

FUNCTIONAL SERVICING REPORT

Water, Sanitary, and Stormwater Management

ASSISTED CARE/LIVING FACILITY

2135 DUNDAS STREET WEST TOWN OF OAKVILLE

OUR FILE: 1614

PREPARED FOR ASC (OAKVILLE) FACILITY LIMITED PARTNERSHIP

DECEMBER 18, 2023

REVISION HISTORY

DATE	REVISION	SUBMISSION
December 18, 2023	4	Issued for Rezoning Application
February, 7 2019	3	Submitted under separate cover
August 17, 2018	2	Submitted under separate cover
November 13, 2017	1	Submitted under separate cover

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1.0 INTRODUCTION

This report was originally prepared in support of the rezoning and site plan applications for the development of an assisted living/care facility located at 2135 Dundas Street West. The development consisted of approximately 21,031 m² combination Assisted Living/Care Units with the building height ranging between four and six floors; there were 98 Assisted Living units and 84 Care units.

This report has been updated to support a rezoning application to permit the conversion of 33 care units into seniors' apartments. Changes to the approved report are denoted in italics below.

Where appropriate, sections have been updated to indicate that certain components have been constructed. This does not constitute a certification or validation of as-constructed components but is provided as information only.

1.1 **Project Description**

Trafalgar Engineering Ltd. has been retained by All Seniors Care Acquisitions to prepare a Functional Servicing Report in support of the Site Plan Application for the property located at 2135 Dundas Street West in Oakville. This report should be read in conjunction with Trafalgar's Site Servicing Plan *and* Grading Plan, and Architectural and Landscape plans *(by others)* prepared for the development.

The subject site is located on the north-west corner of Dundas Street West and Hospital Gate in Oakville. The site is bounded by Dundas Street West on the south, Hospital Gate on the east, a stormwater management pond (Taplow Pond) to the north and vacant lands to the west. The site has historically been referred to as the Mitic Property.

The 1.226 ha site currently contains many buildings including residential dwelling, garages and sheds.

The proposed development for the subject site is for a 21,031 m2 combination Assisted Living/Care Units with the height ranging between four and six floors. There will be 98 Assisted Living units, *51* Care Units, *and 33 seniors' apartments (dwelling units)*. The Assisted Living units will include both 1 bedroom and 2 bedroom units. Vehicle access will be from Hospital Gate to an internal courtyard and a drop-off at the building. Some surface parking will be provided in this area, but the majority of the parking will be underground beneath the building. Access to the building will be provided from the internal driveway at the main floor level and to basement level from the Dundas Street West frontage. Landscape areas are provided around the site with a significant area provided in the western part of the site.

1.2 Previous Studies, Reports and Documents

The following studies/reports/documents were reviewed in the preparation of this report.

- North Oakville Creeks Sub-watershed Study, Town of Oakville, August 2006 (NOCSS)
- North Oakville Creeks Sub-watershed Study Addendum, Town of Oakville, September 5, 2007 (NOCSS Amendment)
- North Oakville Environmental Implementation Report and Functional Servicing Study Terms of Reference, Town of Oakville, August 2, 2007 (Terms of Reference)
- Stormwater Management Planning and Guidelines Manual, Ministry of Environment, March 2003 (MOE Manual)
- Development Engineering Procedures & Guidelines Manual, Town of Oakville, 2016 (Town's Manual)
- Water and Wastewater Linear Design Manual, Regional Municipality of Halton, July 2017 (Region's Manual)
- Sixteen Hollow Employment Area Area Servicing Plan, WalterFedy, January 31, 2014 (revised June 26, 2014) (ASP)
- Stormwater Management Report, EIR/FSS Update and HHS Pond Design Brief, May 9, 2012, WalterFedy (Hospital EIR/FSS)
- 2135 Dundas Street, Oakville Mitic Property Site, Stormwater Management Assessment, WalterFedy, February 3, 2017. (WalterFedy Letter)
- Stormwater Management Report All Senior's Care Acquisition Ltd.-2135 Dundas Street West Oakville, Walterfedy, November 14, 2018 (SWM Report)



2.0 SANITARY DRAINAGE

The below text is provided for context but is out-of-date. The sewer connection to Whistling Springs has been constructed and as-built records are provided in Appendix 'D'.

In the Area Servicing Plan (ASP) prepared by WalterFedy, they had recommended that the subject lands be serviced from the existing 200mm diameter sanitary sewer located On Whistling Springs Crescent, located immediately south of Dundas Street West.

Connection to the existing sewer will require jacking and boring the sewer across Dundas Street West to Whistling Springs, and construction of the sewer to the connection manhole.

A review of record drawings in combination with updated topography indicates that the outlet originally proposed will be in conflict with the existing 1200mm diameter water and storm sewers recently constructed along Dundas Street West. As an alternative, the crossing route has been moved to the east to avoid conflict with the storm sewer. The proposed route may require the relocation of the traffic signal controller for the Dundas Street West/Hospital Gate intersection. This will result in a section of the sewer being constructed along the Whistling Springs Crescent right-of-way. The proposed sanitary sewer route is shown on drawing 1614-S2.

2.1 Estimated Sewage Flows

Since Region of Halton wastewater criteria is based on a unit flow rate per area, there is no change in anticipated discharge with the revised unit mix. The below calculation remains valid.

Sewage flows were estimated using the Region's Manual and assuming the development is similar to a 6 Storey Apartment with equivalent population density of 135per/ha. The resulting flows are summarized below.

•	Average Daily Dry Weather Flow	= 0.5 L/s
•	Peaking Factor	= 4.18
•	Infiltration Allowance	= 0.4 L/s
•	Design Flow	= 2.6 L/s

2.2 Sanitary Sewer Lateral Sizing

The proposed connection sewer is a 200mm diameter sewer at 1.0% with a capacity of 34 L/s, well in excess of the required capacity. *The sewer connection has been constructed and as-built records are provided in Appendix 'D'*.

2.3 Downstream Capacity

The downstream sanitary sewer system was evaluated and no capacity issues were noted. The system was evaluated to a point where the contributing flows from the site were less than 10% of the total flows.

3.0 WATER SUPPLY

There is an existing 400mm watermain located along Hospital Gate immediately adjacent to the site. There is an existing 1200mm diameter trunk watermain located along Dundas Street West.

Fire flow testing was undertaken by Jackson Waterworks on October 4, 2017 on the existing hydrant on Hospital Gate, immediately adjacent to the site. This testing indicated a static water pressure of 42psi and theoretical fire flow of 3355 USGPM (12,700 L/min.).

3.1 Estimated Water Demands

Water demands were estimated using the Region's Manual and assuming the development is similar to a 6 Storey Apartment with equivalent population density of 135per/ha. The resulting flows are summarized below.

Average Daily Demand	= 32 L/min
Maximum Daily Demand	= 71 L/min
Maximum Hourly Flow	= 126 L/min
Fire Flow	= 6,000 L/min
Maximum Daily Plus Fire Flow	= 6.072 L/min

Based on the hydrant flow test, there is sufficient pressure and flow to provide the required demands. It is noted that the existing static pressures are relatively low and booster pumps and fire flow pumps may be required. The Region of Halton is currently undertaking a study to realign the pressure zones that may raise the static pressure at the site.

Connection to the building for both fire and domestic water will be to the existing 400mm watermain along Hospital Gate Road. *The water connections have been constructed.*

4.0 STORM DRAINAGE

There are no proposed changes to the stormwater management design and it is understood that a revised stormwater management report is not required for this application. However, the original content from the approved report is provided below for completeness.

4.1 Background

NOCSS indicates that the subject site is split between Taplow Creek to the east and McCraney Creek to the west. The Hospital EIR/FSS proposed to divert the eastern part of the subject site to McCraney Creek as part of a land swap.

In the WalterFedy letter it was outlined that the Taplow Pond constructed immediately north of the subject site has sufficient capacity to allow a significant portion of the subject lands to be conveyed to the Taplow Pond. Final details of this diversion are being addressed by WalterFedy and are outlined in the WalterFedy SWM Report.

This report only addresses the design of the site's specific drainage.

4.2 Existing Infrastructure

There is an existing 825mm diameter storm sewer along Hospital Gate adjacent to the subject site. This sewer is the primary outlet pipe from Taplow Pond located north of the subject site. The sewer also received uncontrolled flows from a roadside catch basin along Hospital Gate.

There is a storm sewer system on the south side of Dundas Street. The sewer system collects runoff from Dundas Street West, west of the Hospital Gate intersection. Attached to this system is as catch

basin located on the northern part of the Dundas Street West right-of-way. The catch basin collects drainage from part of the existing site.

4.3 Proposed Drainage

Development of the subject site will be split into three different drainage areas.

- Area 1 is the area between the proposed building and Hospital Gate including the entry driveway. This area will sheet flow to Hospital Gate and will be collected in the sewer system along Hospital Gate.
- Area 2 is the areas between the proposed building and the Dundas Street West right-of-way. The western part of this area will sheet flow to Dundas Street West. The eastern area will be conveyed to the existing catch basin in this area.
- Area 3 is the balance of the site and includes the driveway, roof and landscape areas. Runoff from this area will be collected by a series of catch basins connected to a site storm sewer system. The storm sewer will outfall to the Taplow Pond located north of the site. The onsite storm sewer system has been designed to convey the Town of Oakville 5-yr design storm.

Roof drainage will need to be conveyed through internal piping and connected to the internal sewer system. The building's drainage system will need to be water tight to at least elevation 160.20m.

A trench drain will be installed at the bottom of the proposed down ramp to the underground garage and as series of the areas drains installed at the east side of the building. Runoff from these areas will need to be pumped to the internal site's drainage system.

Site flows were calculated using the Rational Method and the Town of Oakville IDF curves. The following table provides summary of the flows from each area.

				5-year	100-year
	Area	Impervious	Runoff	Flow	Flow
Drainage Area	ha	Percentage	Coefficient	L/s	m³/s
Hospital Gate (Area 1)	0.0871	58	0.63	17	38
Dundas Street (Area 2)	0.1617	52	0.58	30	65
Building (Area 3A)	0.4916	91	0.84	131	288
Grounds (Area 3B)	0.4594	63	0.66	96	211
Drains to Pond (Area 3C)	0.0269	0	0.25	2	5
Total to Taplow Pond	0.9779	75	0.74	230	505
Site Total	1.2267	71	0.71	276	607

Summary of Site Flows

 $C_{100} = 1.25 \text{xC}$

To protect the site in the event of an extreme rainfall event or blockage of sewer system, an overland flow route has been provided to the Taplow Pond. A local high point has been provided in the entry driveway to prevent site flows from spilling to Hospital Gate. A second local high point has been established at the top of the down ramp to ensure flow does not spill to the underground garage.

4.4 Flows to Dundas Street

The predevelopment area draining to Dundas Street West the Regional Sewer located on Dundas Street West is 0.262 Ha with an estimate composite runoff coefficient of C=0.39. The calculated pre-development 5-year flow is 33 l/s. This compares to post-development 5-year flow of 30 l/s.

The resulting flow to Dundas Street West is less in the post-development condition.

4.5 LID's

Section 3.3 of the WalterFedy SWM Report discusses in detail the LID restraints and requirements. Section 3.4.3 of the WaterFedy SWM Report concludes by indicating that a 103m³ infiltration gallery with a 712m² foot print is required to meet the water balance requirements for the site.

The site has been designed with the required storage volume and foot print distributed between two infiltration beds.

The infiltration bed on the north side of the building has been sized with an area of 562m². Flows from the roof will be directed to the infiltration bed. Manhole 5 has been designed to direct flows to the infiltration bed and by-pass flows to the by-pass sewer at MH 4 in the event of a infiltration bed failure or an extreme rainfall event. Two lines of Cultec Recharger 330XLHD will be utilized distribute the flows through the infiltration bed. Two parallel line of 150mm diameter will assist in the distribution flow flows through the bed.

A smaller infiltration bed of 158 m² will be located on the west side of the building. This area will receive runoff from the landscape area located on the western side of the building. The western bed will be linked to north bed through CBMH 8 resulting in two bed acting as one facility. The western bed will have two 150mm diameter perforated pipes running through the bed to distribute the runoff. A by-pass sewer between CBMH 7 and CBMH 8 will be installed to provide conveyance in the event the failure of the infiltration system or in the event of an extreme rainfall event.

The outlet pipe from CBMH 8 will control the outflows from the infiltration bed. The outlet has been set at elevation 157.87 which is 0.47m above the bottom of the bed and results in storage of 158 m³. The pipe invert is also 0.30 m above the outlet from MH 3 to prevent from backwashing from parking area to the infiltration bed.

4.6 Water Quality

As outlined in the WalterFedy SWM Report the outlet from the site to the Taplow Pond will by-pass the settling basin. To account for the parking lot area will need to be pre-treated prior to discharging to the Taplow SWM Pond. The WaterFedy SWM Report indicated that a pre-treatment removing 50% of the TSP would be appropriate for the site with the stormwater management pond provide settling the balance of 30% of the TSP. Collectively together the Enhanced (Level 1) water quality would be achieved.

Based on an area of 0.494 Ha and impervious percentage of 63% a Stormceptor Model EF6 or equivalent is required.

4.7 Storm Servicing

All stormwater management facilities and private storm sewers have been constructed. Final grading and area drains are in-progress.

5.0 SUMMARY

- 1. A sanitary connection *is* provided to the existing sewer on Whistling Springs Drive as generally outlined in the ASP *and per the approved FSR prepared by this office*.
- 2. Water connections for both fire and domestic *have been constructed* to the existing 400mm watermain located on Hospital Gate. Relatively low pressure may require booster pumps and fire pumps to be installed within the building.
- 3. The storm sewer outlet for the subject property *is to* Taplow Pond. Fringe areas around the site will flow to the systems on the adjacent roadways.
- 4. To address the water balance issues an infiltration bed in excess of required 712 m² bed area and 103 m3 volume *has been* installed.
- 5. Enhanced (Level 1) water quality *is* provided through a combination of a OGS removing a minimum of 50% of the TSP and the stormwater management pond removing 30% TSP.
- 6. Flows to Dundas Street West will be maintained at the pre-development levels.

This report was originally sealed by Stephen L. Potter, P.Eng.

This report has been prepared only to support the rezoning application to permit the proposed change in unit mix (conversion of 33 care units to seniors' apartments).

PREPARED BY TRAFALGAR ENGINEERING LTD.

J.T. Nelson, P.Eng. Principal



APPENDIX 'A'

TRAFALGAR ENGINEERING LTD.

ESTIMATED SANITARY FLOW

Project:	2135 Dundas Street W. Oak	ville			P	roject No.:	1614
Desc:	Retiremet Home				Pre	epared By:	S.P
					Cł	necked By:	0
Resident	tial						
			Population	Eq.	Per Cap.	Average Da	aily Dry
			Density	Population	Demand	Weathe	er Flow
Land Use	e / Occupancy Type	Area (ha)	(pers/ha)	(cap.)	(L/cap. Day)		(L/s)
6 Storey	Apartment Building	1.23	135	166	275		0.5
TOTAL		1		166			0.5
Residenti	al Peaking Factor:	4.18					
Site Area	: Poto:	1.23 (f	(a, ba)				
Infiltration	Allowance	0.280 (1	/s)				
		0.4 (1					
Total Dry	Weather Flow:	0.5 (l	_/s)				
Design F	low:	2.6 (l	_/s)				

P:\1614 All Seniors\Calculations\[Water and Sanitary Demands .xlsx]WATER

VER 2.0

TRAFALGAR ENGINEERING LTD. Consulting Engineers

SANITARY SEWER DESIGN SHEET (Metric)

Regional Municipality of Halton

															PROPOSED SEWER PIPE					РЕ			
STREET	FROM MH	TO MH	Length in metres	Tributa Res	ry Area (I Comm	Hectares) Total	Population (iet y	Pop Res	ulation Trib Comm.	outary Total	Average Q m ³ /s Increment	Average Q m³/s Total	K Peaking Factor	MAX. Q (m ³ /s)	(m ³ /s)	MAX. FLOW (m ³ /s)	Size (mm)	Slope %	Capacity (m ³ /s)	Velocity Full	(m/s) Actual	Туре	% Cap
Site (Develop Street)	100.4	200.4	100.00	1.000	0.00	1.00	105	1//	0	1//	0.00052	0.00052	4 10	0.0022	0.0004	0.000	200	0.50	0.020	0.07	0.71	DVC	0
Site (Dundas Street) Whistling Spring Cr	100A 200A	200A 64	100.00 84.00	0.29	0.00	1.23	135	100 30	0	205	0.00053	0.00055	4.18	0.0022	0.0004	0.0026	200	0.50	0.050	0.96	0.01	PVC PVC	<u>8</u>
Whistling Spring Cr.	6A	5A	10.50	0.08	0.00	1.60	135	3) 11	0	205	0.00003	0.00069	4.14	0.0027	0.0004	0.0031	200	0.95	0.030	1.30	0.86	PVC	8
Whistling Spring Cr.	5A	4 A	73.98	0.59	0.00	2.19	135	80	0	295	0.00025	0.00094	4.08	0.0038	0.0006	0.0045	200	0.90	0.040	1.29	0.87	PVC	11
								=0			0.0001.6	0.00017	1.21		0.0001					1.05		Price	
Tovell Drive	20A	7A	56.60	0.37	0.00	0.37	135	50	0	50 59	0.00016	0.00016	4.31	0.0007	0.0001	0.0008	150	1.25	0.022	1.25	0.66	PVC DVC	4
Tovell Drive	/A	4A	35.20	0.00	0.00	0.45	155	0	U	50	0.00005	0.00018	4.30	0.0008	0.0001	0.0009	200	0.50	0.050	0.90	0.49	PVC	3
Whistling Spring Cr.	4A	3A	81.80	0.67	0.00	3.29	55	37	0	390	0.00012	0.00124	4.03	0.0050	0.0009	0.0059	200	0.70	0.036	1.14	0.87	PVC	17
			00.44								0.00012	0.00012	4.00	0.0007					0.020	0.04		Price	
Youngstown Gate	12A 11A	11A 24	80.46	0.76	0.00	0.76	55	42	0	42	0.00013	0.00013	4.33	0.0006	0.0002	0.0008	200	0.50	0.030	0.96	0.42	PVC DVC	3
Youngstown Gate	11A	ЗА	20.70	0.00	0.00	0.70	22	U	U	42	0.00000	0.00015	4.55	0.0000	0.0002	0.0008	200	1.50	0.052	1.00	0.07	PVC	
Whistling Spring Cr.	3A	2A	83.69	0.41	0.00	4.46	55	23	0	454	0.00007	0.00145	4.00	0.0058	0.0013	0.0071	200	0.60	0.033	1.05	0.85	PVC	21
Whistling Spring Cr.	2A	1A	62.69	0.32	0.00	4.78	55	18	0	472	0.00006	0.00150	3.99	0.0060	0.0014	0.0074	200	0.55	0.032	1.01	0.85	PVC	23
Whistling Spring Cr.	1A	300A	17.49	0.29	0.00	5.07	55	16	0	488	0.00005	0.00155	3.98	0.0062	0.0014	0.0076	200	0.50	0.030	0.96	0.81	PVC	25
Dine Clen Deed	114	200 4	26.00	0.21	0.00	0.21	55	17	•	17	0.00005	0.00005	4 20	0.0002	0.0001	0.0002	150	1 20	0.022	1 22	0.40	DVC	1
Pine Gien Road	IIA	300A	30.00	0.31	0.00	0.31	55	1/	U	1/	0.00005	0.00005	4.39	0.0002	0.0001	0.0003	150	1.38	0.023	1.32	0.49	PVC	1
Pine Glen Road	300A	400A	83.00	0.43	0.00	5.81	55	24	0	529	0.00008	0.00168	3.96	0.0067	0.0017	0.0083	250	0.48	0.054	1.09	0.82	PVC	16
Willbayan Trail	10.4	94	18.82	0.32	0.00	0.32	55	18	0	18	0.00006	0.00006	1 30	0.0002	0.0001	0.0003	200	2 50	0.067	2 15	0.57	PVC	1
Willhaven Trail	9A	9A 8A	35 11	0.32	0.00	0.52	55	10	0	33	0.00000	0.00000	4 35	0.0002	0.0001	0.0003	200	1.50	0.007	2.13 1.66	0.57	PVC	1
Willhaven Trail	8A	7A	11.03	0.14	0.00	0.74	55	8	0	41	0.00002	0.00011	4.33	0.0006	0.0002	0.0008	200	1.50	0.052	1.66	0.66	PVC	1
Willhaven Trail	7A	7Ax	42.62	0.29	0.00	1.03	55	16	0	57	0.00005	0.00018	4.30	0.0008	0.0003	0.0011	200	1.00	0.043	1.36	0.65	PVC	3
Willhaven Trail	7Ax	400A	9.79	0.15	0.00	1.18	55	8	0	65	0.00003	0.00021	4.29	0.0009	0.0003	0.0012	200	0.50	0.030	0.96	0.51	PVC	4
Pine Clen Road	400 4	500 A	82.50	0.35	0.00	7 34	55	10	0	613	0.00006	0.00195	3 03	0.0077	0.0021	0.0098	250	0.57	0.058	1 10	0.91	PVC	17
			02.00	0100	0.00		~~					0.001/2			0.0021	0.0070			0.020				
Whistling Spring Cr.	23A	22A	87.80	0.36	0.00	0.36	135	49	0	49	0.00015	0.00015	4.32	0.0007	0.0001	0.0008	150	1.43	0.024	1.34	0.64	PVC	3
Whistling Spring Cr.	22A	21A	6.70	0.06	0.00	0.42	135	8	0	57	0.00003	0.00018	4.30	0.0008	0.0001	0.0009	200	1.12	0.045	1.44	0.64	PVC	2
Whistling Spring Cr.	21A	16A	52.90	0.27	0.00	0.69	135	36	0	93 102	0.00012	0.00030	4.25	0.0013	0.0002	0.0015	200	0.82	0.039	1.23	0.61	PVC	4
whisting Spring Cr.	10A	15A	18.90	0.07	0.00	0.70	135	<u> </u>	U	105	0.00005	0.00033	4.24	0.0014	0.0002	0.0010	200	1.00	0.045	1.30	0.07	FVC	4
Tovell Drive	20A	15A	74.20	0.47	0.00	0.47	135	63	0	63	0.00020	0.00020	4.29	0.0009	0.0001	0.0010	200	0.71	0.036	1.14	0.53	PVC	3
																						[]	
Whistling Spring Cr.	15A	14A	66.45	0.58	0.00	1.81	55	32	0	198	0.00010	0.00063	4.15	0.0026	0.0005	0.0031	200	0.75	0.037	1.18	0.75	PVC	8
Whistling Spring Cr.	14A	13A	85.36	0.90	0.00	2.71	55	50	0	247	0.00016	0.00079	4.11	0.0032	0.0008	0.0040	200	2.00	0.060	1.92	1.13	PVC PVC	7
winsuing Spring Cr.	13A	500A	27.03	0.25	0.00	2.90	22	14	U	201	0.00004	0.00083	4.10	0.0034	0.0008	0.0043	200	0.50	0.030	0.90	0.69	PVC	
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Project Name: All Seniors Project No.: 1614 Date: Oct. 26, 2017

TRAFALGAR ENGINEERING LTD. Consulting Engineers

SANITARY SEWER DESIGN SHEET (Metric)

Regional Municipality of Halton

																		PF	OPOSED SEV	WER		PI	PE
							U								5								
							lati ity						r B		rati								
							nde				Average Q	Average Q	aki		Elt	MAX.							
STREET	FROM	ТО	Length in	Tributa	ary Area (I	lectares)	P ₀	Рор	ulation Trib	outary	m ³ /s	m ³ /s	Fa	MAX. Q	E	FLOW	Size	Slope	Capacity	Velocity	(m/s)	_	
	MH	MH	metres	Res	Comm	Total	(per ha.)	Res	Comm.	Total	Increment	Total	М	(m ³ /s)	(m ³ /s)	(m ³ /s)	(mm)	%	(m ³ /s)	Full	Actual	Туре	% Cap
Shadow Court	41.4	40.4	13.07	0.21	0.00	0.21	135	28	0	28	0.0000	0.0000	1 36	0.0004	0.0001	0.0005	200	2.00	0.060	1.02	0.50	PVC	1
Shadow Court	41A	39A	35 50	0.21	0.00	0.21	135	26	0	54	0.00009	0.00009	4.30	0.0004	0.0001	0.0003	200	1 50	0.052	1.52	0.33	PVC	2
Shadow Court	39A	38A	54.12	0.26	0.00	0.66	135	35	0	89	0.00011	0.00028	4.26	0.0012	0.0001	0.0014	200	0.50	0.030	0.96	0.52	PVC	5
Shadow Court	38A	37A	12.67	0.00	0.00	0.66	135	0	0	89	0.00000	0.00028	4.26	0.0012	0.0002	0.0014	200	0.50	0.030	0.96	0.52	PVC	5
Shadow Court	37A	36A	51.76	0.40	0.00	1.06	135	54	0	143	0.00017	0.00046	4.20	0.0019	0.0003	0.0022	200	0.50	0.030	0.96	0.58	PVC	7
Shadow Court	36A	29A	20.00	0.09	0.00	1.15	135	12	0	155	0.00004	0.00049	4.19	0.0021	0.0003	0.0024	200	0.50	0.030	0.96	0.58	PVC	8
St	25.4	25.4	20.50	0.16	0.00	0.16	125			22	0.00007	0.00007	4 30	0.0002	0.0000	0.0002	150	1.02	0.025	1.52	0.52	DVC	1
Stone Gien Cr.	35AX	35A 244	30.50	0.10	0.00	0.10	135	19	0	22	0.00007	0.00007	4.38	0.0003	0.0000	0.0003	150	1.83	0.027	1.52	0.52	PVC	1
Stone Glen Cr.	31A	34A 33A	13 50	0.15	0.00	0.29	135	18	0		0.00008	0.00012	4.34	0.0005	0.0001	0.0006	200	1.0/	0.050	1.60	0.04	PVC PVC	1
Stone Glen Cr.	334	32A	62.00	0.07	0.00	0.30	135	53	0	101	0.00003	0.00013	4.32	0.0007	0.0001	0.0008	200	0.77	0.037	1.05	0.00	PVC	4
Stone Glen Cr.	32A	31A	39.00	0.34	0.00	1.09	135	46	0	147	0.00017	0.00047	4.19	0.0020	0.0002	0.0010	200	0.61	0.033	1.06	0.64	PVC	7
Stone Glen Cr.	31A	30A	17.50	0.07	0.00	1.16	135	9	0	157	0.00003	0.00050	4.18	0.0021	0.0003	0.0024	200	0.45	0.029	0.91	0.58	PVC	8
Stone Glen Cr.	30A	29A	74.72	0.55	0.00	1.71	135	74	0	231	0.00024	0.00073	4.12	0.0030	0.0005	0.0035	200	0.56	0.032	1.02	0.69	PVC	11
														ļ									
Stone Glen Cr.	29A	28A	19.91	0.00	0.00	2.86	135	0	0	386	0.00000	0.00123	4.03	0.0050	0.0008	0.0058	200	0.50	0.030	0.96	0.76	PVC	19
Stone Glen Cr.	28A	27A	37.18	0.12	0.00	2.98	135	16	0	402	0.00005	0.00128	4.02	0.0051	0.0009	0.0060	200	0.50	0.030	0.96	0.76	PVC	20
Stone Gien Cr.	2/A	15A	79.50	0.10	0.00	3.14	55	у	U	411	0.00003	0.00131	4.02	0.0055	0.0009	0.0062	200	0.45	0.029	0.91	0.74	PVC	22
Stone Glen Cr.	23A	22A	21.00	0.16	0.00	0.16	55	9	0	9	0.00003	0.00003	4.42	0.0001	0.0000	0.0002	150	0.40	0.013	0.71	0.26	PVC	1
Stone Glen Cr.	22A	21A	69.50	0.69	0.00	0.85	55	38	0	47	0.00012	0.00015	4.32	0.0006	0.0002	0.0009	200	0.45	0.029	0.91	0.41	PVC	3
Stone Glen Cr.	21A	15A	30.83	0.18	0.00	1.03	55	10	0	57	0.00003	0.00018	4.30	0.0008	0.0003	0.0011	200	0.40	0.027	0.86	0.45	PVC	4
			Ļ	Ļ		ļ									ļ					ļļ			Ļ
Stone Glen Ext Ph.8	12A	13A	90.00	0.70	0.00	0.70	135	95 52	0	95	0.00030	0.00030	4.25	0.0013	0.0002	0.0015	200	1.00	0.043	1.36	0.69	PVC	3
Stone Glen Ext Ph.8	13A 14A	14A	83.00	0.39	0.00	1.09	135	55	0	147	0.00017	0.00047	4.19	0.0020	0.0003	0.0023	200	0.43	0.028	0.89	0.55	PVC DVC	8
Stolle Glell Ext F 11.0	14A	15A	30.50	0.13	0.00	1.22	135	10	U	105	0.00000	0.00052	4.10	0.0022	0.0003	0.0025	200	0.41	0.027	0.07	0.57	rve	, ,
Pine Glen Road	15A	10A	85.00	0.18	0.00	5.57	55	10	0	642	0.00003	0.00204	3.92	0.0080	0.0016	0.0096	250	0.52	0.056	1.14	0.85	PVC	17
				<u> </u>		<u> </u>								<u>.</u>		<u> </u>		<u> </u>		<u> </u>		<u> </u>	[
Stone Glen Cr.	26A	25A	37.00	0.28	0.00	0.28	135	38	0	38	0.00012	0.00012	4.34	0.0005	0.0001	0.0006	150	2.00	0.028	1.58	0.65	PVC	2
Stone Clen Cr	244	254	32.00	0.20	0.00	0.20	135	27	0	27	0 00009	0 00009	4 36	0.0004	0.0001	0 0004	150	2 21	0.029	1.67	0.65	PVC	1
Stone Gren Cr.		2514	52.00	0.20	0.00	0.20	100				0.00009	0.00009		0.0004	0.0001	0.0004	150	2.21	0.027	1.07	0.05	1,10	t
Barnboard Hollow	25A	19A	88.50	0.60	0.00	1.08	135	81	0	146	0.00026	0.00046	4.20	0.0019	0.0003	0.0023	200	0.38	0.026	0.84	0.54	PVC	9
				0.52	0.00	0.52	125	70		70	0.00022												
Future Condo Weedsteel: Treil				0.52	0.00	0.52	135	70	0	70 91	0.00022				ļ	4						ļ	<u>.</u>
Woodstock Trail				0.00	0.00	1.20	135	11 81	0	162	0.00003			+	******	4		÷		••••••••			•
Woodstock Trail	Plug	19A	7.50	0.00	0.00	1.33	135	18	0	180	0.00020	0.00057	4.16	0.0024	0.0004	0.0028	200	1.00	0.043	1.36	0.78	PVC	6
			1	1			1	-						1	1	1	[1		[1	
Woodstock Trail	19A	18A	72.00	0.43	0.00	2.84	135	58	0	383	0.00018	0.00122	4.03	0.0049	0.0008	0.0057	200	0.52	0.031	0.98	0.76	PVC	19
Woodstock Trail	18A	17A	50.00	0.48	0.00	3.32	55	26	0	410	0.00008	0.00130	4.02	0.0052	0.0009	0.0062	200	0.92	0.041	1.30	0.95	PVC	15
Woodstock Trail	17A	10A	71.00	0.51	0.00	3.83	55	28	0	438	0.00009	0.00139	4.00	0.0056	0.0011	0.0067	200	0.83	0.039	1.24	0.98	PVC	17
Woodstock Ext Ph.8	16A	17A	59.00	0.37	0.00	0.37	135	50	0	50	0.00016	0.00016	4.31	0.0007	0.0001	0.0008	200	1.00	0.043	1.36	0.57	PVC	2
Woodstock Ext Ph.8	17A	18A	83.00	0.63	0.00	1.00	135	85	0	135	0.00027	0.00043	4.21	0.0018	0.0003	0.0021	200	0.51	0.030	0.97	0.59	PVC	7
Woodstock Ext Ph.8	18A	19A	128.00	1.12	0.00	2.12	135	151	0	286	0.00048	0.00091	4.09	0.0037	0.0006	0.0043	200	0.52	0.031	0.98	0.71	PVC	14
Woodstock Ext Ph.8	19A	10A	34.50	0.18	0.00	2.30	135	24	0	311	0.00008	0.00099	4.07	0.0040	0.0007	0.0047	200	1.52	0.053	1.67	1.05	PVC	9
Pine Clen Road	10.4	500 4	83.00	0.17	0.00	11 97	55	0	0	1400	0.00003	0.00446	3 70	0.0165	0.003/	0.0100	250	0.49	0.054	1.00	1.02	PVC	37
i me Gien Kodu	IUA	JUUA	03.00	V.1 /	0.00	11.0/	33	7	v	1400	0.00003	0.00440	5.70	0.0105	0.0034	0.0177	400	v.40	0.034	1.09	1.04	110	51
	İ		1	1	1	1	1			1				<u> </u>	1	<u> </u>		1				<u> </u>	
Whistling Spring Ext	500A	15A	53.40	0.36	0.00	22.53	55	20	0	2294	0.00006	0.00730	3.54	0.0258	0.0064	0.0323	300	0.50	0.089	1.26	1.18	PVC	36
Whistling Spring Ext	15A	16A	113.00	0.95	0.00	23.48	55	52	0	2346	0.00017	0.00747	3.53	0.0264	0.0067	0.0331	300	0.48	0.087	1.23	1.17	PVC	38
winsting Spring Ext	16A	I /A	21.20	0.27	0.00	25.75	55	15	U	2301	0.00005	0.00751	3.53	0.0265	0.0068	0.0333	300	0.50	0.089	1.20	1.18	PVC	
			+	÷	·	1	·				-	 		÷	1	·		÷		•			·

Project Name: All Seniors Project No.: 1614 Date: Oct. 27, 2017

APPENDIX 'B'



BASE HYDRANT PRESSURE (PSIG)

Telephone: Toll Free: E-mail: Website:

(905) 547-6770 (800)-734-5732 jww@bellnet.ca www.jacksonwaterworks.ca

FIRE HYDRANT FLOW TEST RESULTS



TEST HYDRANT FLOW (USGPM)

No. of Ports Open	Port Dia. (in)	Pitot Reading (psig) Pitot Conversion (usgprn) Conversion Factor = 0 Residual Pressure (psig)			Test Date	04 October 2017	
1	2.50	30	919	40		Test Time	08:15am
2	2.50	17/17	1384	38		Pipe Diameter (in)	12
THEORETICAL FLOW @ 20psi			3355		S	Static Pressure (psig)	42

	Site Information											
Site Name or Developer Name	Not Provided	Engineer: Trafalgar Engineering Ltd.										
Site Address/Municipality	2135 Dundas Street West, Oakville											
Location of Test Hydrant	Hospital Gate, 2nd North of Dundas Street West											
Location of Base Hydrant	Hospital Gate, 3rd North of Dundas Street West											
Comments	Testing has been completed in accordance with NFPA-291 guidelines when depending on hose nozzle internal design and installation profile. Refer to	ever and whenever possible and practical. Conversion factors for pitot tube readings have been used attached cover letter for additional information.										
Verified By	LLF Mark Schmidt											

TRAFALGAR ENGINEERING LTD.

ESTIMATED WATER DEMAND

Project: 2135 Dundas Street W. Oakville **Project No.:** 1614 Desc: Retiremet Home **Prepared By:** S.P **Checked By:** 0 **Occupancy Data** Peaking Factors **Demand Flow** Population Eq. Per Cap. Max. Hour Max. Daily Population Demand (L/cap. Max. Peak Density Average Daily Demand Demand Land Use / Occupancy Type Area ha (pers/ha) (cap.) Day) Demand (L/min) Hour Max. Daily (L/min) (L/min) 6 Storey Apartment 1.23 135.0 166 275 32 4.00 2.25 126 71 TOTAL 1 166 32 0 126 71 **Fire Flow** Average Daily Demand: 32 (L/min) Using Fire Underwriters Survey Methodology: Maximum Hourly Demand: 126 (L/min) Maximum Daily Demand: 71 (L/min) $F = 220C\sqrt{A}$ Max. Daily Plus Fire: 6071 (L/min) 1. An estimate of the fire flow is given by the formula Where: F = The required fire flow in litres per minute C = Coefficient related to the type of construction A = The total floor area in square metres (including all storeys but excluding basements at least 50% below grade) $|(m^2)|$ Area Note: For fire resistive buildings, consider the Type of Construction: Fire-Resistive Coefficient: 0.60 Total Floor Area: 5540 two largest adjoining floors plus 50% of F = 10000 (L/min) Adequately Protected Vertical Openings: Yes the remaining floors up to eight, when openings are inadequately protected. For 2. Adjust the value in No. 1 for occupancy surcharge/reduction adequately protected vertical openings Occupancy Contents: Limited Combustible Factor: -15% consider only the area of the largest floor plus 25% of each of the two immediately F = 8500 (L/min) adjoining floors 3. Adjust the value in No. 2 for sprinkler 4. Adjust the value in No. 2 for exposure Separation (m) Charge 0% NFPA 13 Sprinkler: Yes Reduction: 30% North 50 50 Standard Water Supply: Yes Reduction: 10% East 0% Fully Supervised: No Reduction: 0% South 50 0% West 15 15% Total Reduction: 40% **Total Charge:** 15% 3400 (L/min) Sprinkler Reduction: Exposure Charge: 1275 (L/min) 5. Estimated Fire Flow is value in No. 2 less Sprinkler Reduction plus Exposure Charge, rounded to the nearest 1000

F = 6000 (L/min)

P:\1614 All Seniors\Calculations\[Water and Sanitary Demands .xlsx]WATER

APPENDIX 'C'







STORM DRAINAGE AREA IN HECTARES **IMPERVIOUSNESS**

DRAINAGE AREA BOUNDARY

JN	SCALE	1:750	
JN	DATE	17/08/2018	

STORM SEWER DESIGN SHEET (Metric)

TRAFALGAR ENGINEERING LTD.

Consulting Engineers

Town of Oakville Design For 5 Year Storm Event

Project Name : All Seniors

Project No. : 1614 Date: 17-Dec-18 By: SP

			DRAINAGE AREA							PROPOSED SEWER							
LOCATION	FROM	то	Area A	Runoff Coeff. R	A x R	Accum. A x R	T of C	Intensity	Expected Flow	Length	Gradient	Pipe Size	Manning's Coeff.	Capacity	Velocity	Time of Flow	Cap.
	МН	MH	(ha)		(ha)	(ha)	(min)	(mm/hr)	(l/s)	(m)	(%age)	(mm)	(n)	(l/s)	(m/s)	(min)	(%age
West Side	CDM117	CDMU9	0.1222	0.66	0.087	0.097	10.00	114	10	42.0	2.00	250	0.012	00	1.74	0.41	21.5
west side	CBMH7 CBMH8	MH3	0.1322	0.00	0.087	0.087	10.00	114	28	3.0	2.00	300	0.013	143	1.74	0.41	18.9
Building	MH6	MH5	0.4916	0.84	0.413	0.413	10.00	114	131	41.0	1.50	375	0.013	225	1.97	0.35	58.3
	MH5	CULTEC				0.413	10.35	112	129	3.0	2.00	375	0.013	259	2.28	0.02	49.6
	MH5	MH4				0.413	10.35	112	129	3.0	2.00	375	0.013	259	2.28	0.02	49.6
Parking Lot	MH4	MH3	0.3272	0.66	0.216	0.629	10.37	112	196	59.0	1.10	425	0.013	269	1.83	0.54	72.9
Cultec Outlet	CULTEC	MH3	-						0	4.0	2.00	300	0.013	143	1.96	0.03	0.0
	MH3	MH2				0.716	10.90	109	217	6.0	1.00	450	0.013	298	1.82	0.06	72.7
	MH2 MH1	MHI				0.716	10.96	109	216	13.0	1.00	525	0.013	450	2.01	0.11	48.1
	WIIII	11.00				0.710	11.07	100	215	10.0	0.50	000	0.015	-7-7	1.50	0.11	47.5
												1					-

P:\1614 All Seniors\Calculations\[2018-12-12 Storm Design Sheet.xls]1614 internal sewers

All Seniors Infiltration Bed Summary

Required Bed Area Required Bed Vol.	712 m2 103 m3	Per WatlerFedy SWM Per WatlerFedy SWM	Report Report	
Bed Area Calculation				
Western Bed Area Northern Bed Area TOTAL AREA	158 m2 562 m2 720 m2			
Bed Volume Calcultation		Depth (mm) Void Ra	ntio Stor Vol.	age m3
Northern Bed Area	562 m2		-	
Cultec Bed Area	178 m2			54.44 from Cultec chart
Difference	384 m2	0.45	0.4	69.12
Western Bed	158 m2	0.45	0.4	28.44
Total Vol.				152 m3
				S. P.

P:\1614 All Seniors\Storm Water Management\[bedvol.xlsx]Sheet1

	Founder o Stori	f Plastic C nwater and <i>Since</i>	Chamber Techno Septic Solutions 1986	ology		1-800-4-CUI ustservice@culte	LTEC ec.com		
Prepared For:	Project Info	ormation:		Engineer:			Calculation	ns Performed B	y:
Name	All Seniors			S. Potter			Name		
Company Name	3000 Hospi	tal Gate		Trafalgar Engine	eering		Company N	lame	
Street Address	Oakville			Street Address			Street Addre	ess	
City	State		Zip	City			City		
State Zip				State	Zip		State		Zip
Phone	Date:	December	r 17, 2018	Phone			Phone		
Fax				Fax			Fax		
Email				Email			Email		
Input Given Parameters	Motrio					Hoight		Chamber Sp	ecifications
Soloct Model	Bocharge					Width		//5.0	
	Recharge					vvidtri		1321.00	matara
Stope Deresity	40.0%			111111111111111111111111111111111111111			ath	2.59	meters
Number of Header Systems	40.0%					Bare Chamber V	yun /olume	2.13	
Stope Dopth Above Chamber	150	mm			In	stalled Chambo	Volume	1.40	cu. meters
Stone Depth Below Chamber	150	mm		A REAL PROPERTY AND INCOMENTATION OF A REAL PROPERTY AND A REAL PR	113		volume	2.24	cu. meters
cience 2 optin 2010 in chambon	150			ALL STREET		mage for visual refe	erence only.May	v not reflect selected	l model.
Workable Bed Depth	1.50	meters				Bed Depth	1	1.41	meters
Max. Bed Width	3.45	meters				Bed Width	1	3.40	meters
Storage Volume Required	119.00	cu. meters				torage Volume F	Provided	119.48	cu. meters
Materials List									
Recharger 330XLHD Stormwater System	by CULTEC. Inc	2.							
Approx. Unit Count - not for construct	tion 53	pieces			HVLV FC-24	Feed Connector	1	pieces	
Actual Number of Chambers Requi	red 48	pieces		(CULTEC No. 41	0™ Filter Fabric	523.08	sq. meters	
Starter Chamb	ers 2	pieces		CUL	TEC No. 20L P	olyethylene Liner	3.40	meters	
Intermediate Chamb	ers 44	pieces				Stone	119.63	cu. meters	
End Chamb	ers 2	pieces							

Bed Detail



Number of Rows Wide	2	pieces
Number of Chambers Long	24	pieces
Chamber Row Width	2.79	meters
Chamber Row Length	51.66	meters
Bed Width	3.40	meters
Bed Length	52.27	meters
Bed Area Required	177.91	sq. meters

Bed detail for reference only. Not project specific. Not to scale. Use CULTEC StormGenie to output project specific detail.



Project Name: All Seniors

Date: December 17, 2018

Cross Section Detail



Conceptual graphic only. Not job specific.

Recharger 330XLHD

Pavement	76	mm
95% Compacted Fill	256	mm
Stone Above	150	mm
Chamber Height	774.7	mm
Stone Below	150	mm
Effective Depth	1074.9	mm
Bed Depth	1407.4	mm





Α	Depth of Stone Base	150.0	mm	Breakdown	of Storage	Provided by
В	Chamber Height	775.0	mm	Recharger 330XLHD	Stormw	ater System
С	Depth of Stone Above Units	150.0	mm	Chambers	71.61	cu. meters
D	Depth of 95% Compacted Fill	256.0	mm	Feed Connectors	0.01	cu. meters
Е	Max. Depth of Cover Allowed Above Crown of Chamber	3.7	meters	Stone	47.86	cu. meters
F	Chamber Width	1321.0	mm	Total Storage Provided	119.48	cu. meters
G	Center to Center Spacing	1.47	meters			

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Date:

Project Information:

All Seniors Storage Depth at 0.45m deep

Chamber Model-	Recharger 330XLHD	
Number of Rows-	2	units
Total number of chambers -	48	units
HVLV FC-24 Feed Connectors-	1	units
Stone Void -	40	%
Stone Base -	152	mm
Stone Above Units -	152	mm
Area -	177.92	m²
Base of Stone Elevation-	157.40	m



177.92 Min. Area Required Note: Min. Area required is based on 305mm around the system and typ. spacing

Recharger 330XLHD Incremental Storage Volumes						
Height of System	Chamber Volume	HVLV Feed Connector Volume	Stone Volume	Cumulative Storage Volume	Total Cumulative Storage Volume	Elevation
mm	m³	ft3	m³	m³	m³	m
1080	0.000	0.000	1.81	1.81	119.80	158.48
1054	0.000	0.000	1.81	1.81	117.99	158.45
1029	0.000	0.000	1.81	1.81	116.18	158.43
1003	0.000	0.000	1.81	1.81	114.37	158.40
978	0.000	0.000	1.81	1.81	112.57	158.38
953	0.000	0.000	1.81	1.81	110.76	158.35
927	0.001	0.000	0.90	0.90	108.95	158.33
914	0.182	0.000	1.73	1.92	108.05	158.31
889	0.490	0.000	1.61	2.10	106.13	158.29
864	0.806	0.000	1.49	2.29	104.03	158.26
838	1.190	0.000	1.33	2.52	101.74	158.24
813	1.440	0.000	1.23	2.67	99.22	158.21
787	1.661	0.000	1.14	2.80	96.54	158.19
762	1.833	0.000	1.07	2.91	93.74	158.16
737	1.987	0.000	1.01	3.00	90.83	158.14
711	2.121	0.000	0.96	3.08	87.83	158.11
686	2.237	0.000	0.91	3.15	84.75	158.09
660	2.342	0.000	0.87	3.21	81.60	158.06
635	2.438	0.000	0.83	3.27	78.39	158.04
610	2.534	0.000	0.79	3.33	75.12	158.01
584	2.601	0.000	0.77	3.37	71.79	157.98
559	2.717	0.000	0.72	3.44	68.42	157.96
533	2.822	0.000	0.68	3.50	64.98	157.93
508	2.841	0.000	0.67	3.51	61.48	157.91
483	2.870	0.000	0.66	3.53	57.97	157.88
457	2.889	0.002	0.65	3.54	54.44	157.86
432	2.909	0.001	0.64	3.55	50.90	157.83
406	2.918	0.001	0.64	3.56	47.34	157.81
381	2.937	0.001	0.63	3.57	43.78	157.78
356	3.005	0.001	0.61	3.61	40.21	157.76
330	3.081	0.001	0.58	3.66	36.60	157.73
305	3.091	0.001	0.57	3.66	32.94	157.70
279	3.101	0.001	0.57	3.67	29.28	157.68
254	3.110	0.001	0.56	3.67	25.61	157.65
229	3.120	0.001	0.56	3.68	21.94	157.63
203	3.139	0.000	0.55	3.69	18.26	157.60
178	3.187	0.000	0.53	3.72	14.57	157.58
152	0.000	0.000	1.81	1.81	10.85	157.55
127	0.000	0.000	1.81	1.81	9.04	157.53
102	0.000	0.000	1.81	1.81	7.23	157.50
76	0.000	0.000	1.81	1.81	5.42	157.48

Phone: 203-775-4416 Fax: 203-775-1462 www.cultec.com custservice@cultec.com

Recharger 330XLHD Incremental Storage Volumes						
Height of System	Chamber Volume	HVLV Feed Connector Volume	Stone Volume	Cumulative Storage Volume	Total Cumulative Storage Volume	Elevation
mm	m ³	ft3	m³	m³	m³	m
51	0.000	0.000	1.81	1.81	3.62	157.45
25	0.000	0.000	1.81	1.81	1.81	157.43
0	0.000	0.000	0.00	0.00	0.00	157.40



Stormceptor[®]



Brief Stormceptor Sizing Report - All Seniors

Project Information & Location					
Project Name	All Seniors	Project Number	1614		
City	Oakville	State/ Province	Ontario		
Country	Canada	Date	11/8/2017		
Designer Informatio	n	EOR Information (optional)			
Name	Stephen Potter	Name			
Company	Trafalgar Engineering Ltd.	Company			
Phone #	905-338-3366	Phone #			
Email	spotter@trafalgareng.com	Email			

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	All Seniors
Target TSS Removal (%)	60
TSS Removal (%) Provided	64
Recommended Stormceptor Model	EF6

The recommended Stormceptor Model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

EF Sizing Summary				
EF Model	% TSS Removal Provided			
EF4	59			
EF6	64			
EF8	67			
EF10	68			
EF12	70			
StormceptorMAX	Custom			

Stormceptor[®]

FORTERRA[®]

Sizing	Details

Drainage	Area	Water Quality Objective				
Total Area (ha)	0.459	TSS Removal (60.0			
Imperviousness %	63.0	Runoff Volume Cap				
Rainfa	ll	Oil Spill Capture Volume (L)				
Station Name	TORONTO CENTRAL	Peak Conveyed Flow				
State/Province	Ontario	Water Quality Flow F				
Station ID #	0100	Up Stre	am Storage			
Years of Records	18	Storage (ha-m)	Dischar	rge (cms)		
Latitude	43°37'N	0.000 0.000				
Longitude	79°23'W	Up Stream Flow Diversion				

Max. Flow to Stormceptor (cms)

Particle Size Distribution (PSD) The selected PSD defines TSS removal							
CA ETV							
Particle Diameter (microns)	Distribution %	Specific Gravity					
2.0	5.0	2.65					
5.0	5.0	2.65					
8.0	10.0	2.65					
20.0	15.0	2.65					
50.0	10.0	2.65					
75.0	5.0	2.65					
100.0	10.0	2.65					
150.0	15.0	2.65					
250.0	15.0	2.65					
500.0	5.0	2.65					
1000.0	5.0	2.65					
	Notes						

• Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.

• Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.

• For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.

For Stormceptor Specifications and Drawings Please Visit: http://www.imbriumsystems.com/technical-specifications



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100 MAXIMUM POPULATION PER ho	
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1. FOR GENERAL NOTES SEE DWG. No. 100	
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APPENDIX 'D'



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Project Name: 2135 Dundas St. W

SANITARY SEWER DESIGN SHEET (Metric)

Regional Municipality of Halton

Project No.: 1614 Date: 25-Nov-21

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APPENDIX 'E'

GENERAL NOTES

 CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE LATEST STANDARDS OF THE REGIONAL MUNICIPALITY OF HALTON (INCLUDING REGION OF HALTON'S CONTRACTOR INFORMATION PACKAGE), TOWN OF OAKVILLE AND THE ONTARIO BUILDING CODE (PART 7). ONTARIO PROVINCIAL STANDARD SPECIFICATIONS AND DRAWINGS (OPSS & OPSD) SHALL BE USED IN ABSENCE OF LOCAL STANDARDS.
 THIS DRAWING SHALL BE READ IN CONJUNCTION WITH ALL ARCHITECTURAL,

MECHANICAL AND LANDSCAPE DRAWINGS. 3. ALL INFORMATION SHOWN REGARDING THE LOCATION AND SIZE OF EXISTING UTILITIES AND/OR SERVICES HAS NOT BEEN VERIFIED. THE CONTRACTOR IS RESPONSIBLE FOR VERIFYING LOCATION OF UTILITIES PRIOR TO CONSTRUCTION AND

PROTECTING AND MAINTAINING DURING CONSTRUCTION.4. THE CONTRACTOR SHALL CHECK AND VERIFY ALL GIVEN GRADES AND ELEVATIONS PRIOR TO CONSTRUCTION AND REPORT ALL DISCREPENCIES TO THE ENGINEER.

5. ALL GRADING CHANGES SHALL BE APPROVED BY THE ENGINEER AND TOWN OF OAKVILLE PRIOR TO IMPLEMENTATION.

6. THE CONTRACTOR SHALL CLEAN ALL MUD TRACKED ON TO ADJACENT ROADWAYS.7. CONTRACTOR SHALL FLUSH AND VIDEO STORM AND SANITARY SEWERS UPON

INSTALLATION AND PROVIDE VIDEO TO THE ENGINEER. 8. CONTRACTOR SHALL PROVIDE A DIGITAL AS-BUILT SURVEY OF ALL UNDERGROUND AND ABOVEGROUND WORKS TO THE SATISFACTION OF THE ENGINEER.

SERVICING NOTES

1. ALL UTILITIES SHALL BE BACKFILLED WITH GRANULAR BACKFILL COMPACTED TO 98% S.P.M.D.D. NATIVE BACKFILL MAY BE USED WITH THE PERMISSION OF THE GEOTECHNICAL CONSULTANT. BEDDING AND COVER MATERIAL SHALL BE PER THE GEOTECHNICAL CONSULTANT'S RECOMMENDATIONS.

2. BACKFILLING AND RESTORATION WITHIN THE PUBLIC ROW SHALL BE IN ACCORDANCE WITH THE TOWN OF OAKVILLE ROAD CUT PERMIT AND TO THE SATISFACTION OF THE ENGINEERING & CONSTRUCTION DEPARTMENT.

3. SURROUND ALL MANHOLES WITH A MINIMUM OF 1.5m COMPACTED GRANULAR 'C' BACKFILL.

4. ALL ENDS OF SERVICE CONNECTIONS SHALL BE MARKED WITH 50x100 LUMBER PLACED FROM INVERT OF SERVICE TO 1.0m ABOVE GRADE.

STORM SEWERS

 ALL STORM SEWERS 600 mm AND SMALLER SHALL BE PVC SDR35 CSA B182.2 WITH BEDDING PER OPSD 802.010 UNLESS OTHERWISE NOTED.
 ALL STORM SEWERS 675 mm AND LARGER SHALL BE REINFORCED CONCRETE

PIPE CLASS 65-D CSA A257.2 COMPLETE WITH BEDDING PER OPSD 802.030. 3. CATCHBASIN SHALL BE PER OPSD 705.010, DOUBLE CATCHBASIN PER OPSD 705.020 c/w GRATE PER OPSD 400.100.

4. ALL CB AND CBMH IN PAVED AREAS SHALL BE INSTALLED WITH 3.0m-100mm PERFORATED PIPE c/w FILTER SOCK EXTENDING OUT FROM THE CB AND LOCATED BELOW THE SUBGRADE SURROUNDED BY 50mm GRANULAR 'A'.

 ALL CB LEADS SHALL BE 250mmø AT 1.0% UNLESS OTHERWISE NOTED. ALL DCB OR DI SHALL BE 300mmø AT 1.0% UNLESS OTHERWISE NOTED.
 CATCHBASINS IN LANDSCAPE AREAS SHALL BE SUMPLESS AND WITH 'BEEHIVE' TOP PER TOWN STD. 5–2.

7. ALL STORM MH'S SHALL BE 1200mmø PER OPSD 701.010 c/w COVER PER OPSD 401.010, UNLESS OTHERWISE NOTED.

8. ALL CATCHBASIN MANHOLES SHALL BE BENCHED.

WATERMAIN NOTES

1. 100mm AND LARGER SERVICES SHALL BE PVC, C-900, CLASS 150, SDR18 c/w MECHANICAL RESTRAINTS & TRACER WIRE PER REGION OF HALTON REQUIREMENTS.

- 2. 50mm AND SMALLER SERVICE SHALL BE TYPE "K" SOFT COPPER TUBING.
- 3. BEDDING ON WATER SERVICE SHALL BE PER OPSD 802.010*.
- 4. VALVE AND BOX FOR 100mm TO 300mm WATER SERVICE PER REGION OF HALTON STDS.
- 5. COVER SHALL BE 1.7m MIN. UNLESS OTHERWISE NOTED.
- 6. CONNECTION TO EXISTING WATERMAIN SHALL BE PER REGION OF HALTON STD RH 409.01.

7. WATER SYSTEM SHALL BE PRESSURE TESTED TO 150 PSI FOR 3 HRS AND WITNESSED BY REGION OF HALTON.

8. HYDRANTS SHALL BE MANUFACTURED IN ACCORDANCE WITH AWWA C502 AND SHALL HAVE STEAMER PORTS AS PER REGION STANDARD SPECIFICATIONS (SEE NOTE 11). ALL HYDRANTS SHALL BE INSTALLED AS PER OPSD 1105.010*. IF HYDRANT BARREL DEPTH EXCEEDS 1.7m A HYDRANT THAT CAN BE RAISED FROM THE BOTTOM WITHOUT INCREASING ROD LENGTH IS TO BE USED.

9. * INDICATES O.P.S.D. CAN BE USED AS MODIFIED BY REGION OF HALTON.10. MINIMUM LATERAL SEPARATION FROM OTHER UTLITIES IS 2.5m

REGIONAL APPROVAL:

REGION DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

SIGNED:_____DATED:___DATED:____DATED:_____DATED:_____DATED:_____DATED:_____DATED:_____DATED:______DATED:______DATED:_____DATED:_____DATED:______DATED:_____DATED:_____DATED:_____DATED:_____DATED:_____DATED:_____DATED:_____DATED:_____DATED:______DATED:______DATED:_____DATED:______DATED:______DATED:_______DATED:_______DATED:

The Applicant should be aware that the approval of the water system on private property is the responsibility of the Local Municipality. Regardless, the Applicant must ensure that the Region of Halton's standards and specifications are met. (the Water and Wastewater Linear Design Manual may be obtained from the Data Management Group at 905-825-6032) Furthermore, all water quality tests must be completed to Halton Region's satisfaction, before the water supply can be turned on.





GENERAL NOTES

1. CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE LATEST STANDARDS OF THE REGIONAL MUNICIPALITY OF HALTON (INCLUDING REGION OF HALTON'S CONTRACTOR INFORMATION PACKAGE), TOWN OF OAKVILLE AND THE ONTARIO BUILDING CODE (PART 7). ONTARIO PROVINCIAL STANDARD SPECIFICATIONS AND DRAWINGS (OPSS & OPSD) SHALL BE USED IN ABSENCE OF LOCAL STANDARDS.

2. THIS DRAWING SHALL BE READ IN CONJUNCTION WITH ALL ARCHITECTURAL, MECHANICAL AND LANDSCAPE DRAWINGS.

3. ALL INFORMATION SHOWN REGARDING THE LOCATION AND SIZE OF EXISTING UTILITIES AND/OR SERVICES HAS NOT BEEN VERIFIED. THE CONTRACTOR IS RESPONSIBLE FOR VERIFYING LOCATION OF UTILITIES PRIOR TO CONSTRUCTION AND PROTECTING AND MAINTAINING DURING CONSTRUCTION.

4. THE CONTRACTOR SHALL CHECK AND VERIFY ALL GIVEN GRADES AND ELEVATIONS PRIOR TO CONSTRUCTION AND REPORT ALL DISCREPENCIES TO THE ENGINEER.

5. ALL GRADING CHANGES SHALL BE APPROVED BY THE ENGINEER AND TOWN OF OAKVILLE PRIOR TO IMPLEMENTATION.

6. THE CONTRACTOR SHALL CLEAN ALL MUD TRACKED ON TO ADJACENT ROADWAYS.

GRADING NOTES

 SEDIMENT CONTROL MEASURES INCLUDING SILT FENCE AND MUD PAD ETC. SHALL BE INSTALLED PRIOR TO START OF CONSTRUCTION, CHECKED AND REPAIRED ON A REGULAR BASIS, AND LEFT IN PLACE UNTIL PAVING AND LANDSCAPING IS COMPLETED. SEDIMENT CONTROL WHEN REMOVED SHALL BE DISPOSED OFF-SITE.
 ALL TOPSOIL SHALL BE STRIPPED PRIOR TO GRADING.

3. ALL FILL PLACEMENT SHALL BE DONE IN ACCORDANCE WITH THE GEOTECHNICAL ENGINEERS RECOMMENDATIONS (TERRAPROBE, OCTOBER 31, 2017).

4. RETAINING WALLS WITH A HEIGHT GREATER THAN 1.0m ARE TO BE DESIGNED AND STAMPED BY A PROFESSIONAL ENGINEER.

5. ALL DISTURBED AREAS TO BE RESTORED WITH 200mm TOPSOIL AND SOD.

6. ALL DISTURBED AREAS WITH IN PUBLIC R.O.W TO BE REINSTATED TO THE SATISFACTION OF THE ENGINEERNG & CONSTRUCTION DEPARTMENT. EXISTING SODDED BLVD. AREAS TO BE REINSTATED WITH 200mm TOPSOIL AND SOD. SIDEWALKS AND PATHWAYS SHALL BE RESTORED WITH MATERIAL TO MATCH ORIGINAL UNLESS OTHERWISE NOTED.

7. REFER TO GEOTECHNICAL REPORT PREPARED BY EXP DATED JUNE 03, 2017 (FILE No. BRM-00603989-A0) FOR PAVEMENT STRUCTURE PAVEMENT STRUCTURE (HEAVY DUTY)

HL-3	40mm
HL-8	80mm
19mmCRL	150mm
50mmCRL	350mm

INC. OR AS OTHERWISE APPROVED BY EXP.

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