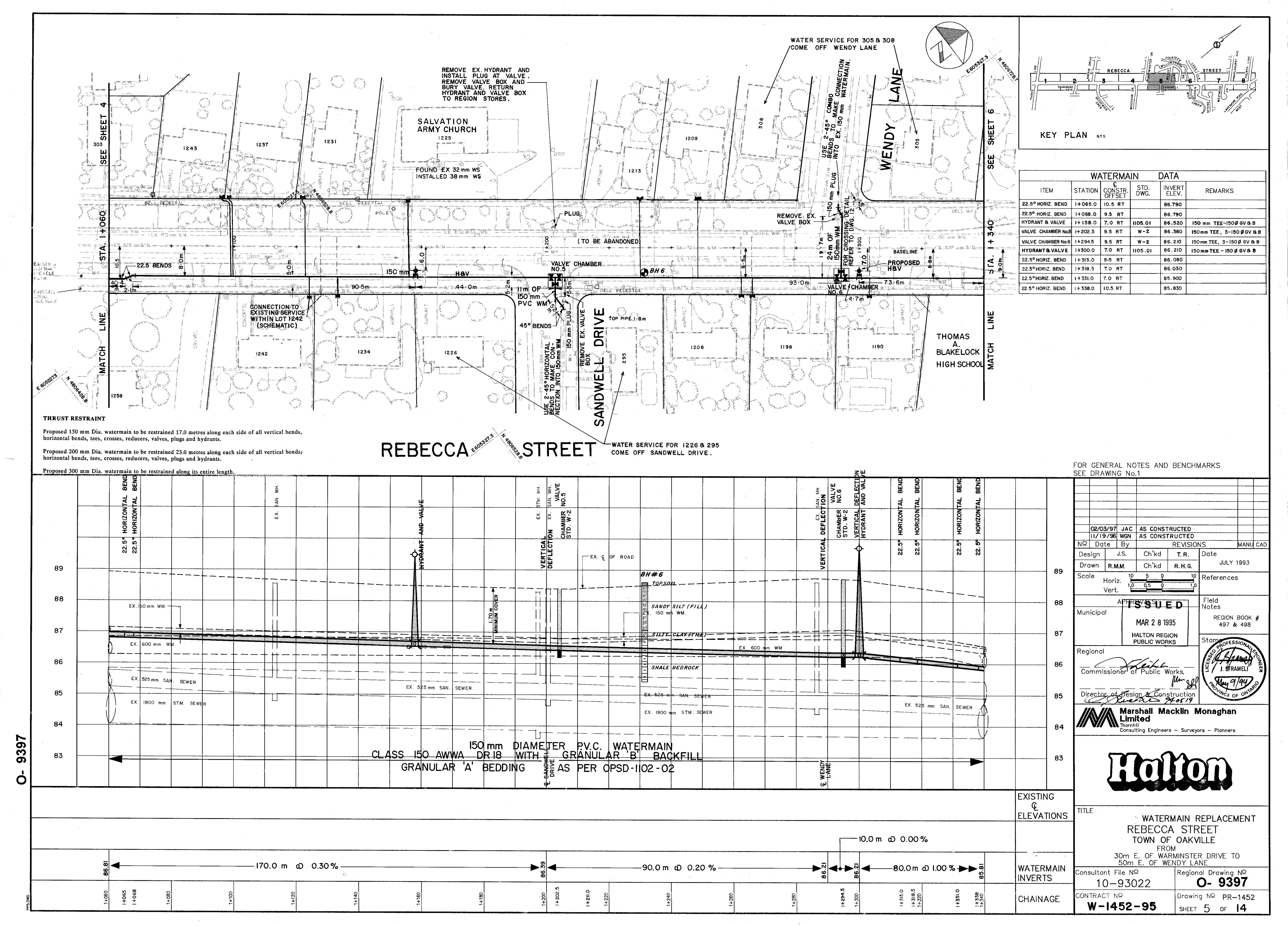
# **RECORD DRAWINGS AND BACKGROUND INFORMATION**

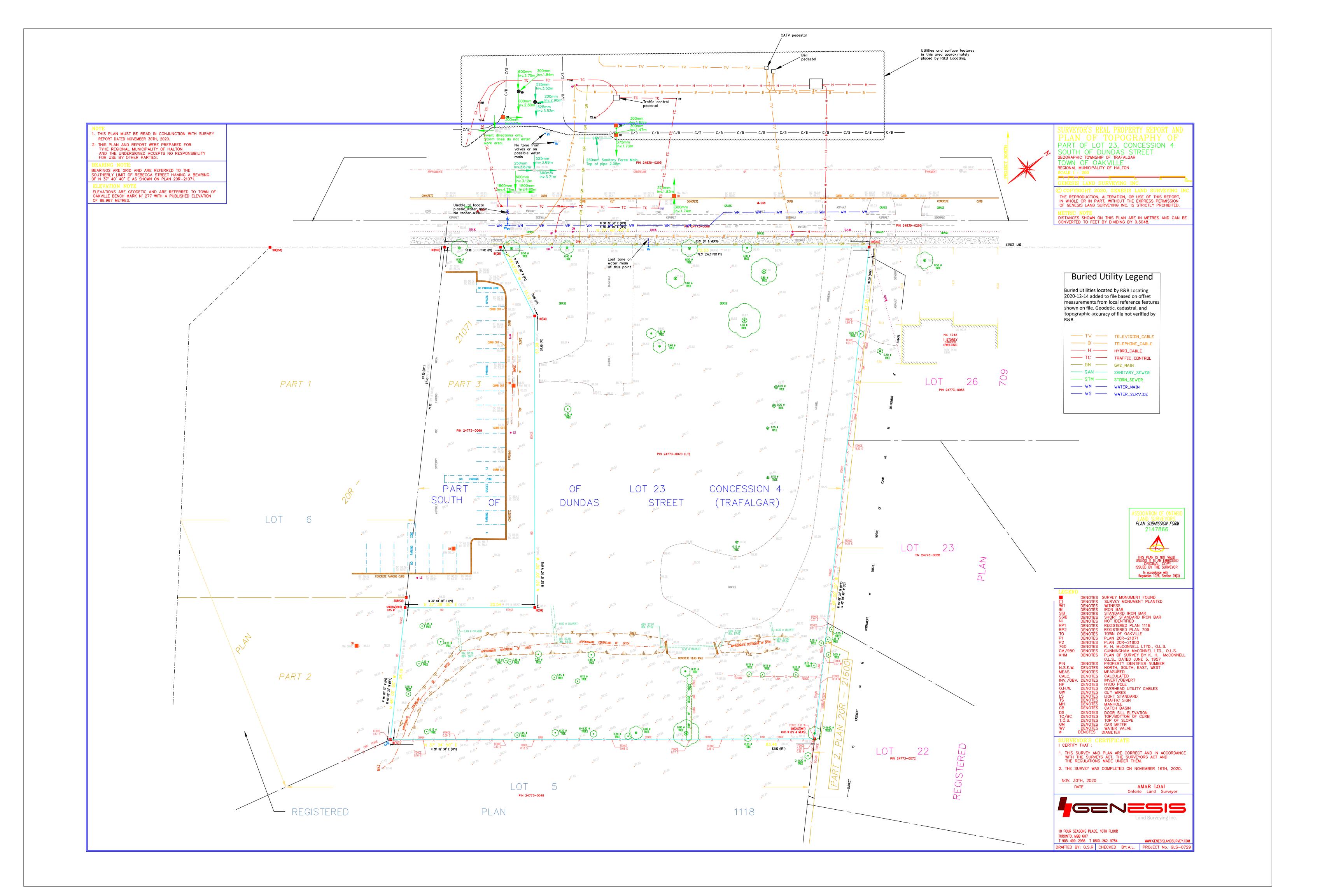


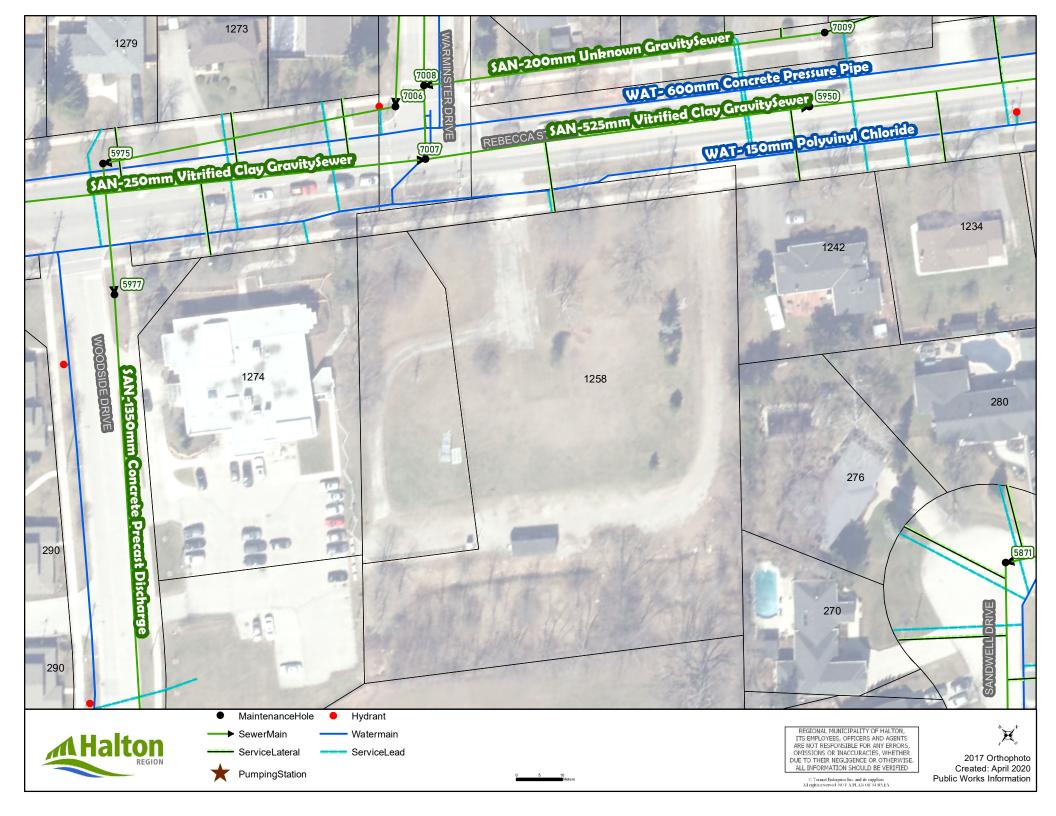








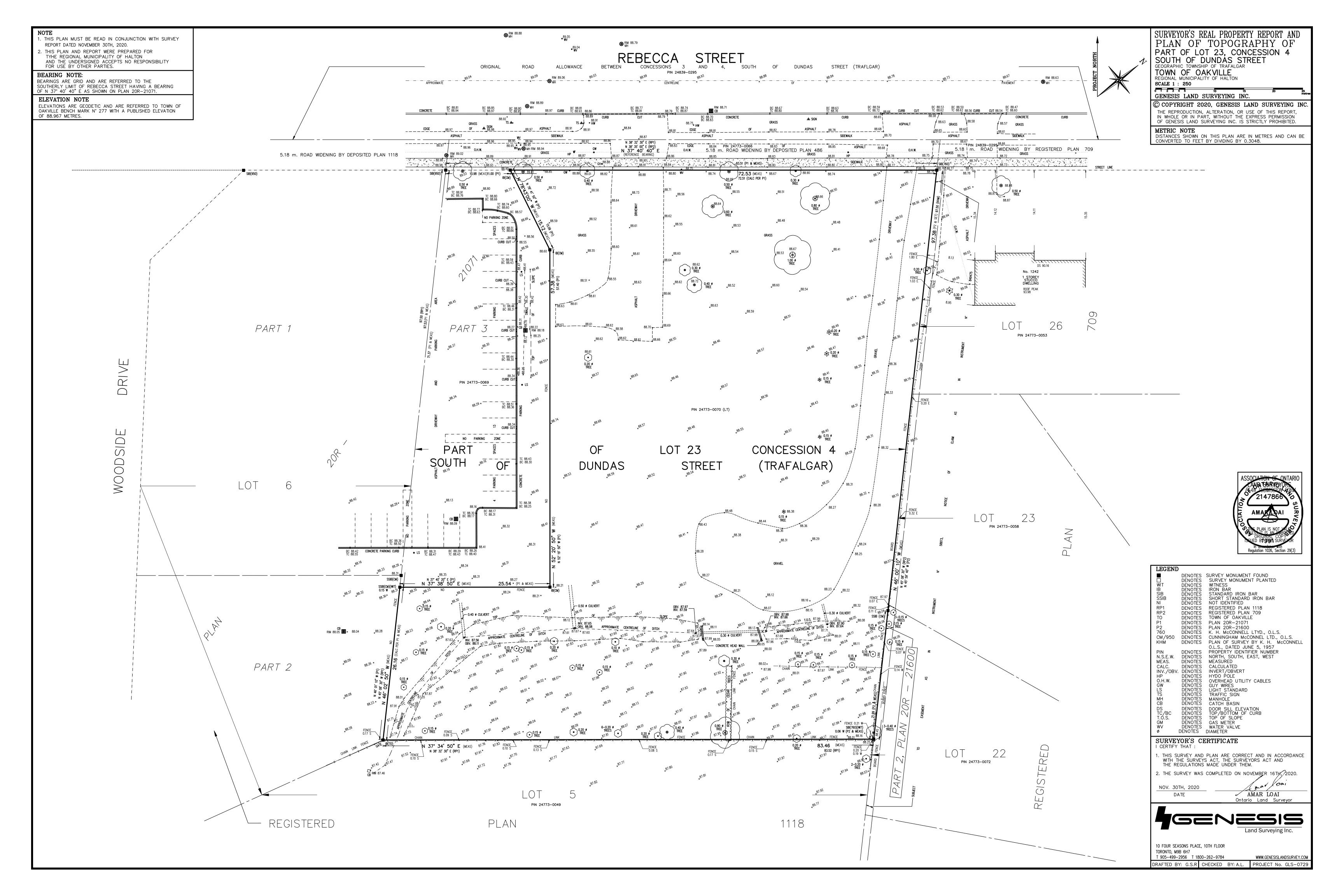




## **APPENDIX C**

# **TOPOGRAPHIC SURVEY**

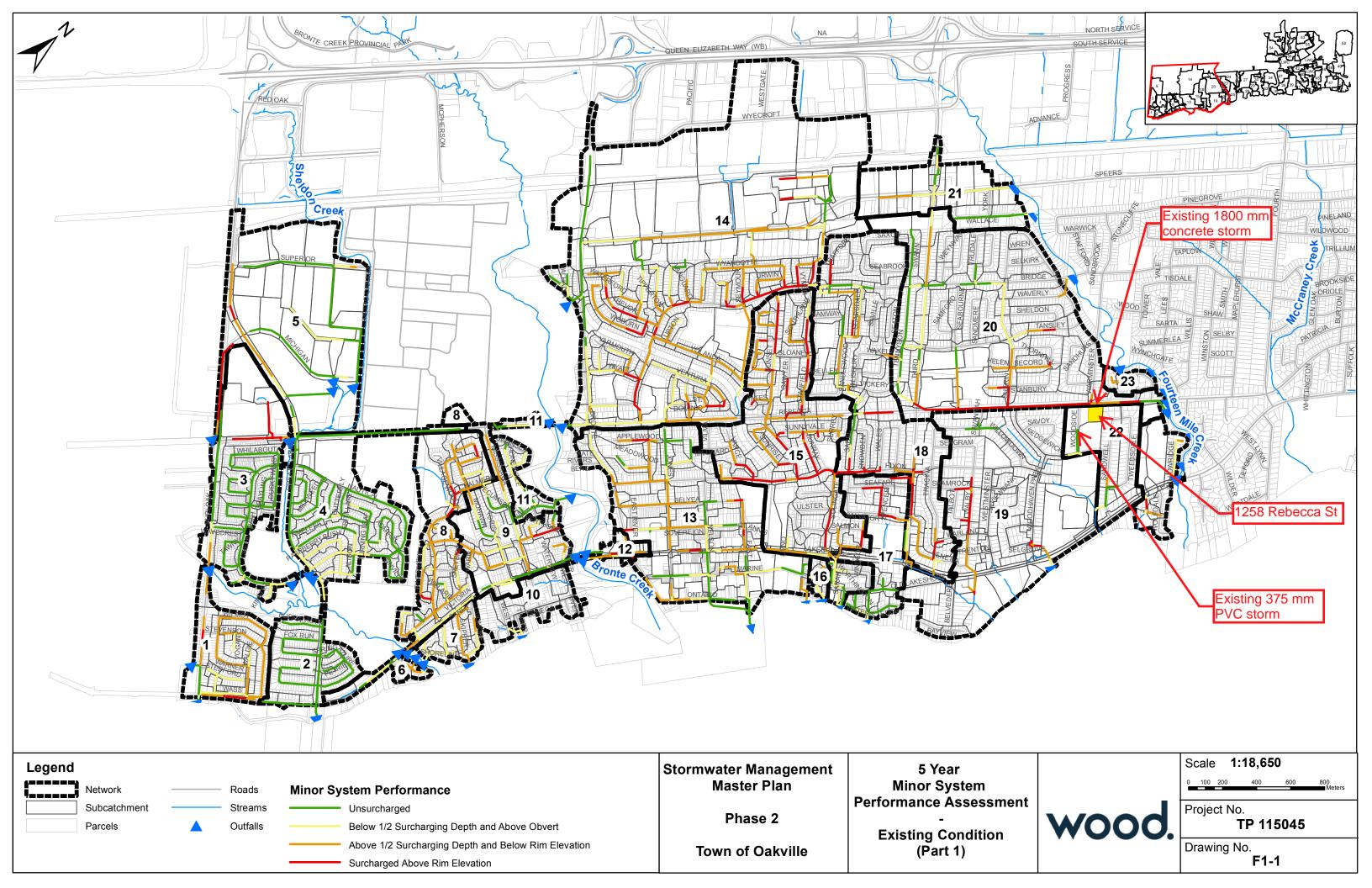


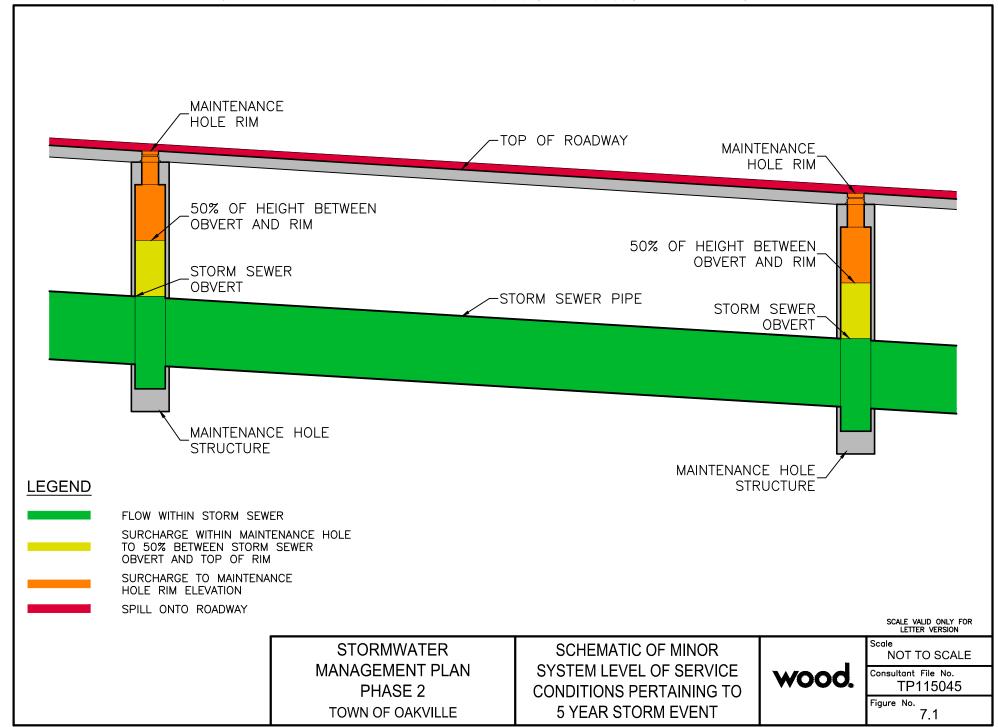


### APPENDIX D

### **STORM SERVICING CALCULATIONS**









Starting  $T_c$  (min)=

### 5-Year Storm Design - Existing Woodside Drive Independent Living Facility 1258 Rebecca Street Town of Oakville, Halton Region

Rainfall Intensity (i) = A A= 1170  $(T_c+B)^c$  B= 5.8 c= 0.843

= Includes Catchments 101 and EXT-1 (Figure 3.1)

**Project: Independent Living Facility** 

Project No. 2480

Date: 12-Jan-23
Designed By: M.L.M.

Reviewed By: P.G.

P:\2480 1258 Rebecca Street Oakville - Halton Region\Design\Pipe Design\Storm\[2480-PRE Dev-Storm Design Sheet-Woodstream Drive Downstream Analysis.xlsm]Design

LOCATION					5 Y	EAR				EXTERN	AL FLOWS		TOTAL FLOW			PIPE DATA				l
	MAINTENA	NCE HOLE	5-YEAR	RUNOFF	"AR"	ACCUM.	RAINFALL	ACCUM.	AREA	ELOW DATE	EVT ELOW	ACCUM.	TOTAL	LENGTH	SLOPE	PIPE	FULL FLOW	FULL FLOW	TIME OF	ACCUM. TIME
STREET	FROM	то	AREA	COEFF.	··AK··	"AR"	INTENSITY	FLOW	AKLA	FLOW RATE	EXT. FLOW	EXT. FLOW	(Qdes)	LENGIH	SLOPE	DIAMETER	CAPACITY	VELOCITY	CONC.	OF CONC.
	1110.01	10	(ha)	(R)			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	(min)
PATRICIA-PICKNELL SCHOOL GROUNDS	EX.DICB1	EX.MH5	0.70	0.31	0.21	0.21	114.21	0.068	0.000	0.000	0.000	0.000	0.068	13.0	2.00	300	0.137	1.935	0.11	10.11
WOODSIDE DRIVE	EX.MH5	EX.MH4	0.71	0.70	0.50	0.71	113.54	0.225	0.000	0.000	0.000	0.000	0.225	60.0	1.75	375	0.232	2.100	0.48	10.59
WOODSIDE DRIVE	EX.PLUG	EX.MH4	1.02	0.60	0.61	0.61	114.21	0.194	0.000	0.000	0.000	0.000	0.194	10.5	2.00	450	0.403	2.535	0.07	10.07
WOODSIDE DRIVE	EX.MH4	EX.MH3	1.10	0.40	0.44	1.76	110.75	0.543	0.000	0.000	0.000	0.000	0.543	69.0	0.75	600	0.531	1.881	0.61	11.20
WOODSIDE DRIVE	EX.MH3	EX.MH2	0.37	0.40	0.15	1.91	107.38	0.570	0.000	0.000	0.000	0.000	0.570	67.0	0.70	600	0.513	1.817	0.61	11.81
SEDGEWICK DRIVE	EX.DICB2	EX.CBMH6	0.47	0.35	0.16	0.16	114.21	0.052	0.000	0.000	0.000	0.000	0.052	7.5	1.00	250	0.059	1.211	0.10	10.10
SEDGEWICK DRIVE	EX.CBMH6	EX.MH2	0.11	0.40	0.04	0.21	113.59	0.066	0.000	0.000	0.000	0.000	0.066	52.5	0.30	300	0.053	0.749	1.17	11.27
SEDGEWICK DRIVE	EX.MH2	EX.MH1	1.21	0.40	0.48	2.60	104.21	0.754	0.000	0.000	0.000	0.000	0.754	22.0	0.60	675	0.651	1.820	0.20	12.02
SEDGEWICK FOREST OUTFALL	EX.MH1	EX.HW	0.28	0.40	0.11	2.72	103.22	0.779	0.000	0.000	0.000	0.000	0.779	4.0	0.60	675	0.651	1.820	0.04	12.05



### 5-Year Storm Design - Proposed Woodside Drive **Independent Living Facility** 1258 Rebecca Street Town of Oakville, Halton Region

Rainfall Intensity (i) = A = 1170B=5.8c = 0.843

Starting  $T_c$  (min)=

= Includes Catchments 201, 202 and EXT-1 (Figure 3.2)

= Allowable Release Rate

Includes Catchment 204 (Figure 3.2) and 0.71 ha from Trafalgar Engineering drainage plan

**Project: Independent Living Facility** 

Project No. 2480

Date: 12-Jan-23 Designed By: M.L.M.

Reviewed By: P.G.

LOCATION					5 Y	EAR				EXTERNA	AL FLOWS		TOTAL FLOW			PIPE DATA	1			
	MAINTENA	NCE HOLE	5-YEAR	RUNOFF	"AR"	ACCUM.	RAINFALL	ACCUM.	AREA	FLOW RATE	EXT. FLOW	ACCUM.	TOTAL	LENGTH	SLOPE	PIPE		FULL FLOW	_	ACCUM. TIME
STREET	FROM	то	AREA	COEFF.		"AR"	INTENSITY	FLOW				EXT. FLOW	(Qdes)			DIAMETER	CAPACITY	VELOCITY	CONC.	OF CONC.
			(ha)	(R)			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	(min)
1258 REBECCA STREET	MH1	EX.MH5	0.00	0.00	0.00	0.00	114.21	0.000	0.57	74.39	0.042	0.042	0.042	15.0	0.50	375	0.124	1.123	0.22	10.22
WOODSIDE DRIVE	EX.MH5	EX.MH4	0.73	0.69	0.50	0.50	112.87	0.158	0.00	0.00	0.000	0.042	0.201	60.0	1.75	375	0.232	2.100	0.48	10.70
WOODSIDE DRIVE	EX.PLUG	EX.MH4	1.02	0.60	0.61	0.61	114.21	0.194	0.00	0.00	0.000	0.000	0.194	10.5	2.00	450	0.403	2.535	0.07	10.07
																				<u> </u>
WOODSIDE DRIVE	EX.MH4	EX.MH3	1.10	0.40	0.44	1.56	110.12	0.476	0.00	0.00	0.000	0.042	0.519	69.0	0.75	600	0.531	1.881	0.61	11.31
WOODSIDE DRIVE	EX.MH3	EX.MH2	0.37	0.40	0.15	1.70	106.79	0.506	0.00	0.00	0.000	0.042	0.548	67.0	0.70	600	0.513	1.817	0.61	11.92
GEDGEWICK DDIVE	EV DICDA	EV CDMIC	0.47	0.35	0.16	0.16	114.21	0.052	0.00	0.00	0.000	0.000	0.052	7.5	1.00	250	0.059	1.211	0.10	10.10
SEDGEWICK DRIVE	EX.DICB2	EX.CBMH6	****			0.16		0.052											0.10	10.10
SEDGEWICK DRIVE	EX.CBMH6	EX.MH2	0.11	0.40	0.04	0.21	113.59	0.066	0.00	0.00	0.000	0.000	0.066	52.5	0.30	300	0.053	0.749	1.17	11.27
																				<u> </u>
SEDGEWICK DRIVE	EX.MH2	EX.MH1	1.21	0.40	0.48	2.40	103.66	0.690	0.00	0.00	0.000	0.042	0.733	22.0	0.60	675	0.651	1.820	0.20	12.13
SEDGEWICK FOREST OUTFALL	EX.MH1	EX.HW	0.28	0.40	0.11	2.51	102.68	0.716	0.00	0.00	0.000	0.042	0.758	4.0	0.60	675	0.651	1.820	0.04	12.16



# 100-Year Storm Design - Proposed Rebecca Street Independent Living Facility 1258 Rebecca Street Town of Oakville, Halton Region

Rainfall Intensity (i) =  $\frac{A}{(T_c+B)^c}$  A= 2150 B= 5.7

Starting  $T_c$  (min)=

c= 0.861

861

= Includes Catchment 203 (Figure 3.2) = Includes 100 Year Runoff Coefficient Increase Factor of 1.25 **Project: Independent Living Facility** 

Project No. 2480

Date: 12-Jan-23 Designed By: M.L.M.

Reviewed By: P.G.

P:\2480 1258 Rebecca Street Oakville - Halton Region\Design\Pipe Design\Storm\[2480-POST Dev-Storm Design Sheet-Rebecca Street.xlsm]Design

LOCATION					100 Y	EAR				EXTERNA	AL FLOWS		TOTAL FLOW			PIPE DATA				
	MAN	HOLE	100-YEAR	RUNOFF	"AR"	ACCUM.	RAINFALL	ACCUM.	AREA	FLOW RATE	EXT FLOW	ACCUM. EXT.	TOTAL	LENGTH	SLOPE			FULL FLOW		ACCUM. TIME
STREET	FROM	то	AREA	COEFF.	, and	"AR"	INTENSITY	FLOW	, inc.	TEOW RATE	EXI.TEO W	FLOW	(Qdes)	LENGTH	SECTE	DIAMETER	CAPACITY	VELOCITY	CONC.	OF CONC.
	11101	10	(ha)	"R"			(mm/hr)	(m3/s)	(ha)	(l/s/ha)	(m3/s)	(m3/s)	(m3/s)	(m)	(%)	(mm)	(m3/s)	(m/s)	(min)	(min)
REBECCA STREET	EX.MH3	EX.MH2	0.11	0.81	0.089	0.089	200.80	0.050	0.000	0.000	0.000	0.000	0.050	171.6	0.20	1800	5.138	2.020	1.42	11.42

Meeting Minutes from April 11, 2022
Paramedic Services Logistics - Joel Smith, Superintendent
Housing Action Team - Zach Richards, Project Manager III

### McClymont, Melissa

From: Richards, Zach < Zach.Richards@halton.ca>

**Sent:** Monday, April 11, 2022 3:34 PM

**To:** Richards, Zach

**Subject:** 220411 - Meeting Notes - we can connect through EMS Lands

- Joel:
  - We can close the one entrance to EMS
  - o EMS trucks can back into the loading bays at the other entrance
  - Would close the one entrance off during road cut for new storm pipe
  - o We are happy to accommodate your needs for your development
  - We need a parking space to the north (library)
    - Melissa: This is likely not feasible due to set backs
  - We need a parking space behind the northern most parking space (towards your site)
    - Melissa: This is a potential solution. Could go for a minor variance. Could extend your entire parking towards our site, but not on our site.
  - The handicap space took away the 8 parking space, we need at least 1 more space.
  - Staff typically go to parking at 6am and 6pm, maybe could use the library lands for a day or two while the storm pipe road cut takes place.
- Jason:
  - o I am good with any solution. EMS lands works well
  - o Can get a by-law exemption for parking on the road during the construction.

#### Zach Richards, P.Eng.

Project Manager III, Housing Action Team (H.A.T.)

Performance, Emergency & Enterprise Risk Management Legislative & Planning Services

**Halton Region** 

905-825-6000, ext. 7108 | 1-866-442-5866



### **APPENDIX E**

### **STORMWATER MANAGEMENT CALCULATIONS**



### **EXISTING WEIGHTED RUNOFF COEFFICIENT**

1258 Rebecca Street, Oakville NT Project Number: 2480

> Date: January 2023 Designer Initials: P.A.T.

Catchment	<b>101</b> Runoff	Outlets to:	Woodside Drive Weighted Runoff
	Coefficient	Area (ha)	Coefficient
Asphalt	0.90	0.03	0.04
Gravel	0.40	0.08	0.05
Grass	0.25	0.55	0.21
TOTAL		0.66	0.30

Catchment	Catchment EXT-1 Runoff		Woodside Drive Weighted Runoff
	Coefficient	Area (ha)	Coefficient
Asphalt	0.90	0.003	0.07
Rooftops	0.90	0.01	0.18
Grass	0.25	0.03	0.18
TOTAL	·	0.04	0.43



### ALLOWABLE RELEASE RATE

1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023

Designer Initials: P.A.T.

5 Year storm

Runoff Coefficient: C1 = 0.40

Allowable Release Rate Calculation										
Outlet	let Area time Intensity Flow									
ID	ID t i=a/(t+b)^c Q=CiA/360									
	ha	min	mm/hr	l/s						
Woodside Drive	0.33	10.00	114.21	42.4						

\* a,b,c's per Town of Oakville

As identified on the Woodside Drive Reconstruction Storm Drainage Area Plan prepared by Trafalgar Engineering Ltd. dated March 2001 (refer to Appendix B), approximately 0.33 ha of the existing site has been accounted for within the Woodside Drive storm sewer system.



Future

Future

### PROPOSED WEIGHTED RUNOFF COEFFICIENT

1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023 Designer Initials: P.A.T.

	100 Yea	r Runoff Coeffic	cient Increase Factor:	1.25
Catchment	201	Outlets to:	Woodside Drive	
	Runoff Coefficient	Area (ha)	Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Asphalt	0.90	0.10	0.22	0.25
Rooftops	0.90	0.09	0.19	0.21
Permeable Pavement	0.90	0.11	0.24	0.27
Grass	0.25	0.12	0.07	0.09
TOTAL		0.42	0.72	0.81
Catchment	202  Runoff Coefficient	Outlets to:  Area (ha)	Woodside Drive Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Residential Development	0.65	0.11	0.65	0.81
TOTAL		0.11	0.65	0.81
Catchment	EXT-1  Runoff Coefficient	Outlets to:  Area (ha)	Woodside Drive Weighted Runoff Coefficient	Weighted Runoff Coefficient (100 Year)
Asphalt	0.90	0.003	0.07	0.07
Rooftops	0.90	0.01	0.18	0.20
Grass	0.25	0.03	0.18	0.23
TOTAL			*****	0.25
		0.04	0.43	0.50
Catchment	203	0.04 Outlets to:		
	Runoff Coefficient	Outlets to: Area (ha)	0.43  Rebecca Street  Weighted Runoff Coefficient	0.50  Weighted Runoff Coefficient (100 Year)
Catchment Residential Development	Runoff	Outlets to:	0.43 Rebecca Street Weighted Runoff	0.50 Weighted Runoff
	Runoff Coefficient	Outlets to: Area (ha)	0.43  Rebecca Street  Weighted Runoff Coefficient	0.50  Weighted Runoff Coefficient (100 Year)
Residential Development	Runoff Coefficient 0.65	Outlets to:  Area (ha)  0.11	0.43  Rebecca Street  Weighted Runoff Coefficient  0.65	0.50  Weighted Runoff Coefficient (100 Year) 0.81
Residential Development TOTAL	Runoff Coefficient 0.65  204  Runoff	Outlets to:  Area (ha)  0.11  0.11  Outlets to:	0.43  Rebecca Street  Weighted Runoff Coefficient  0.65  0.65  Woodside Drive  Weighted Runoff	0.50  Weighted Runoff Coefficient (100 Year) 0.81 0.81  Weighted Runoff

0.02

0.39

0.47

TOTAL



### PROPOSED WEIGHTED RUNOFF COEFFICIENT

1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023 Designer Initials: P.A.T.

### **Overall Total**

	Runoff		Weighted Runoff
Catchment	Coefficient	Area	Coefficient
201	0.72	0.42	0.44
202	0.65	0.11	0.10
EXT-1	0.43	0.04	0.02
203	0.65	0.11	0.10
204	0.39	0.02	0.01
TOTAL		0.70	0.67



### **SUMMARY**

1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023

Designer Initials: P.A.T.

						100 Year				
Catchment ID	Routing		Runoff Coef.	Area (ha)	Release Rate (L/s) 12	Storage Required (m³) 1	Storage Available (m³) ³	Orifice Size (mm)	Orifice Release Rate (L/s)	Uncontrolled Release Rate (L/s)
201	is routed through		0.81	0.42	37.7	187.4	194.4	133	37.7	
202	is routed through	201	0.81	0.11	49.9	0.0	0.0	uncontrolled	-	49.9
EXT-1	is routed through	201	0.50	0.04	11.1	0.0	0.0	uncontrolled	-	11.1
203	is routed through		0.81	0.11	49.9	0.0	0.0	uncontrolled	-	49.9
204	is routed through		0.47	0.02	4.7	0.0	0.0	uncontrolled	-	5
Total				0.70	153.3	187.4	194.4	-	-	

Woodside Drive Allowable Release Rate 42.4 L/s Woodside Drive Proposed Release Rate 42.4 L/s

Rebecca Street Proposed Release Rate 49.9 L/s

#### Notes:

<sup>&</sup>lt;sup>1</sup> Per Modified Rational Calculations (attached)

<sup>&</sup>lt;sup>2</sup> The allowable release rate was determined using the area identified in the Woodside Drive Storm Drainage Area Reconstruction Plan (Trafalgar, March 2001)

<sup>&</sup>lt;sup>3</sup> See attached for orifice details



1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023 Designer Initials: P.A.T.

201 Area ID:

> **0.424** ha Area =

"C" = 0.81 AC= 0.3442

Tc = **10.0** min

Time Increment = **3.0** min

Release Rate = **37.73** l/s Town of Oakville 100 Year

**187.4** m<sup>3</sup> Max.Storage =

a= 2150 b= 5.7 c= 0.861

Time	Rainfall	Storm	Runoff	Released	Storage	
	Intensity	Runoff	Volume	Volume	Volume	
(min)	(mm/hr)	(l/s)	(m <sup>3</sup> )	(m <sup>3</sup> )	(m <sup>3</sup> )	
10.0	200.8	253.19	151.9	22.6	129.3	
13.0	172.7	217.80	169.9	26.0	143.9	
16.0	152.0	191.61	183.9	29.4	154.5	
19.0	135.9	171.39	195.4	32.8	162.6	
22.0	123.2	155.29	205.0	36.2	168.8	
25.0	112.7	142.13	213.2	39.6	173.6	
28.0	104.0	131.17	220.4	43.0	177.4	
31.0	96.7	121.88	226.7	46.4	180.3	
34.0	90.3	113.91	232.4	49.8	182.6	
37.0	84.8	106.98	237.5	53.2	184.3	
40.0	80.0	100.91	242.2	56.6	185.6	
43.0	75.8	95.53	246.5	60.0	186.5	
46.0	72.0	90.74	250.4	63.4	187.1	
49.0	68.6	86.44	254.1	66.8	187.4	
52.0	65.5	82.55	257.6	70.2	187.4	<<<<
55.0	62.7	79.03	260.8	73.6	187.2	
58.0	60.1	75.81	263.8	77.0	186.9	
61.0	57.8	72.87	266.7	80.4	186.3	
64.0	55.6	70.16	269.4	83.8	185.7	
67.0	53.7	67.66	272.0	87.1	184.8	
70.0	51.8	65.34	274.4	90.5	183.9	
73.0	50.1	63.19	276.8	93.9	182.9	
76.0	48.5	61.19	279.0	97.3	181.7	
79.0	47.0	59.32	281.2	100.7	180.4	

<sup>&</sup>lt;sup>1</sup> The storm runoff from Catchment 202 and EXT-1 has been added to the storm runoff of Catchment 201



### ON-SITE DETENTION AND ORIFICE DETAILS

1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023 Designer Initials: P.A.T.

Area ID 201

Orifice Equation:  $Q = C_d A (2gh)^{1/2}$ 

Orifice Diameter: 133 mm

Area:  $0.014 \text{ m}^2$   $g = 9.81 \text{ m/sec}^2$  $C_d = 0.62$  Type of Control: vertical
Location: 1

Pipe Storage

Diameter	Area	Length	Volume
(mm)	(m²)	(m)	(m <sup>3</sup> )
0.9 * 1.8 BOX	1.620	120	194.4
	To	194.4	

	Stage (m)	Head (m)	Storage (m³)	Discharge (m³/s)
Invert E.L.	86.25	0.00	0.0	0.00
100 Year WL	87.30	0.98	194.4	0.038



1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023

Designer Initials: P.A.T.

Area ID: 202

Area = **0.110** ha

"C" = **0.81** AC= **0.0894** 

Tc = **10.0** min

Time Increment = 3.0 min

Release Rate = 49.89 l/s Town of Oakville 100 Year

Max.Storage =  $0.0 \text{ m}^3$  a= 2150

b= 5.7 c= 0.861

### NOTE: Catchment 202 is routed through Catchment 201

Time	Rainfall	Storm	Runoff	Released	Storage
	Intensity	Runoff	Volume	Volume	Volume
(min)	(mm/hr)	(l/s)	(m <sup>3</sup> )	(m <sup>3</sup> )	(m <sup>3</sup> )
10.0	200.8	49.89	29.9	29.9	0.0

<<<



1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023 Designer Initials: P.A.T.

Area ID: EXT-1

Area = **0.040** ha

"C" = **0.50** 

AC= **0.0200** 

Tc = **10.0** min

Time Increment = 3.0 min

Release Rate = 11.14 l/s Town of Oakville 100 Year

Max.Storage =  $0.0 \text{ m}^3$  a= 2150

b= 5.7 c= 0.861

NOTE: Catchment EXT-1 is routed through Catchment 201

1						
ı	Time	Rainfall	Storm	Runoff	Released	Storage
	(min)	Intensity (mm/hr)	Runoff (l/s)	Volume (m³)	Volume (m³)	Volume (m³)
	10.0	200.8	11.14	6.7	6.7	0.0

<<<<



1258 Rebecca Street, Oakville Project Number: 2480 Date: January 2023

Designer Initials: P.A.T.

Area ID: 203

Area = **0.110** ha

"C" = **0.81** AC= **0.0894** 

Tc = **10.0** min

Time Increment = 3.0 min

Release Rate = 49.89 l/s Town of Oakville 100 Year

Max.Storage =  $0.0 \text{ m}^3$  a= 2150

b= 5.7 c= 0.861

Time	Rainfall	Storm	Runoff	Released	Storage
	Intensity	Runoff	Volume	Volume	Volume
(min)	(mm/hr)	(l/s)	(m <sup>3</sup> )	(m <sup>3</sup> )	(m³)
10.0	200.8	49.89	29.9	29.9	0.0

<<<

## APPENDIX F SANITARY FLOW CALCULATIONS





### SANITARY SEWER FLOW CALCULATIONS

Job Number: 2480 Date: January 2023 Designer Initials: M.L.M.

### 1258 Rebecca Street

Proposed Sanitary Flow Calculations	
Average Residential Flow Rate	275.0 litres/capita/day
Residential Population Density	
Single Family Semi-detached	55 persons/ha 100 persons/ha
Residential Population Single Family (0.22 ha)	12 persons
Semi-detached (0.44 ha)  Total population	44 persons <b>56 persons</b>
rotal population	36 persons
Peaking Factor	4.30
Residential Peak Flow	0.77 L/s
Site Area	0.66 ha
Infiltration (0.286 L/s/ha)	0.189 L/s
Total Proposed Peak Sanitary Flow	0.96 L/s
Existing Sanitary Flow Calculations	
Community Services Flow Rate	11,000 litres/ha/day
Community Services Population Density	40 persons/ha
Community Services Population (0.66 ha)	26.4 persons
Peaking Factor	3.49
Existing Peak Flow	0.29 L/s
Site Area	0.66 ha
Infiltration (0.286 L/s/ha)	0.189 L/s
Total Existing Peak Flow	0.48 L/s
Net Increase in Sanitary Peak Flow	0.47 L/s



Sanitary Design Sheet 1258 Rebecca Street Halton Region Town of Oakville

Tow
Minimum Sewer Diameter (mm) = 200 Avg. Domestic Flow (l/cap/day) = 275

Mannings n = 0.013 Infiltration Rate (l/s/ha) = 0.286

Minimum Velocity (m/s) = 0.60 Max. Harmon Peaking Factor = 0.0

Maximum Velocity (m/s) = 3.65 Min. Harmon Peaking Factor = 2.0

Minimum Pipe Slope (%) = 0.50 NOMINAL PIPE SIZE USED

Project: 1258 Rebecca Street

Project No. 2480

Date: 12-Jan-23

Designed By: M.M.

Reviewed By: P.G.

P.\2480 1258 Rebecca Street Oakville - Halton Region\Design\Pipe Design\Sanitary\[2480-Sanitary Sheet Design.xlsm]Desi

LOCATION						RESIDEN	TIAL			INI	DUSTRIAL	/COMMERCIA	AL/INSTITUT	IONAL			F	LOW CALCU	LATIONS					1	PIPE DATA	A	ļ
	MAN	HOLE	AREA	ACCUM.	UNITS	DEN	SITY	RESIDENTIAL	ACCUM. RESIDENTIAL	AREA	ACCUM.	POPULATION	FLOW	ACCUM. EQUIV.	INFILTRATION	TOTAL ACCUM.	AVG. DOMESTIC	ACCUM. AVG. DOMESTIC	PEAKING	PEAKED RESIDENTIAL	ICI	TOTAL	LENGTH	PIPE	SLOPE	FULL FLOW	FULL FLOW
STREET	FROM	то	AREA	AREA	UNIIS	PER UNIT		POPULATION	POPULATION	AREA	AREA	DENSITY	RATE	POPULATION		POPULATION	FLOW	FLOW	FACTOR	FLOW	FLOW	FLOW	LENGIH	DIAMETER	SLOFE	CAPACITY	VELOCITY
			(ha)	(ha)	(#)	(p/unit)	(p/ha)			(ha)	(ha)	(p/ha)	(l/s/ha)		(L/s)		(L/s)	(L/s)		(L/s)	(L/s)	(L/s)	(m)	(mm)	(%)	(L/s)	(m/s)
1258 REBECCA STREET	CTRL.MH	EX.MH1A	0.66	0.66	0		84.8	56	56	0	0	0	0	0	0.19	56	0.2	0.2	4.30	0.77	0.0	0.96	15.9	200	1.00	32.8	1.04
REBECCA STREET	EX.MH1A	EX.MH2A	0	0.66	0			0	56	0	0	0	0	0	0.19	56	0.0	0.2	4.30	0.77	0.0	0.96	85.3	525	0.25	214.9	0.99

### **APPENDIX G**

### **WATER MODELLING ANALYSIS**



#### **HYDRANT INSPECTION & FLOW REPORT**



**HYDRANT DESCRIPTION** 

Prepared By: The Ontario Clean Water Agency

Prepared For: SCS Consulting Residual Hyd Andrew Cruickshank

Flow Hyd(s) Kelly Smith

SUGGESTED NFPA RATING BLUE **CLASS AA** 

7547 gpm @ 20 psi (138 kPa)

Time: 10:17 AM

Date: 26-Oct-22

Hydrant	ID:	75	17		Side	of Street:	South		M	ake:		Concord	Ор	en Dir:	L	.eft
Addre	ddress: cation:  LINSPECTION OK - Cotion OK FR N/A ct		1	234 Re	becca St	reet			Мо	del:	Pr	remier D-67M	La	titude:		
Locatio	n:			Oak	ville, ON Ye					ear:		1995	Lon	gitude:		
GENERAL INSPECTION OK - Good (					dition	lition FR - Future Repair Required N/A					I/A -	A - Not Applicable CF - Component Failu				
Upper Section	ОК	FR	N/A	CF	<u>M</u>	id Section	ОК	FR	N/A	CF		General	ОК	FR	N/A	CF
Bonnet			<b>√</b>		Po	ort Height			<b>√</b>			Accessibility			✓	
Operating Nut			<b>√</b>		Cap	os / Nozzles			<b>√</b>			Position / Height			<b>√</b>	
Gaskets / Bolts			<b>✓</b>			Chains			<b>✓</b>			Paint Cond			<b>✓</b>	
O-Ring(s)			<b>✓</b>		Tra	affic Flange			<b>✓</b>			Drain Ports			<b>✓</b>	
Hydı	ostatic	Leak Te	esting			<u>Maintenance</u>						Auxilia	ary / Se	condary	<u>Valve</u>	
Hydrant	Above	Grade	Leak	N/A		Lubricate	Operati	ng Nut		N/A		Located	I / Acce	ssible		N/A
Closed	Subs	urface L	_eak	N/A	Lu	ubricate & C	lean Noz	zle Thre	ads	N/A		Operate	ed/Exer	cised		N/A
Hydrant	Above	Grade	Leak	N/A		Lubricate &	Clean Ca	p Threa	ds	N/A		Numb	er of Tu	ırns		N/A
Open	Subs	urface L	_eak	N/A	W	Vater Remov	ed (if no	n-drain	ing)	N/A		Open	Directi	on		
Comments:									Auxiliary Valve Lo	cation:						

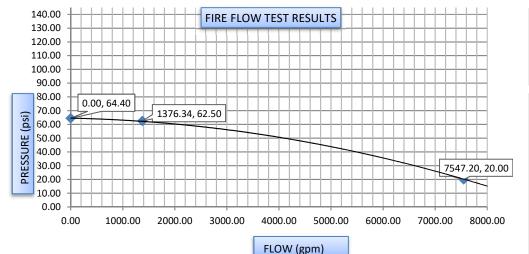
**FLUSHING** \*If hydrants are being flow tested, inspections and flushing are completed prior to testing

Hydrant Operated	Clear Flow Obtained	Cl2 Residual	Time Flushed	Flow	Total Flow	Dechlorinated
Yes - Easily Operated	Yes	N/A	5 minutes	1376 gal	6882 gal	Yes

STATIC AFTER FLOW TEST WAS PERFORMED 64.32 PSI Comments:

**FLOW TESTING** \*Flow testing results may be from previous year(s). Note date & time

		Test Hydrant								
ID	Flow Device Used	Size	Coefficient	Time Flushed	Flow	Total Flow	Pitot	ID	Static	Residual
16600	Pollard Diffuser	2.5"	0.832	5.0 minutes	776 gal	3878 gal	25 psi	7517	64.40	62.50
16600	Pollard Diffuser	2.5"	0.832	5.0 minutes	601 gal	3004 gal	15 psi			

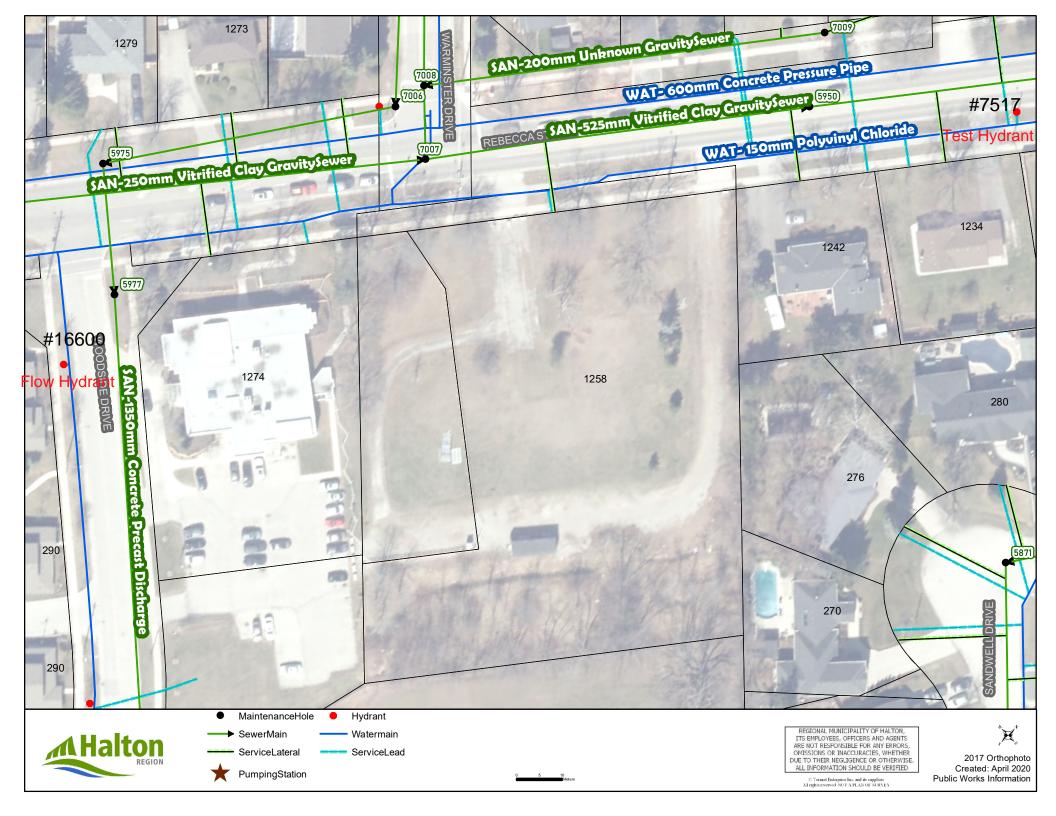


<b>Calculated Results</b>									
Calculated Flow @ 20 psi	7547 gpm								
Calculated Flow @ 0 psi	9226 gpm								
Pressure Drop	2.95%								

Time: 10:17 AM

Date: 26-Oct-22

Comments:





### **Multi Use Water Demand Table**

Date: January 2023 Project No.: 2480 Prepared By: M.L.M.

WATER CONNECTION	
Connection Point	Rebecca Street
Residential Water Usage Rate	0.275 m <sup>3</sup> /ca/day
Single Family Population	12 persons
Semi-detached Population	44 persons
Hydrant flow test	October 26, 2022 by OCWA
Hydrant flow test location	Hydrants # 7517 (Test) and 16600 (Flow)

	Pi	resure		Flow	Time
	(kPa)	(psi)	(L/s)	(gpm)	Tillio
Minimum water pressure	430.9	62.5	86.8	1376	5 min
Maximum water pressure	444.0	64.4	0	0	0 min

			WATER DEMA	NDS		
N	o. Demand Type	Residential Peaking Factor	Single Family Demand (L/s)	Residential Peaking Factor	Semi-Detached Demand (L/s)	Total Demand (L/s)
1	Average Day	1.00	0.04	1.00	0.14	0.18
2	2 Maximum Day	2.25	0.09	2.25	0.32	0.40
3	Maximum Hour	4.00	0.15	4.00	0.56	0.71
5	Fire flow (see <i>Note 1</i> )	-	67 (4,000 L/min)	-	100 (6,000 L/min)	100.0 (6,000 L/min)
6	Maximum day plus fire flow	_	-	-	-	100.4 (6,024 L/min)

No.	WATER PRESSURES						
	Demand Type	Preferred Pressure Range	Required Pressure Range	Available Pressure			
		(kPa)	(kPa)	(kPa)			
1	Average Day	350 - 550	275 - 700	444.0			
2	Maximum Day	350 - 550	275 - 700	444.0			
3	Maximum Hour	350 - 550	275 - 700	444.0			
5	Fire flow	-	> 140	427.0			
6	Maximum day plus fire flow	-	> 140	426.9			

#### Notes

1. Single Family fire demand is based on FUS Note J - "Short Method" for detached one family dwellings. Semi-Detached fire demand calculations are attached.



30 Centurian Drive, Suite 100 Markham, Ontario L3R 8B8 Phone 905 475 1900 Fax 905 475 8335



### FIRE FLOW REQUIREMENT

PROJECT INFORMATION

Project No. 2480 Date: January 2023 Designed by: M.L.M.

Address:	1258 Rebecca Street		N		: Semi-Detached homes Fire area is based on <b>Buildings 5-7</b> , wood		
	Town of Oakville						
				frame stru	ctures separated	by less than 3 m.	
BASE FLOW CAL	CULATION					FLOW (L/min)	
			2				
A= Effective area			335 m <sup>2</sup>				
C= Wood frame			1.5				
F= Required fire flow			6,040 L/min				
"F" Rounded to nearest 1,000			6,000 L/mir			6,000	
FLOW 'F' ADJUS	TMENTS			CREDITS	CHARGES	FLOW (L/min)	
Occupancy Adjustments (F')		%					
Limited combustible		-15%	-900	-900		5,100	
Exposure Adjustments (E )							
Exposure Aujusti		Chargo					
Exposure N	Sep. (m) 30	Charge 10%					
E	15	15%					
S	70	0%					
W	32	5%					
E = Total Exposure Charge		30%	1,530		1530	6,630	
Sprinkler Adjusm	nents (S)						
Sprinklered as pe		No	0			6,630	
Standard Water		Yes	-510	-510		6,120	
Fully supervised water supply		No	0	310		6,120	
. any supervised	supply	110	Ŭ			0,120	
REQUIRED FLOV	VS (F"=F+E+S)		(L/mi	n)		6,000	

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