

### **FUNCTIONAL SERVICING REPORT**

Water, Sanitary, and Stormwater Management

### MACDONALD ROSE INC. SUBDIVISION

358 REYNOLDS STREET TOWN OF OAKVILLE

**OUR FILE: 1816** 

PREPARED FOR MACDONALD ROSE INC.

**NOVEMBER 10, 2023** 

Functional Servicing and Stormwater Management Report 358 Reynolds Street, Oakville

MacDonald Rose Inc. Subdivision

### **REVISION HISTORY**

DATE	REVISION	SUBMISSION			
November 10, 2023	2	Revised for 1st Pre-Submission Comments			
June 27, 2023	1	Issued for Rezoning/ Draft Plan of Subdivision Application			

### **TABLE OF CONTENTS**

1.0 INTRODUCTION	1
<ul> <li>1.1 Scope of Functional Servicing Report.</li> <li>1.2 Reference Documents.</li> <li>1.3 Site Location and Description</li> <li>1.4 Proposed Development.</li> </ul>	2
2.0 MUNICIPAL WATER AND WASTEWATER	2
2.1Water2.2Wastewater	
3.0 STORM DRAINAGE AND STORMWATER MANAGEMENT	4
3.1 Existing Storm Drainage	∠
3.1.1 Minor System	
3.1.2 Major System	
3.2 Proposed Storm Drainage	
3.2.1 Minor and Major System	
3.3 Stormwater Management	
3.3.1 Stormwater Quantity Control (Peak Flow Control)	7
4.0 GRADING	8
5.0 CONCLUSION	8
APPENDICES	
APPENDIX 'A'	
<ul><li>Draft Plan of Subdivision</li><li>Topographic Survey</li><li>Architectural Site Plan</li></ul>	
APPENDIX 'B'	
<ul> <li>Engineering Record Drawings</li> <li>Town of Oakville Stormwater Management Master Plan, Drawings 7.3 -7.4, 7.7</li> </ul>	
APPENDIX 'C' - Estimated Water Demand	
<ul><li>Estimated Sanitary Flow</li><li>Stormwater Calculations</li></ul>	
APPENDIX 'D' - Engineering Drawings	

### 1.0 INTRODUCTION

### 1.1 Scope of Functional Servicing Report

This report has been prepared in support of the Rezoning and Draft Plan of Subdivision Application for a proposed residential development located at 358 Reynolds Street in Oakville.

The Draft Plan of Subdivision for the subject lands was prepared by SGL Planning & Design Inc. dated November 6, 2023 and can be found in Appendix 'A'. The Draft Plan of Subdivision consists of 3 blocks. Block 1 and 2 are development blocks, while Block 3 is a road widening for MacDonald Road and includes a daylighting triangle at the southwest corner of MacDonald Road and Reynolds Street. The topographic survey prepared by R-PE Surveying Ltd. can also be found in Appendix 'A'.

This report outlines how the subdivision can be serviced by the existing and proposed infrastructure for water, wastewater, and storm drainage. This report should be read in conjunction with the other plans and reports submitted in support of the planning approvals being sought for the project.

For the purposes of this report, north is defined as running parallel to Reynolds Street.

### 1.2 Reference Documents

The following studies/reports/documents were reviewed in the preparation of this report.

- Drawing 7.3 to 7.4 "Stormwater Management Master Plan, Town of Oakville"
- Development Engineering Procedures & Guidelines Manual, Town of Oakville, May 2023 (Town's Manual)
- Stormwater Management Planning and Guidelines Manual, Ministry of Environment, March, 2003 (**MOE Manual**).
- "Water and Wastewater Linear Design Manual", Region of Halton October, 2019.
   (Region's Manual)

Furthermore, Trafalgar Engineering prepared plans and reports to support previous planning applications for the subject lands.

MacDonald Rose Inc. Subdivision

### 1.3 Site Location and Description

As previously mentioned, the site is known municipally as 358 Reynolds Street. The 0.283ha property is located on the south-west corner of MacDonald Road and Reynolds Street. The west and south sides of the property abut existing low density residential uses. The subject lands were the previous home of the Oakville Medical Arts building. An existing three storey building is located at the east side of the property and is currently vacant. South and west of the building is a large parking lot with a fringe of landscaping along its boundary. Driveway accesses are provided to both Reynolds Street and MacDonald Road. The existing site is relatively flat.

### 1.4 Proposed Development

The development blocks created by Plan of Subdivision will be further divided into 11 parcels/units and developed with two three-storey townhouse blocks consisting of 6 street townhomes for the west block (Block 1) and 5 street townhomes for the east block (Block 2). Building construction is slab on grade hence no basements are proposed. Each townhouse will have its own driveway entrance off of McDonald Road, with the exception of the corner unit on the east which will have a driveway entrance off of Reynolds Street. Pedestrian access will be provided by a new sidewalk proposed along MacDonald Road. A copy of the preliminary site plan is included in Appendix 'A' for reference.

### 2.0 MUNICIPAL WATER AND WASTEWATER

Municipal water and wastewater services for the subject site are to be designed in accordance with the Region of Halton Design Manual.

Per the Halton Water & Wastewater Linear Design Manual, for townhouses, the equivalent population density is 135 persons per hectare. Based on this density, the site would have an equivalent of 38 persons (135 persons/ha x 0.283 ha).

### 2.1 Water

There is an existing 300mm diameter watermain along MacDonald Road and an existing 300mm diameter watermain along Reynolds Street. The existing building is connected to the MacDonald Road watermain. See the engineering record drawings in Appendix 'B' for further detail.

Using the development area and Region of Halton design criteria, the domestic water usage is estimated and summarized below (see Appendix 'A' for supporting calculations). The fire flow is estimated for demand purposes only using the Fire Underwriter's Survey methodology and should be confirmed at the building permit stage.

MacDonald Rose Inc. Subdivision

### **Table 1 - Estimated Water Demands**

Average Daily Demand	5.0	(L/min)
Minimum Hourly Demand	5.0	(L/min)
Maximum Hourly Demand	20.0	(L/min)
Maximum Daily Demand	11.0	(L/min)
Estimated Fire Demand (FUS 1999)	8,000	(L/min)
Maximum Daily Plus Fire Demand	8,011	(L/min)

A flow test was undertaken (June 9, 2023) using the base hydrant at the east side of the site and the test hydrant at the north side of the site. The results of the flow test are included in Appendix 'C' and are summarized as follows:

### Base Hydrant at 358 Reynolds Street

Static Pressure; 57 psig

Flow 1,353 usgpm (5,100 L/min) residual 56 psig Flow 2,372 usgpm (10,320 L/min) residual 54 psig Theoretical Flow 3,560 usgpm (13,500 L/min) residual 20 psig

Estimated Max. Daily Plus Fire Service Pressure 56 psig

Based on the hydrant flow test, there is enough pressure and flow to meet the required demands.

The locations of the nearby hydrants on Reynolds Street and MacDonald Road provide adequate coverage for the proposed development and are within 90 metres of all principal entrances.

The subject site will be serviced using the existing 300mm local watermain on MacDonald Road for domestic water. Each townhouse will have typical 25mm individual service connections. The existing water connection to MacDonald Road will be disconnected.

### 2.2 Wastewater

There are existing 200mm diameter sanitary sewers along MacDonald Road and Reynolds Street. The two sanitary sewers on MacDonald Road flow west to Trafalgar Road and are about 2m deep to the invert. The sanitary sewer on Reynolds Street flows south and is approximately 2m deep to the invert. Records show that the existing building is connected to the existing sewer along MacDonald Road. Record drawings also show a second sewer lateral was provided to the property as part of the sewer reconstruction along Reynolds Street that was undertaken in 2006. See Appendix 'B' for further detail. The sewage flows were calculated for the development and the results are as summarized below. Further detail can be found in Appendix 'C'.

### **Table 2 - Estimated Sanitary Demands**

Average Daily Dry Weather Flow	0.12	(L/s)
Modified Harmon Peaking Factor	4.34	
Infiltration Allowance (0.26 L/s-ha)	0.08	(L/s)
Peak Daily Flow	0.61	(L/s)

The subject site will be serviced using the existing 200mm diameter sanitary sewers on MacDonald Road and Reynolds Street. Each townhouse will have typical 125mm individual service connections. The existing sanitary service to the building will be disconnected.

The MacDonald Road sewer is tributary to the Trafalgar Road/Rebecca Street Trunk sewers. An analysis of the downstream sewer system can be provided once the Region's Infoworks model is available.

### 3.0 STORM DRAINAGE AND STORMWATER MANAGEMENT

### 3.1 Existing Storm Drainage

### 3.1.1 Minor System

There is a 975mm diameter sewer running along Reynolds Street adjacent to the subject site. The sewer system is tributary to the Sixteen Mile Creek. The record drawings also indicate that there is an abandoned 450mm diameter sewer along Reynolds Street (See Appendix 'B'). Adjacent to the site, along MacDonald Road, is a flat roadside ditch draining from west to east to the Reynolds Street sewer.

Based on a review of Oakville's Stormwater Master Plan (Drawing 7.3 and 7.4 – see Appendix 'B' for further detail), the storm sewer on Reynolds Street in the vicinity of the site is identified as unsurcharged during the 5-year event and ½ surcharging depth and above the obvert during the 100-year storm in the existing condition.

The topographic survey indicates that the majority of the parking lot west of the existing building drains towards the existing ditch along MacDonald Road. A small fringe strip along the southern part of the parking lot drains towards the adjacent lands to the south.

The driveway south of the existing building is drained by two catchbasins that collect drainage from the driveway. The rainwater leaders from the roof run along the outside face of the building and are connected to an underground drainage system. Both above items indicate that there is an onsite storm sewer system, however we have not been able to determine the connectivity of the existing sewer system.

### 3.1.2 Major System

Based on a review of Oakville's Stormwater Master Plan (*Drawing 7.7 – See Appendix 'B' for further detail*), the flow is contained within the curb during the 100-year storm in the existing condition.

A review of the existing major overland flow along MacDonald Road indicates that the elevation at the corner of Reynolds and MacDonald prevents overland flow from being directed along the municipal right-of-way. Flow analysis in HEC-RAS was undertaken to assess the existing conditions, and the results showed that the major overland flow route is through the subject lands.

The area draining towards the existing ditch on the south side of the roadway includes the entire MacDonald Road right-of-way, the residential lots on the north side of the roadway, parts of the lots on the south side of MacDonald Road west of the site, and the site itself. Using existing topographic mapping, a drainage area was estimated to be 1.04 ha as shown in the Storm Drainage Area Plan (Appendix 'D').

### 3.2 Proposed Storm Drainage

### 3.2.1 Minor and Major System

The Town's Stormwater Management Master Plan sets out evaluation criteria and hierarchy for conveyance capacity improvements (major systems) within the Town's network. Figure 8.2.1 from the Master Plan provides a flow chart for making those evaluations. When greater than 50% of the major overland flow is outside the ROW and toward the buildings, the evaluation indicates the need to increase the pipe size within the minor system and to re-profile the road where offline storage is unavailable. Since there are no opportunities for offline storage, we propose removal of the existing ditch, re-profiling the south edge, introducing a curb, gutter, and boulevard (urbanization), and a municipal storm sewer on MacDonald Road.

With the urbanization of MacDonald Road across the subject land's frontage, the existing ditch will be replaced with a storm sewer and a series of catchbasins and connected to the existing 975mm diameter storm sewer on Reynolds Street. The proposed storm sewer will be 450mm in diameter and has been designed for the 100-year storm.

Flows from the existing ditch west of the site will be intercepted by a ditch inlet catchbasin and conveyed to the 525mm diameter storm sewer which will allow flows from the ditch to the west to enter the sewer system.

The front yards, driveways, and front roof areas will sheet flow from the buildings to MacDonald Road. The rear roof areas will splash to grade and be directed to a rear lot catchbasin and lead to the proposed 450mm storm sewer on MacDonald Road.

The overland flow route from the subject site will be directed east along MacDonald Road and ultimately south along Reynolds Street. Due to the grading conditions at the south end of the property, the rear lot catchbasin will require a lower top of grate elevation than the proposed catchbasins on MacDonald Road. To avoid the potential of the storm sewer backing up and spilling from the rear lot catchbasin, a backflow preventer is proposed in the catchbasin lead directly north of the catchbasin. This will ensure that stormwater is self-contained and that there is safe conveyance to municipal lands. Further detail on the 100-year ponding level of the rear lot catchbasin will be provided at the site plan stage.

### 3.3 Stormwater Management

The Town of Oakville requirements for stormwater management are as follows:

### 1. <u>Stormwater Quantity Control (Peak Flow Control)</u>

The minimum control is to maintain post-development peak runoff rates to predevelopment levels for all events up to and including the 100-year storm.

### 2. <u>Stormwater Runoff Volume Reduction (Water Balance)</u>

As per the draft Oakville Development Engineering Procedures and Guidelines (May 2023), sites are to be designed such that the runoff from a 25 mm event shall be retained on site.

### 3. <u>Stormwater Quality Control</u>

- i) Construction Phase (Erosion and Sediment Control)
- Post Construction: Achieve Enhanced Level 1 Protection, as per the Ministry of Environment's Stormwater Management Planning and Design Manual (March 2003).

### 3.3.1 Stormwater Quantity Control (Peak Flow Control)

The required quantity control for the site is to limit the peak post-development flows to the predevelopment flows.

Based on the existing topographic survey, a pre-development composite runoff coefficient was determined for the subject site. In calculating the runoff coefficient, C=0.25 was used for pervious areas and C=0.90 used for impervious areas (building roof, parking lots, walkways).

Using a similar method, a post-development composite runoff coefficient was developed using the proposed site plan.

The overall post-development imperviousness of the site will be slightly less than in the predevelopment condition given that the existing site mainly consists of an asphalt parking lot and building. The pre-development runoff coefficient was found to be C=0.84, while the postdevelopment runoff coefficient was calculated as C=0.71. As a conservative approach, a postdevelopment runoff coefficient of C=0.84 was used to determine the allowable release rate in the post-development condition. With this approach, there is no change in flows when comparing the pre-development condition to the post development condition. Therefore, no quantity controls are proposed.

### 3.3.2 Stormwater Runoff Volume Reduction (Water Balance)

As per the Town's Development Manual, it is recommended that 25 mm of water is retained across the site. This would result in 70.75 m³ of retention volume. Given the tenure of the development, space limitation, and desired tree preservation, the opportunity for introduction of meaningful LID measures is limited. Notwithstanding, best efforts to address the volume control criteria should be made. We suggest the use of an infiltration strip across the rear yards outside the tree preservation zone. Further detail can be provided *once a hydrogeologic study is undertaken to determine if groundwater and soil conditions are suitable for infiltration*.

### 3.3.3 Stormwater Quality Control

Stormwater quality controls will need to be implemented during the construction phase as well as post-construction.

### i) Construction Phase (Erosion and Sediment Control)

The primary source of sediment laden runoff will be as a result of vehicle mud tracking. In addition to on-site controls, off-site controls in the vicinity of the site will be required to mitigate sediment transport. Prior to any construction activity, all sediment and erosion control measures shall be implemented. These measures include sediment control fence, mud mat at construction entrance, catch basin sediment control and routine 'housekeeping' such as sweeping and flushing of the surrounding roads.

All controls shall be inspected on a regular basis and after rainfall events that generate runoff. Of particular importance are the controls placed at catch basins. If not maintained, the tendency for these to become obstructed is high and hence there is a potential for localized pooling and/or drainage issues.

### Our File: 1816

### ii) Post Construction

The majority of the site's drainage will be from the roof of the buildings, which can be considered clean and will not require treatment. No measures are proposed for the driveways and front yards. All other drainage will be directed through grassed swales in the rear yards, which will help to trap and remove sediments prior to discharge into the rear lot catchbasin. No further quality control measures are proposed.

### 4.0 GRADING

The grading of the subdivision must take into account the boundary conditions that exist along all sides of the property such that existing drainage patterns are maintained. The grading to the north is controlled by the top of curb and boulevard gradient of the proposed urbanized roadway, while the grading to the east is controlled by the existing curb and sidewalk on Reynolds Street. The west and south sides of the site must match into the existing elevations along the adjoining properties. In addition, the south side of the site provides some further constraints due to several trees along the property line that are to be preserved. A 3:1 slope is proposed along the tree protection fence to avoid negative impact to the trees. Refer to the Engineering Drawings in Appendix 'D' for further information.

It is proposed that the lots follow a split drainage approach. The lots are sloped such that there will be a walkout condition from the ground floor level out to the rear yard, while the principal entrance is through the main floor level.

Between the two blocks, a swale is proposed to collect drainage. The swale will drain south into a proposed rear lot catchbasin. The south side of both townhouse blocks will also consist of shared swales to collect drainage from the rear yards of the townhouses.

The west side of the site will drain south through a proposed swale. A site visit has noted that the property to the west slopes away from the subject site with the front yard sloping towards the street and the rear yard towards the south.

The adjacent properties to the south drain away from the subject lands toward the south.

### 5.0 CONCLUSION

Adequate municipal infrastructure exists within the abutting road allowances to support the proposed Draft Plan of Subdivision and Rezoning Amendments being sought. The information in this report provides the framework from which detailed designs can evolve as the development progresses through the planning approval and permitting process.

A 525mm storm sewer will be constructed to collect the 100-year storm from the existing drainage area tributary to the ditch fronting the property.

The development proposal results in a minor decrease in impervious area and therefore a decrease in flows from the subject lands. Using the pre-development runoff coefficient of C=0.84 as the post-development runoff coefficient, there is no increase in flows in the post-development condition. No quality or quantity controls are proposed.

Implementation of the servicing and grading designs presented in this report will provide the normal expected level of service for the proposed development with no impact to the abutting properties.

PREPARED BY TRAFALGAR ENGINEERING LTD.

Mary Fornasier, EIT Intermediate Designer Paul Cifoni, P.Eng. Consulting Engineer

Principal

P:\1816 358 Reynolds Street\03-Documents\05-Reports\2023-03-31 FSR\2023-03-31 FSR\docx

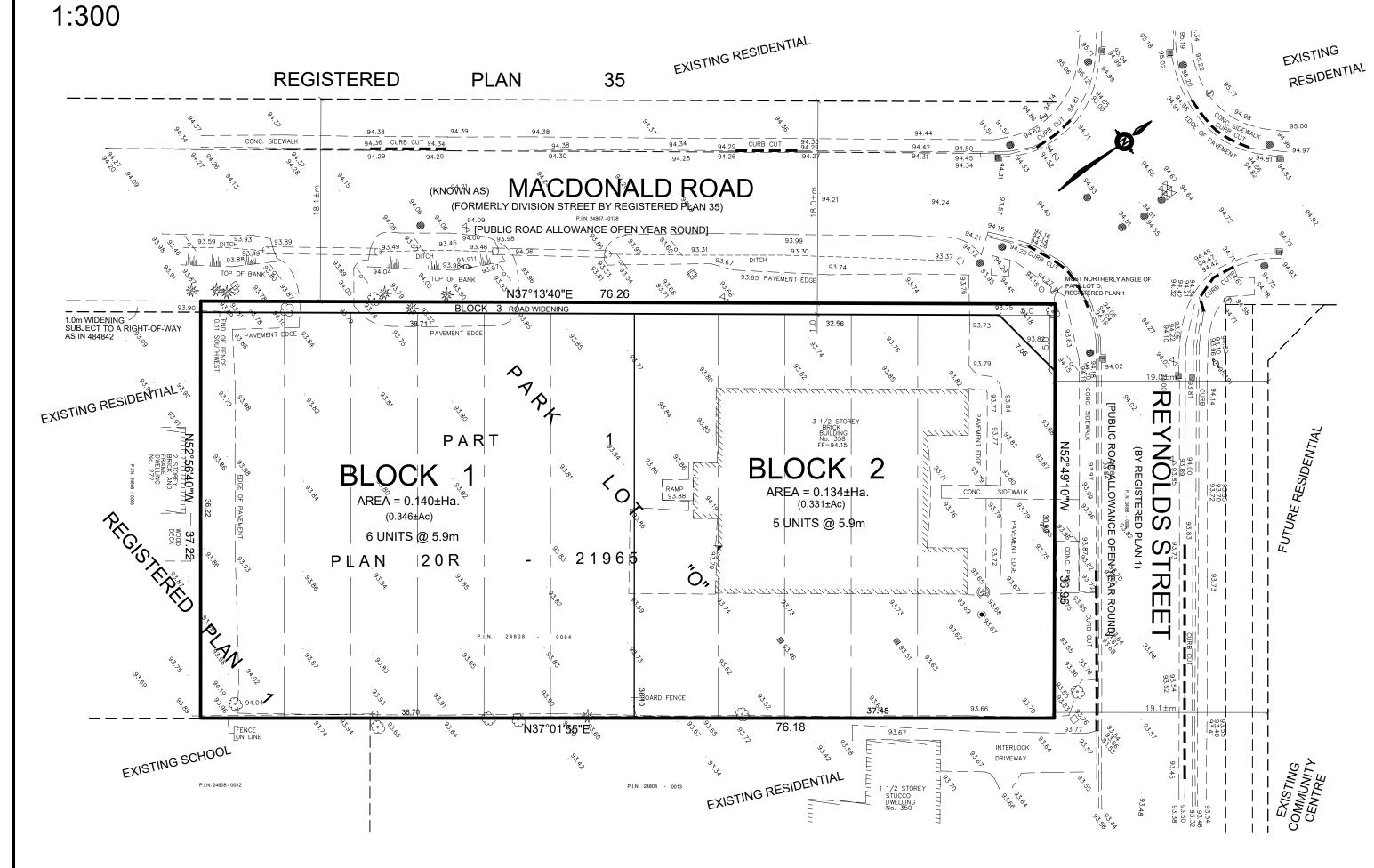
### APPENDIX 'A'

Draft Plan of Subdivision

Topographic Survey

Architectural Site Plan

## DRAFT PLAN OF SUBDIVISION PART OF PARK LOT "O" REGISTERED PLAN 1 TOWN OF OAKVILLE REGIONAL MUNICIPALITY OF HALTON



### **OWNER'S CERTIFICATE**

I AUTHORIZE SGL PLANNING & DESIGN INC. TO PREPARE AND SUBMIT THIS DRAFT PLAN OF SUBDIVISION TO THE TOWN OF OAKVILLE FOR APPROVAL.

OWNER:

### MACDONALD ROSE INC.

c/o MELROSE INVESTMENTS INC. 145 REYNOLDS STREET SUITE 400 OAKVILLE, ONTARIO L6J 0A7

SILVIO GUGLIETTI A.S.O.

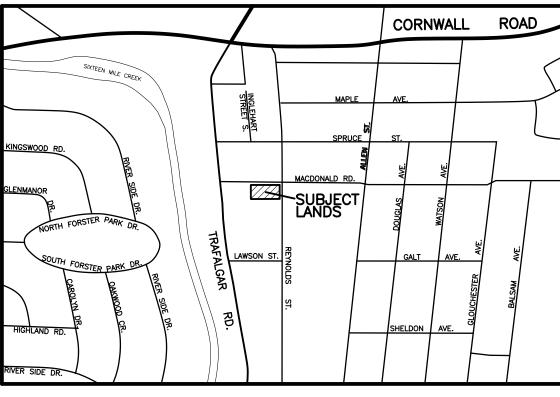
### SURVEYOR'S CERTIFICATE

I HEREBY CERTIFY THAT THE BOUNDARIES OF THE LAND TO BE SUBDIVIDED AS SHOWN ON THIS PLAN, AND THEIR RELATIONSHIP TO THE ADJACENT LAND ARE ACCURATELY AND CORRECTLY SHOWN.

DATE NOVEMBER, 2023

R. DENBROEDER O.L.S.

### DRAFT PLAN 24T-



**KEY PLAN** 

SCALE 1:10 000

### SECTION 51, PLANNING ACT, ADDITIONAL INFORMATION

- A. AS SHOWN ON DRAFT PLAN
- B. AS SHOWN ON DRAFT PLAN
- C. AS SHOWN ON DRAFT PLAN
- ACCUONAL ON DRAFT DUAN
- E. AS SHOWN ON DRAFT PLAN
- H. MUNICIPAL PIPED WATER AVAILABLE AT TIME OF DEVELOPMENT
- I. CLAY-LOAN
- J. AS SHOWN ON DRAFT PLAN
- K. SANITARY AND STORM SEWERS, GARBAGE COLLECTION, FIRE PROTECTION
- L. AS SHOWN ON DRAFT PLAN

### SCHEDULE OF LAND USE

TOTAL AREA OF LAND TO BE SUBDIVIDED = 0.283±Ha. (0.699±Acs)

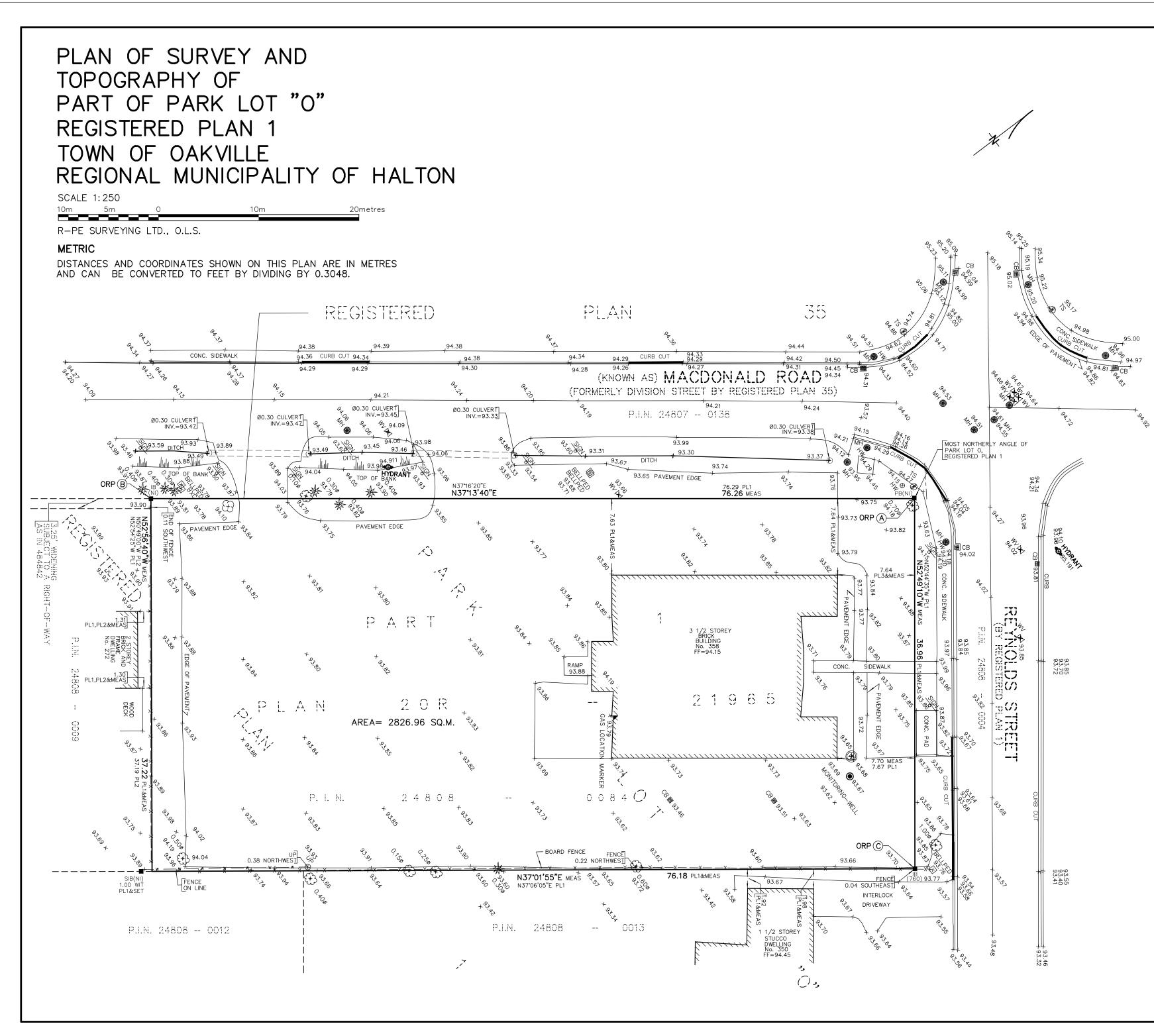
		BLOCKS	RES. UNITS	±Ha.	±Acs.
BLOCKS 1 and 2	- TOWNHOUSE (Min 5.9.m/Unit)	2	11	0.274	0.677
BLOCK 3	- ROAD WIDENING	1		0.009	0.022
TOTAL		3	11	0.283	0.699

NOTE - ELEVATIONS RELATED TO CANADIAN GEODETIC DATUM

3395DES2

(XREF: 3295MAS2 & 3295TOPO2) NOVEMBER 6, 2023





### **LEGEND**

BELLPED DENOTES BELL BOX DENOTES COMMUNICATION CABLE BOX DENOTES CATCH BASIN DENOTES CONCRETE DENOTES FINISHED FLOOR DENOTES FINISHED FLOOR
DENOTES CULVERT INVERT ELEVATION
DENOTES UTILITY POLE
DENOTES TRAFFIC SIGN DENOTES HANDWELL DENOTES HYDRANT VAULT DENOTES MANHOLE DENOTES WATER VALVE WV DENOTES OVERHEAD WIRE -W-DENOTES DIAMETER
DENOTES DECIDUOUS TREE DENOTES CONIFEROUS TREE DENOTES FENCE LINE DENOTES WELL

### **NOTES**

DENOTES STANDARD IRON BAR DENOTES IRON BAR DENOTES PLASTIC BAR PB DENOTES PROPERTY IDENTIFIER NUMBER P.I.N. DENOTES PLAN 20R-21965 PL1 DENOTES PLAN OF SURVEY BY SEWELL AND SEWELL O.L.S., DATED MARCH 31, 1969 DENOTES McCONNELL MAUGHAN LIMITED, O.L.S.

DENOTES WITNESS

DENOTES NOT IDENTIFIED

DENOTES OBSERVED REFERENCE POINT

DENOTES MONUMENT FOUND

### BENCHMARK NOTE

ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES.

TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD.

ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

### INTEGRATION NOTE

BEARINGS ARE GRID, UTM, NAD83 (CSRS: CBNv6: 2010.0), DERIVED FROM OBSERVED REFERENCE POINTS FROM REAL TIME NETWORK STATION 20120110009 (NORTHING 4801633.529, EASTING 597944.44).

COORDINATES ARE UTM, ZONE 17, NAD83 (CSRS: CBNv6: 2010.0), TO URBAN ACCURACY PER SEC. 14 (2) OF O.REG. 216/10, AND CANNOT, IN THEMSELVES, BE USED TO RE-ESTABLISH CORNERS OR BOUNDARIES SHOWN ON THIS PLAN.

POINT	NORTHING	EASTING
ORP (A)	4812052.21	607160.68
ORP (B)	4811991.51	607114.55
ORP ©	4812029.89	607190.11

DISTANCES ARE GROUND AND CAN BE CONVERTED TO GRID BY MULTIPLYING BY THE COMBINED SCALE FACTOR OF 0.999732.

### SURVEYOR'S CERTIFICATE

1. THIS SURVEY AND PLAN ARE CORRECT AND IN ACCORDANCE WITH THE SURVEYS ACT, THE SURVEYORS ACT AND THE REGULATIONS MADE UNDER

2. THE SURVEY WAS COMPLETED ON THE 18<sup>th</sup> DAY OF JANUARY , 2023

DATE JANUARY 19<sup>th</sup> , 2023

R. DENBROEDER

ONTARIO LAND SURVEYOR

THIS PLAN OF SURVEY RELATES TO AOLS PLAN SUBMISSION FORM NUMBER 2203815.

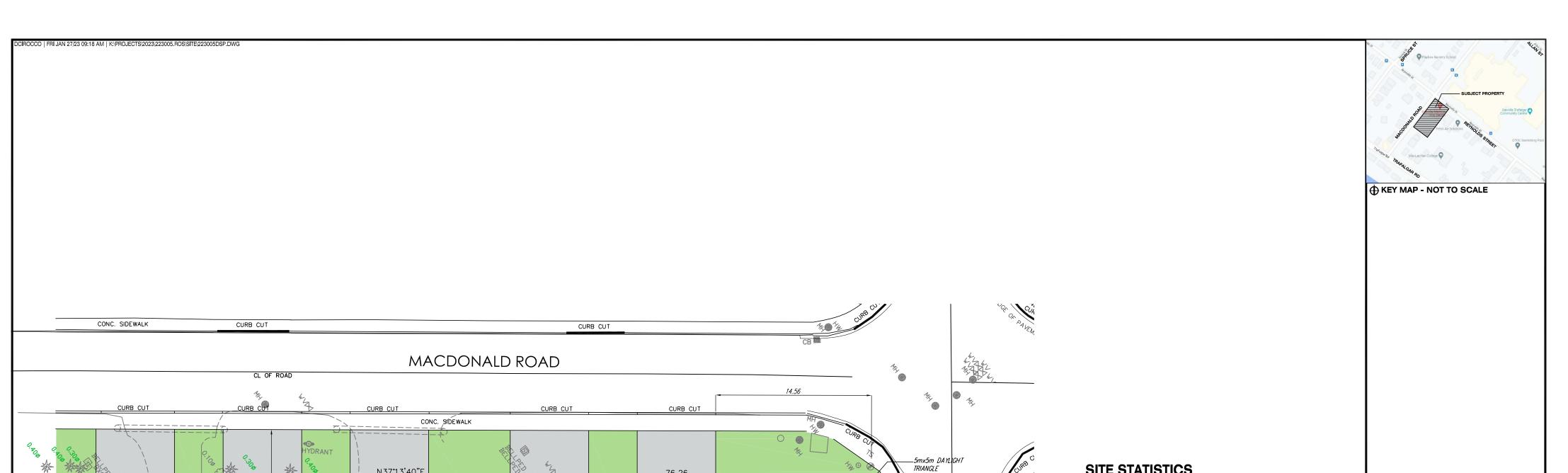


### R—PE SURVEYING LTD. Ontario land surveyors

643 Chrislea Road, Suite 7 Woodbridge, Ontario L4L 8A3 Tel.(416)635-5000 Fax (416)635-5001 Tel.(905)264-0881 Fax (905)264-2099 Website: www.r-pe.ca

DRAWN: S.L. CHECKED: R.D.

JOB No. 22-388 CAD FILE No.22-388TP01A



76.26

EXISTING BUILDING BE DEMOLISHED

1 1/2 STOREY STUCCO DWELLING No. 350

BUILDING 1
3-STOREY TOWNHOUSES
5.94
5.94

N37°13'40"E

1.0m ROAD WIDENING

6

N37°01'55"E

BU LDING 2 3-STOREY TOWNHOUSES

### SITE STATISTICS

SITE AREA:

STREET

REYNOLDS

INTERLOCK DRIVEWAY

GROSS SITE AREA = 2827.03 s.m. (0.283 HA)

ROAD WIDENING = 76.26 s.m. DAYLIGHT TRIANGLE = 12.44 s.m.

NET SITE AREA = 2738.33 S.M. (0.274 HA)

TOTAL UNITS: 11 UNITS (38.9 UNITS/HA)

PROPOSED ZONING STANDARDS: MINIMUM FRONT YARD: 6.0m MINIMUM REAR YARD: 7.5m MINIMUM INTERIOR SIDE YARD: 1.2m

MINIMUM EXTERIOR SIDE YARD: 3.0m MAXIMUM BUILDING HEIGHT : 14.0m

AREA CALCULATIONS						
LOT	LOT AREA	UNIT	AREA	U	VIT COVERA	GE
	(S.M.)	(S.M)	(S.F.)	(S.M.)	(S.F.)	(%)
1	439.93	343.00	3692	140.28	1510	31.9%
2	213.91	281.59	3031	129.69	1396	60.6%
3	214.03	281.59	3031	129.69	1396	60.6%
4	214.15	281.59	3031	129.69	1396	60.6%
5	269.48	284.75	3065	132.57	1427	49.2%
6	269.72	281.59	3031	132.57	1427	49.2%
7	214.58	281.59	3031	129.69	1396	60.4%
8	214.70	281.59	3031	129.69	1396	60.4%
9	214.82	281.59	3031	129.69	1396	60.4%
10	214.94	281.59	3031	129.69	1396	60.3%
11	270.52	284.75	3065	132.57	1427	49.0%

THE UNDERSIGNED HAS REVIEWED AND TAKES RESPONSIBILITY FOR THIS DESI AND HAS THE QUALIFICATIONS AND MEETS THE REQUIREMENTS SET OUT IN TH ONTARIO BUILDING CODE TO BE A DESIGNER. HUNT DESIGN ASSOCIATES INC. DESIGN ASSOCIATES INC. www.huntdesign.ca 8966 Woodbine Ave, Markham, ON L3R 0J7 T 905.737.5133 email: hdai@huntdesign.ca 358 REYNOLDS STREET, OAKVILLE, ON. **ROSEHAVEN HOMES - 223005** 223005DSP

### **APPENDIX 'B'**

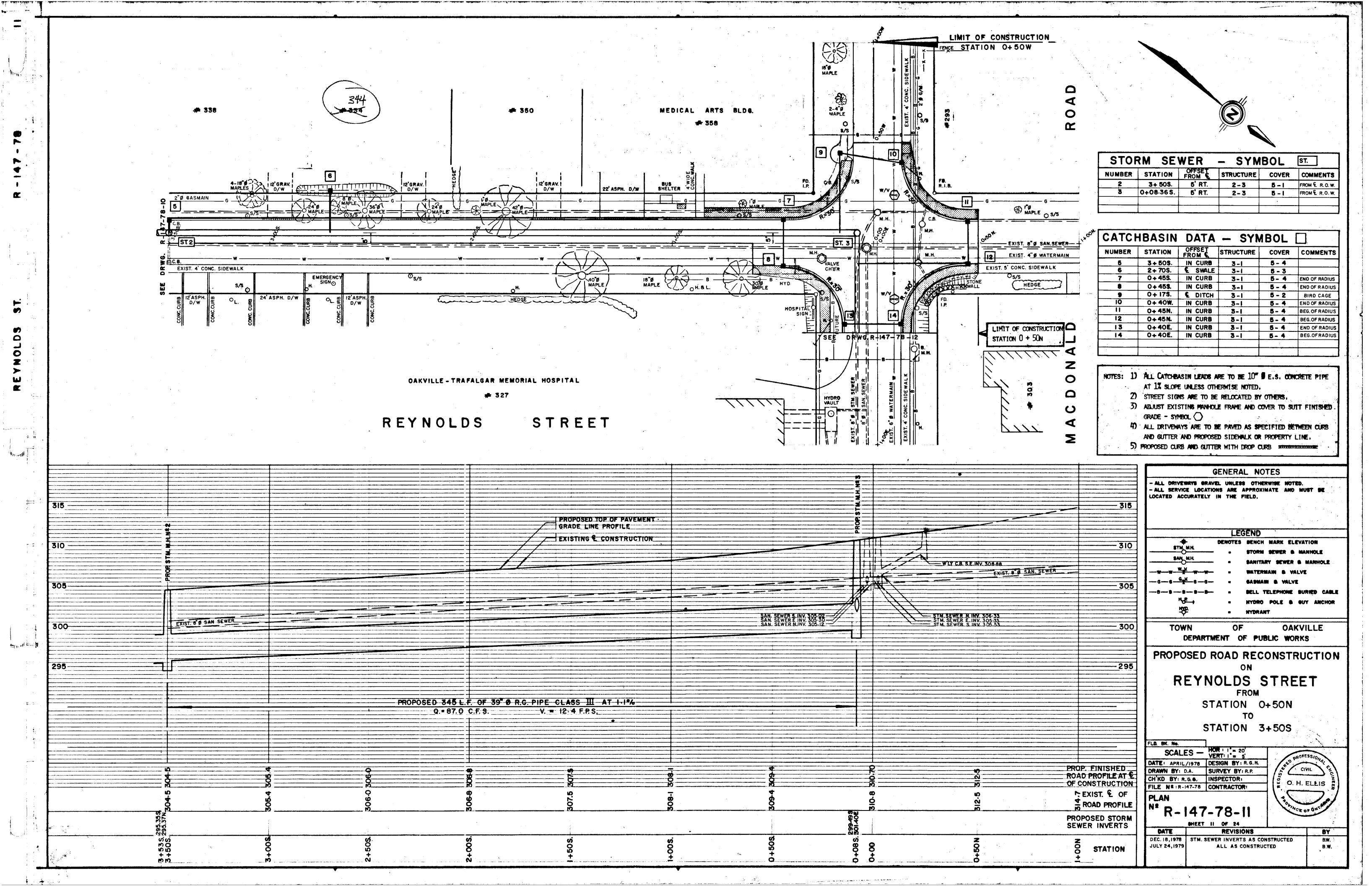
### **Engineering Record Drawings**

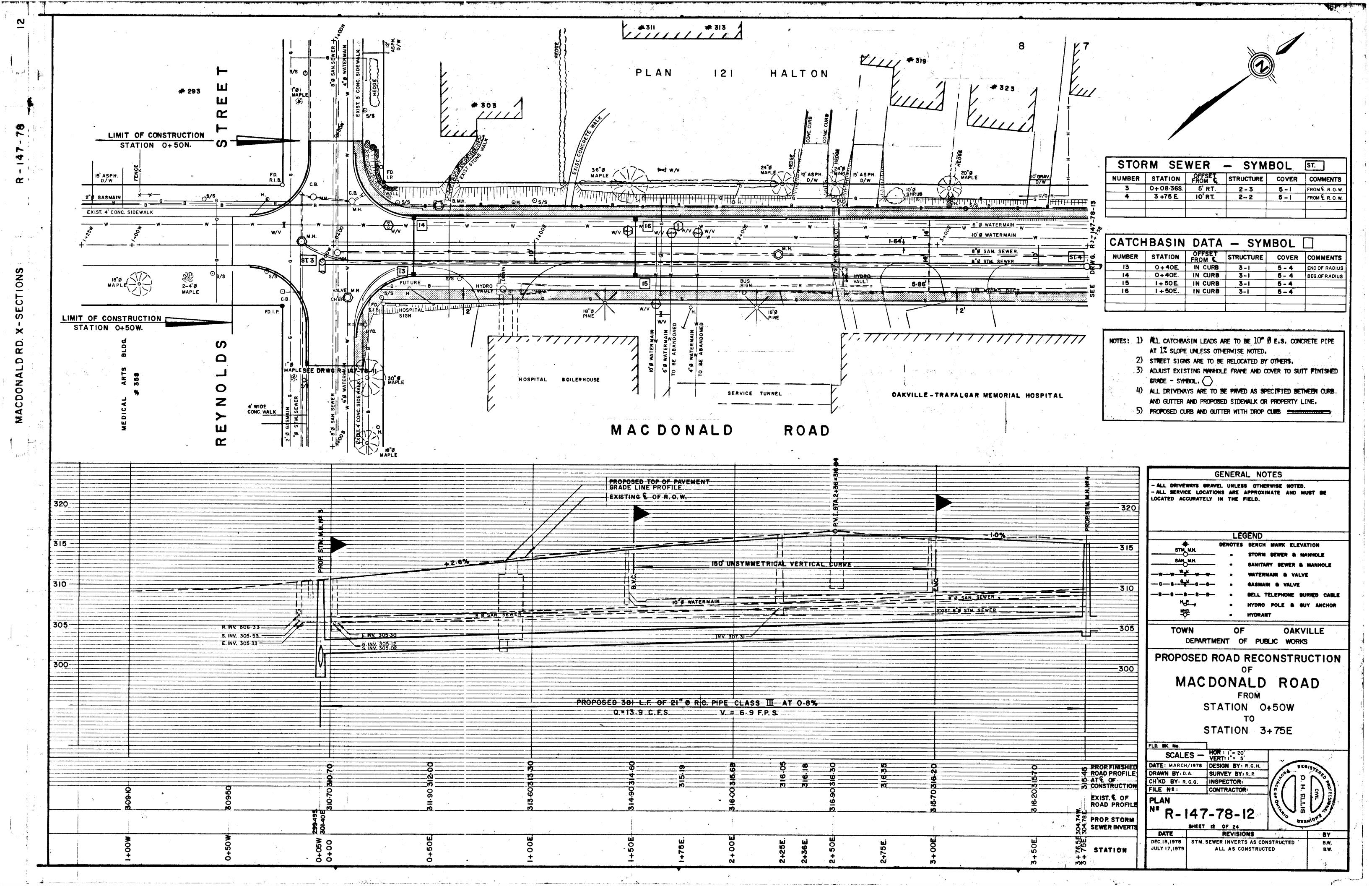
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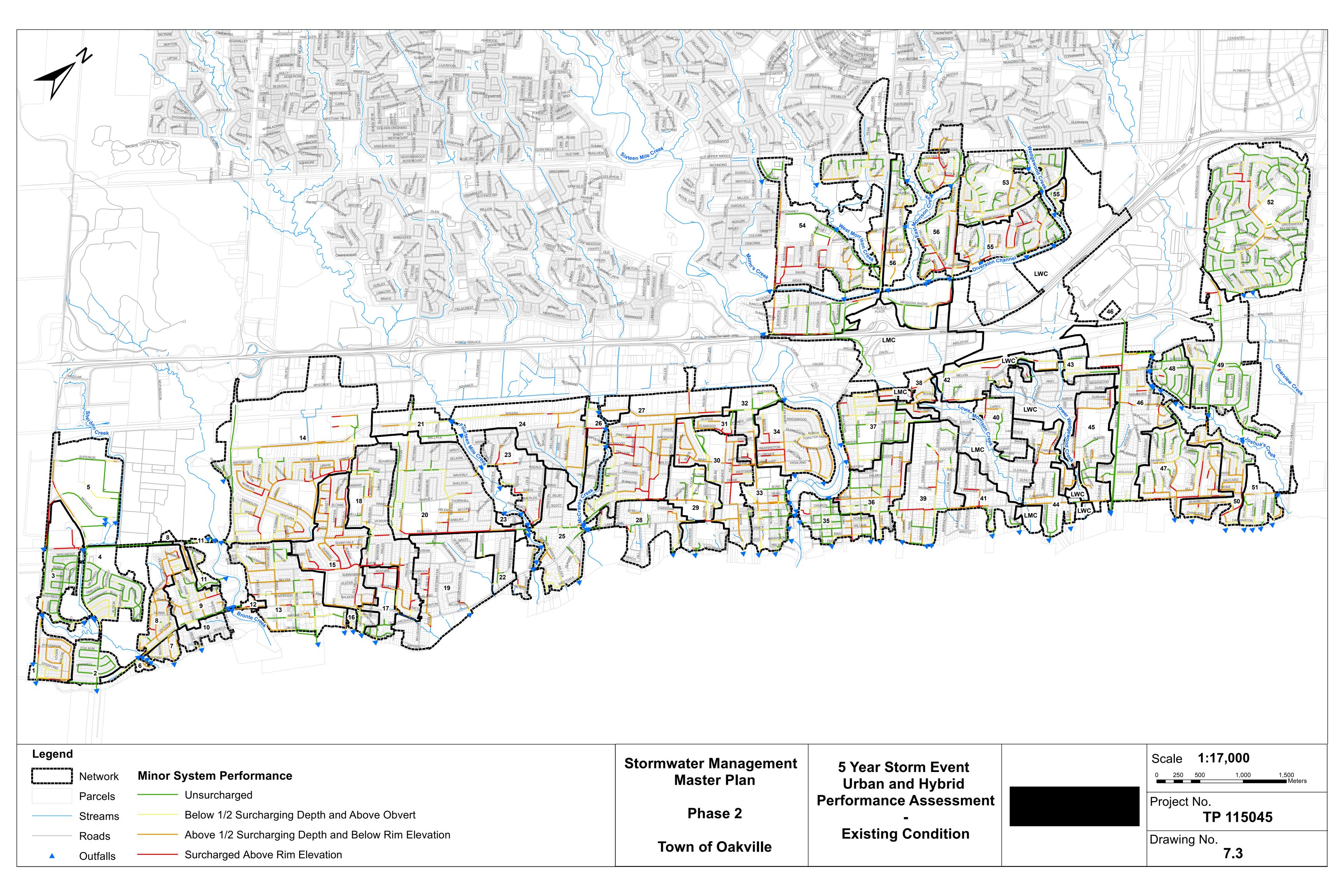
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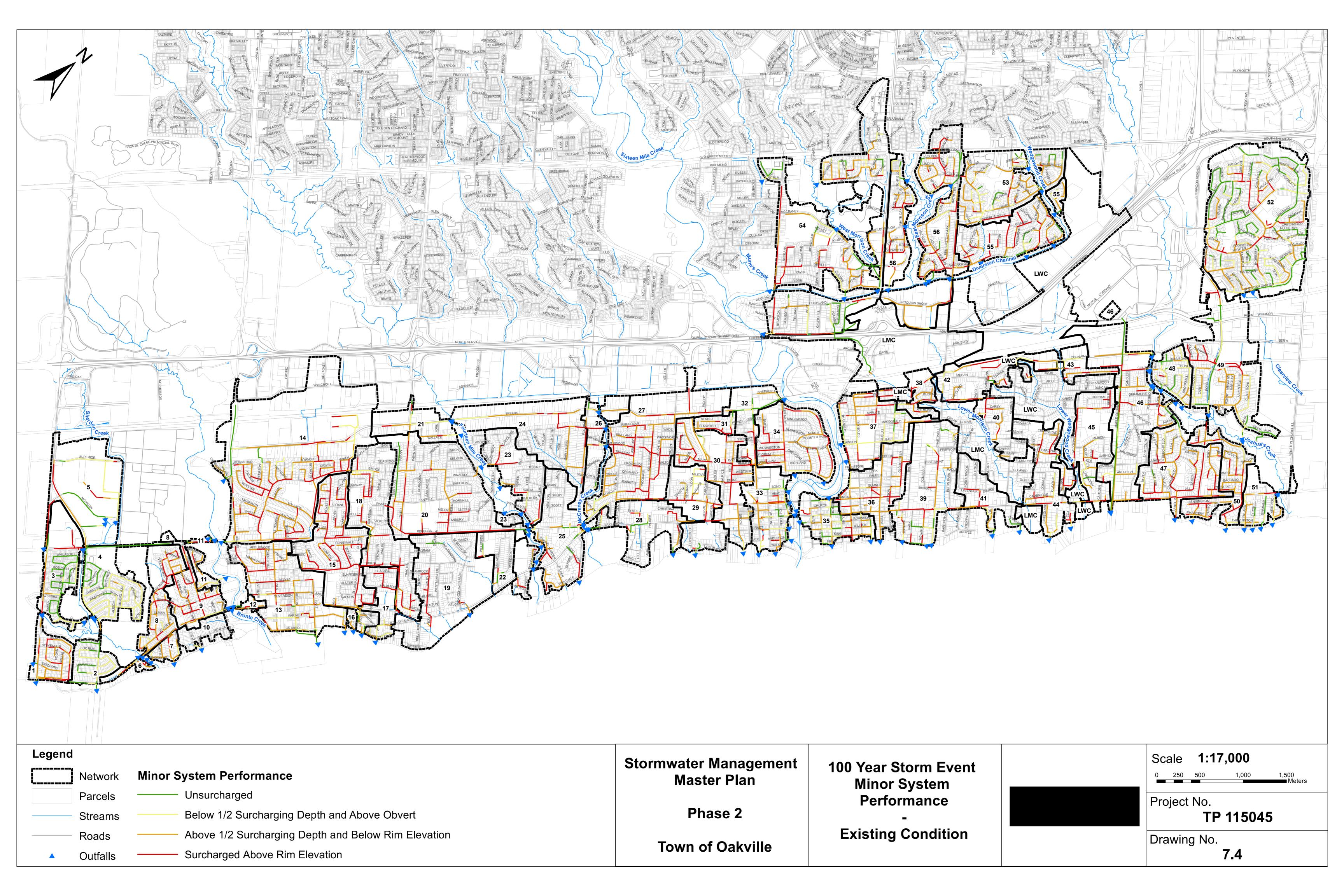
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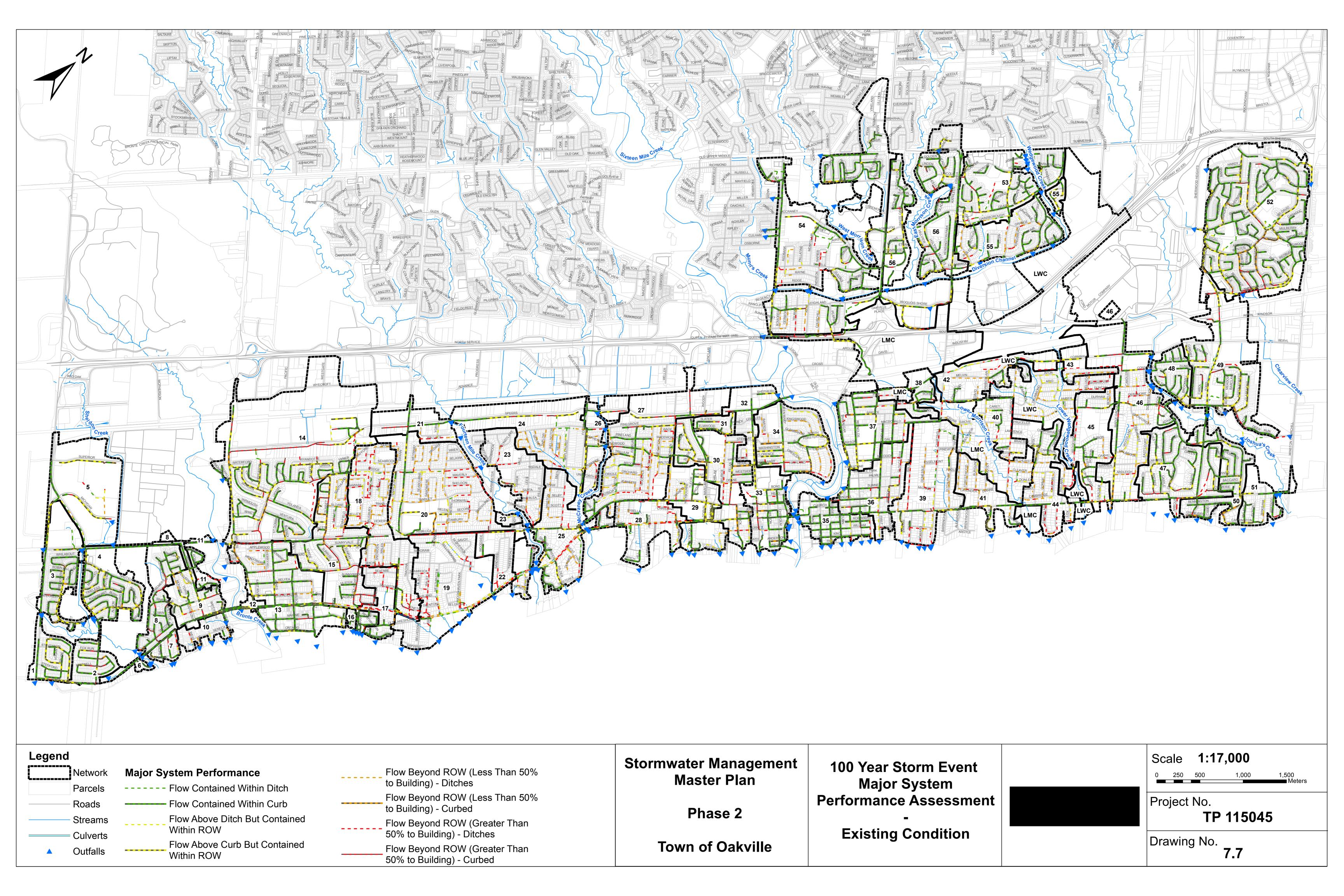
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### APPENDIX 'C'

**Estimated Water Demand** 

Estimated Sanitary Flow

Stormwater Calculations

### **ESTIMATED WATER DEMAND**

Project: 358 Reynolds Street Project No.: 1816 Townhouse Units Prepared By: MF Desc: Checked By: PC **Occupancy Data Peaking Factors Demand Flow** Population Per Cap. Min. Hour Max. Hour Max. Daily Density Eq. Population Demand (L/cap. Average Daily Demand Demand Demand Land Use / Occupancy Type Area (ha) (pers/ha) (cap.) Day) Demand (L/min) Min. Hour Peak Hour Max. Daily (L/min) (L/min) (L/min) Townhouse Units 0.283 135.0 191 1.00 4.00 11 \*Per Cap. Demand based on O.B.C. Table 8.2.1.3.B. - 5 L/1.0m<sup>2</sup> Stores TOTAL 38 5 20 11 5 Fire Flow Average Daily Demand: 5 (L/min) **Using Fire Underwriters Survey Methodology: Minimum Hourly Demand:** 5 (L/min) **Maximum Hourly Demand:** 20 (L/min) An estimate of the fire flow is given by the formula  $F = 220C\sqrt{A}$ Maximum Daily Demand: 11 (L/min) 1. Max. Daily Plus Fire: 8011 (L/min) Where: F = The required fire flow in litres per minute C = Coefficient related to the type of construction A = The total floor area in square metres (including all storeys but excluding basements at least 50% below grade) Area Note: For fire resistive buildings, consider the Type of Construction: Ordinary Coefficient: 1.00 Total Floor Area: 360 (m<sup>2</sup>) two largest adjoining floors plus 50% of F = 4000 (L/min) Adequately Protected Vertical Openings: No the remaining floors up to eight, when openings are inadequately protected. For 2. Adjust the value in No. 1 for occupancy surcharge/reduction adequately protected vertical openings Free Burning **Occupancy Contents:** Factor: 15% consider only the area of the largest floor plus 25% of each of the two immediately F = 4600 (L/min) adjoining floors 3. Adjust the value in No. 2 for sprinkler 4. Adjust the value in No. 2 for exposure Separation (m) Charge 0% 25 NFPA 13 Sprinkler: No Reduction: North 10% 0% 0 Standard Water Supply: No Reduction: East 25% 9 Reduction: 0% Fully Supervised: No South 20% 25% West **Total Reduction:** 0% **Total Charge:** 75% Sprinkler Reduction: 0 (L/min) **Exposure Charge:** 3450 (L/min)

5. Estimated Fire Flow is value in No. 2 less Sprinkler Reduction plus Exposure Charge, rounded to the nearest 1000

F = 8000 (L/min)

### ESTIMATED DEMAND PRESSURE (AT MAIN)

Project:358 Reynolds StreetProject No.:1816Desc:Townhouse UnitsPrepared By:MFChecked By:PC

### Hydrant Residual Flow (Refer to Attached Flow Test Results)

Coefficient	C=	0.9
Port Diameter	D=	2.5 (inch)
Pitot Pressure	P <sub>pit</sub> =	45 (psig)
Residual Flow	$Q_R =$	1126 (us gpm)
Residual Flow	$Q_R =$	4262 (L/min)

### **Hydrant Theoretical Flow (Refer to Attached Flow Test Results)**

Static Pressure	P <sub>stat</sub> =	57 (psig)
Residual Pressure	P <sub>res</sub> =	56 (psig)
Theoretical Pressure	P <sub>theo</sub> =	20 (psig)
Theoretical Flow	$Q_T = $	7913 (us gpm)
Theoretical Flow	$Q_T =$	29951 (L/min)

### **Max. Demand Pressure**

Maximum Demand	$Q_D =$	5136 (L/min)
Maximum Demand	$Q_D = \overline{}$	1357 (us gpm)
Calculated Pressure	P=	56 (psig)

### Where:

$$Q_R = 29.84 \times C \times D^2 \times P_{pit}^{0.5}$$
  
 $Q_T = Q_R \times [(P_{stat} - P_{theo})/(P_{stat} - P_{res})]^{0.54}$   
 $P = P_{stat} - (Q_D/Q_R)^{1.852} \times (P_{stat} - P_{res})$ 

### Notes

Refer to attached hydrant flow test results for 300mm main on Church Street prepared by Jackson Waterworks dated May 2, 2016.

### **ESTIMATED SANITARY FLOW**

Project:358 Reynolds StProject No.:1816Desc:TownhousesPrepared By:MF

Checked By: PC

### Residential

Land Haa / Occupancy Type	Aroa (ha)	Population Density	Eq. Population	Per Cap. Demand (m³/cap-day)	Average Daily Dry Weather Flow
Land Use / Occupancy Type Townhouse, Maisonette - 6 storey or less	Area (ha) 0.283	(pers/ha) 135.0	(cap.) 38	(m /cap-day) 0.275	(L/s) 0.12

TOTAL	0.283	38	0.12

### Industrial / Commercial / Institutional

Density Population Demand		Populati	on Eq.	Per Cap.	Average Daily Dry
1 111 (O T		Density	Population	Demand	Weather Flow
Land Use / Occupancy Type GFA (pers/ha) (cap.) (L/Ha. Day)	Land Use / Occupancy Type GF	FA (pers/h	a) (cap.)	(L/Ha. Day)	(L/s)

ΤΟΤΛΙ	0.000	n	0

Residential Peaking Factor: 4.34
ICI Peaking Factor: 4.50
Include ICI Peaking? No

Tributary Area: 0.283 (ha)
Infiltration Allowance: 0.286 (L/s ha)

 Residential Average Daily Flow:
 0.12 (L/s)

 ICI Average Daily Flow:
 0.00 (L/s)

 Total Average Flow:
 0.12 (L/s)

 Residential Peak Flow:
 0.53 (L/s)

 ICI Peak Flow:
 0.00 (L/s)

 Infiltration:
 0.08 (L/s)

 Design Flow:
 0.61 (L/s)

### **RATIONAL METHOD FLOWS**

Based on Town of Oakville IDF Data

Project:Reynolds TownhousesProject No.:1816Desc:358 Reynolds StreetPrepared By:MFChecked By:PC

### **Pre-Development Parameters**

	Site	External	Total
'C'	0.835	0.000	0.835
'A' (ha)	0.283	0.000	0.283
'AC'	0.236	0.000	0.236

### **Pre-Development Flow**

	Intensity	Site Flow	<b>External Flow</b>	<b>Total Flow</b>
Return	(mm/hr)	(L/s)	(L/s)	(L/s)
2-yr	82.2	54	0	54
5-yr	114.2	75	0	75
10-yr	134.8	88	0	88
25-yr	162.2	117	0	117
50-yr	182.1	143	0	143
100-yr	200.8	158	0	158

Flows have been adjusted using 25-, 50-, and 100-yr factors of 1.1, 1.2, and 1.25 (To a maximum C of 1.0)

### **Post-Development Parameters**

	Controlled	Uncontrolled	External	Total
'C'	0.840	0.000	0.000	0.840
'A' (ha)	0.283	0.000	0.000	0.283
'AC'	0.237	0.000	0.000	0.237

### **Post-Development Flow**

	Intensity		Uncontrolled Flow	Peak Rooftop Flow	External Flow	Total Flow
Return	(mm/hr)	Peak Inflow (L/s)	(L/s)	(L/s)	(L/s)	(L/s)
2-yr	82.2	54	0	0	0	54
5-yr	114.2	75	0	0	0	75
10-yr	134.8	88	0	0	0	88
25-yr	162.2	117	0	0	0	117
50-yr	182.1	143	0	0	0	143
100-yr	200.8	158	0	0	0	158

Flows have been adjusted using 25-, 50-, and 100-yr factors of 1.1, 1.2, and 1.25 (To a maximum C of 1.0)

### Post-to-Pre Comparison\*

	Pre-Dev Total	Post-Dev Total	
Return	(L/s)	(L/s)	Percent Change
2-yr	54	54	0%
5-yr	75	75	0%
10-yr	88	88	0%
25-yr	117	117	0%
50-yr	143	143	0%
100-yr	158	158	0%

<sup>\*</sup>Storage may be required, refer to Modified Rational Method Storage Calculation and Summary sheets if applicable



Prepared By: MF

Checked By: PC

Project No.: 1816

**STORM SEWER DESIGN SHEET** 358 Reynolds Street Project Name :

Town of Oakville **Municipal Number:** 100-Year Storm Date:

2023-11-08 Sheet: 1 of 1

				DRAINAGE AREA			FLOW			SEWER DESIGN				PIPE HYDRAULICS					
FROM LOCATION MH	TO MH	Area, A (ha)	Runoff Coeff., C	A x C (ha)	Accum. A x C (ha)	Time of Conc., T <sub>c</sub> (min)	Intensity, I (mm/h)	Expected Flow, Q (L/s)	Length, L (m)	Gradient, s (%)	Pipe Dia., D (mm)	Manning's Coeff., n	Full Flow Capacity, Q <sub>F</sub> (L/s)	Full Flow Velocity, V <sub>F</sub> (m/s)	d/D	Actual Velocity, V (m/s)	Time of Flow (min)	Q/Q <sub>F</sub>	
	DICB	MH2	0.460	0.65	0.299	0.299													
			0.037	0.84	0.031	0.330	10.00	201.4	185	2.5	2.0	450	0.013	421	1.12	0.46	2.50	0.02	0.44
			0.197	0.65	0.128	0.458													
			0.052	0.84	0.044	0.502		1		<b>-</b>	<b>†</b>	<b>†</b>					1		
			0.033	0.84	0.028	0.530													
			0.103	0.65	0.067	0.596													
MacDonald Road	MH2	MH1	0.143	0.84	0.120	0.717	10.02	201.2	400	66.0	1.0	525	0.013	449	1.79	0.73	2.29	0.48	0.89
	MH1	MH3	0.000	0.70	0.000	0.717	10.50	196.0	390	13.0	1.0	525	0.013	449	1.75	0.72	2.27	0.10	0.87
			0.000	0.70	0.000	0.7.7	10.00	.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				525	0.0.0		0	0.7.2		00	
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																	+		
		1	1	-				-	-		-	-	-				+		<u> </u>

1) Pipe diameter is nominal

2) Capacity and velocity are based on Imperial I.D. (Nom. Dia x 25.4/25) 3) Time of Flow is based on Actual Velocity

Intensity, I = A /  $(T_c + B)^C$  where:

A= 2150

Expected Flow, Q = 2.778 x C x I x A

Full Flow Capacity (Manning's Equation), Q<sub>F</sub>

B= 5.7 C = 0.86  $Q_F = (1/n) \times A \times R^{2/3} \times s^{1/2}$ =  $(1/n) \times 311.7 \times D^{8/3} \times s^{1/2}$ 

 $t_{\text{c}}\text{=}\,$  Time of Concentration in minutes

P:\1816 358 Reynolds Street\01-Calculations\01-SWM\[Storm Sewer Design Sheet rev 2.xlsx]Street Name

### APPENDIX 'D'

Cover Sheet

Erosion and Sediment Control Plan

General Servicing Plan

Storm Drainage Area Plan

Sanitary Drainage Area Plan

Composite Utility Plan

**Grading Plan** 

Plan Profile (STA 0+000 to 0+120)

Standard Notes

## MACDONALD ROSE INC. SUBDIVISION

358 REYNOLDS STREET

### TOWN OF OAKVILLE



# SPRUCE STREET TRAFALGAR ROAD SITE LAWSON ST. KEY PLAN



CONSULTANT FILE: 1816

TOWN FILE: 24T-XXXXX

DRAWING INDEX

EROSION AND SEDIMENT CONTROL PLAN

GENERAL SERVICING PLAN

COMPOSITE UTILITY PLAN

**GRADING PLAN** 

STANDARD NOTES

STORM DRAINAGE AREA PLAN

SANITARY DRAINAGE AREA PLAN

PLAN PROFILE (STA 0+000 TO 0+120)

<u>Sheet</u>

E1

S1

S2

S3

CU1

G1

P1

N1

2 ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE INSPECTED, REPAIRED/MAINTAINED WEEKLY AND FOLLOWING ALL SIGNIFICANT RAINFALLS.

3. THE MEASURES AS PROPOSED MAY BE MODIFIED AT THE DISCRETION OF THE ENGINEER TO SUIT THE PROPOSED CONSTRUCTION PROGRAMS.
THE GENERAL INTENT OF THE PROPOSED EROSION CONTROL MEASURES WILL BE MAINTAINED AT ALL TIMES.

4. DECOMMISSIONING OF ALL EROSION CONTROL MEASURES SHALL OCCUR ONLY ONCE VEGETATIVE COVER IS ESTABLISHED.

5. DESIGNATED ENTRANCE FOR ALL CONSTRUCTION TRAFFIC TO BE INSTALLED WITH MUD CONTROL DEVICE AS PER MUD MAT DETAIL. MUD CONTROL DEVICES TO BE INSTALLED PRIOR TO START OF CONSTRUCTION AND ARE TO BE MAINTAINED IN GOOD WORKING ORDER UNTIL GRADING WORKS ARE COMPLETED. MUD MAT MAY BE DELETED WITH THE APPROVAL OF THE TOWN OF OAKVILLE.

6. ANY DISTURBED AREA NOT SCHEDULED FOR FURTHER CONSTRUCTION WITHIN 30 DAYS SHALL BE PROVIDED WITH A TEMPORARY SEED.

7. INSTALL CATCHBASIN SEDIMENT CONTROL ON EXISTING CATCHBASINS PRIOR TO START OF CONSTRUCTION.

8. INSTALL CATCHBASIN SEDIMENT CONTROL ON NEW CATCHBASINS AT TIME OF INSTALLATION.

9. ALL EROSION AND SEDIMENT CONTROLS ARE TO BE INSTALLED ACCORDING TO THE APPROVED PLANS PRIOR TO COMMENCEMENT OF ANY EARTH MOVING WORK ON THE SITE AND SHALL REMAIN IN PLACE UNTIL ALL DISTURBED AREAS ARE STABILIZED WITH THE INTENDED

10. EROSION AND SEDIMENT CONTROLS SHALL BE INSPECTED BY THE BUILDER/DEVELOPER:

- WEEKLY
- BEFORE AND AFTER ANY PREDICTED RAINFALL EVENT
- FOLLOWING AN UNPREDICTED RAINFALL EVENT
- DAILY, DURING EXTENDED DURATION RAINFALL EVENTS

30M AWAY FROM PROPERTY LINE.

- AFTER SIGNIFICANT SNOW MELT EVENTS 11. DEWATER EXISTING PONDS ONSITE AS REQUIRED WITH DEWATERING BAG ON WOOD PALLETS AND PUMP. DEWATERING BAG TO BE PLACED A MINIMUM OF

12. EROSION AND SEDIMENT CONTROLS SHALL BE MAINTAINED IN PROPER WORKING ORDER AT ALL TIMES. DAMAGED OR CLOGGED DEVICES SHALL BE REPAIRED WITHIN 48 HOURS.

13. WHERE A SITE REQUIRES DEWATERING AND WHERE THE EXPELLED WATER CAN BE FREELY RELEASED TO A SUITABLE RECEIVER, THE EXPELLED WATER SHALL BE TREATED TO CAPTURE SUSPENDED PARTICLES GREATER THAN 40 MICRON IN SIZE. THE CAPTURED SEDIMENT SHALL BE DISPOSED OF PROPERLY PER MOECC GUIDELINES. THE CLEAN EXPELLED WATER SHALL FREELY RELEASE TO A SUITABLE RECEIVER THAT DOES NOT CREATE DOWNSTREAM ISSUES INCLUDING BUT NOT LIMITED TO EROSION, FLOODING -NUISANCE OR OTHERWISE, INTERFERENCE ISSUES, ETC.

14. EXISTING STORM SEWER AND DRAINAGE DITCHES ADJACENT TO THE WORKS SHALL BE PROTECTED AT ALL TIMES FROM THE ENTRY OF SEDIMENT/SILT THAT MAY MIGRATE FROM THE SITE. FOR STORM SEWERS: ALL INLETS (REAR LOT CATCHBASINS, ROAD CATCHBASINS, PIPE INLETS, ETC.) MUST BE SECURED/FITTED WITH SILTATION CONTROL MEASURES. FOR DRAINAGE DITCHES: THE INSTALLATION OF ROCK CHECK DAMS, SILTATION FENCE. SEDIMENT CONTAINMENT DEVICES MUST BE INSTALLED TO TRAP AND CONTAIN SEDIMENT. THESE SILTATION CONTROL DEVICES SHALL BE INSPECTED AND MAINTAINED PER ITEMS B AND C ABOVE.

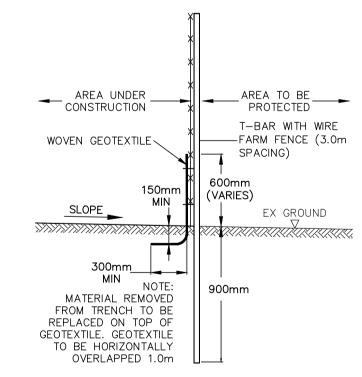
15. IN THE EVENT OF A SPILL (RELEASE OF DELETERIOUS MATERIAL) ON OR EMANATING FROM THE SITE, THE OWNER OR OWNERS AGENT SHALL IMMEDIATELY NOTIFY THE MOECC AND FOLLOW ANY PRESCRIBED CLEAN UP PROCEDURE. THE OWNER OF OWNERS AGENT WILL ADDITIONALLY IMMEDIATELY NOTIFY THE TOWN.

### CONSTRUCTION STAGING SEQUENCE

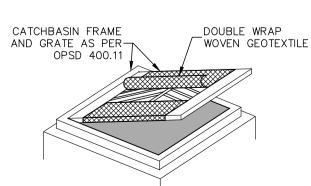
1. INSTALL SILT FENCE, CONSTRUCTION ACCESS, AND TREE PROTECTION FENCING 2. STRIP TOPSOIL

3. PROCEED WITH SITE WORKS

4. REMOVE SILT FENCE ONCE SITE IS STABALIZED.



### SEDIMENT CONTROL FENCE

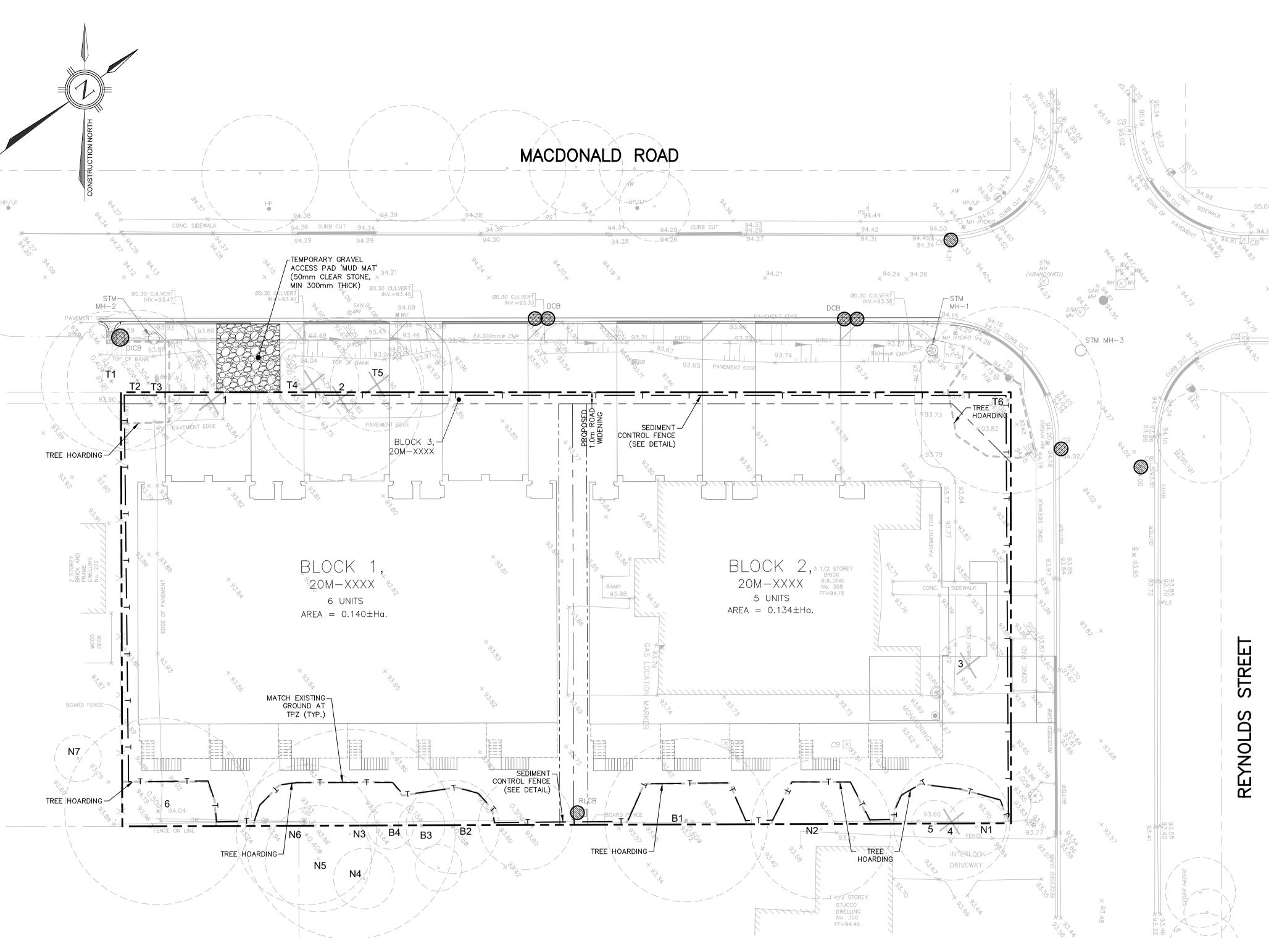


1. TO BE USED UNDER APPROPRIATE DRAINAGE CIRCUMSTANCES, BETWEEN APRIL AND DECEMBER

2. WOVEN GEOTEXTILE TO HAVE EQUIVALENT OPENING SIZE OF 0.15mm AND A MAXIMUM EQUIVALENT OPENING

3. WOVEN GEOTEXTILE TO BE REPLACED PERIODICALLY WHEN ACCUMULATED SEDIMENTS INTERFERES WITH

CATCHBASIN SEDIMENT CONTROL IN PAVED AREAS

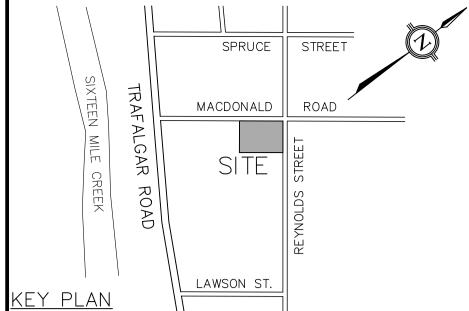


TREE PROTECTION LEGEND (REFER TO ARBORIST REPORT) TREE HOARDING

EXISTING TREE

EXISTING TREE TO BE REMOVED

1, B1, N1, T1 EXISTING TREE NUMBER



### LEGEND

PROPOSED CATCHBASIN PROPOSED DOUBLE CATCHBASIN

PROPOSED STORM MANHOLE

PROPOSED SANITARY MANHOLE PROPOSED FIRE HYDRANT

PROPOSED VALVE & BOX

PROPOSED CURB STOP

--- PROPERTY LINE

+ 94.55 **EXISTING ELEVATION** 

+ 94.55 EXISTING ELEVATION TO REMAIN

→ PROPOSED DRAINAGE DIRECTION

------ PROPOSED SWALE DRAINAGE DIRECTION PROPOSED OVERLAND FLOW DIRECTION

PROPOSED SLOPE

SEDIMENT CONTROL CB IN PAVED AREAS

SEDIMENT CONTROL CB IN LANDSCAPED AREA

T SEDIMENT CONTROL FENCE

BENCHMARK

ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING

AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL

THE SURVEY WAS COMPLETED ON THE 18TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 22-388 CAD FILE No.22-388TP01

DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

2023/11/10 PC/GL REVISED PER PRE-SUBMISSION COMMENTS RZA DPA

2023/06/27 PC/GL ISSUED FOR RZA AND DPA No | DD/MM/YY|By/DRN 1816E.dwg 11/10/23 References

1:200 APPROVALS APPROVED IN PRINCIPLE SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO TOWN OF

OAKVILLE STANDARDS AND SPECIFICATIONS. Hydro Cable Traf. Water Manager of Development Services egional Approval

Field Notes

EGISLATIVE AND PLANNING SERVICES DEPT.





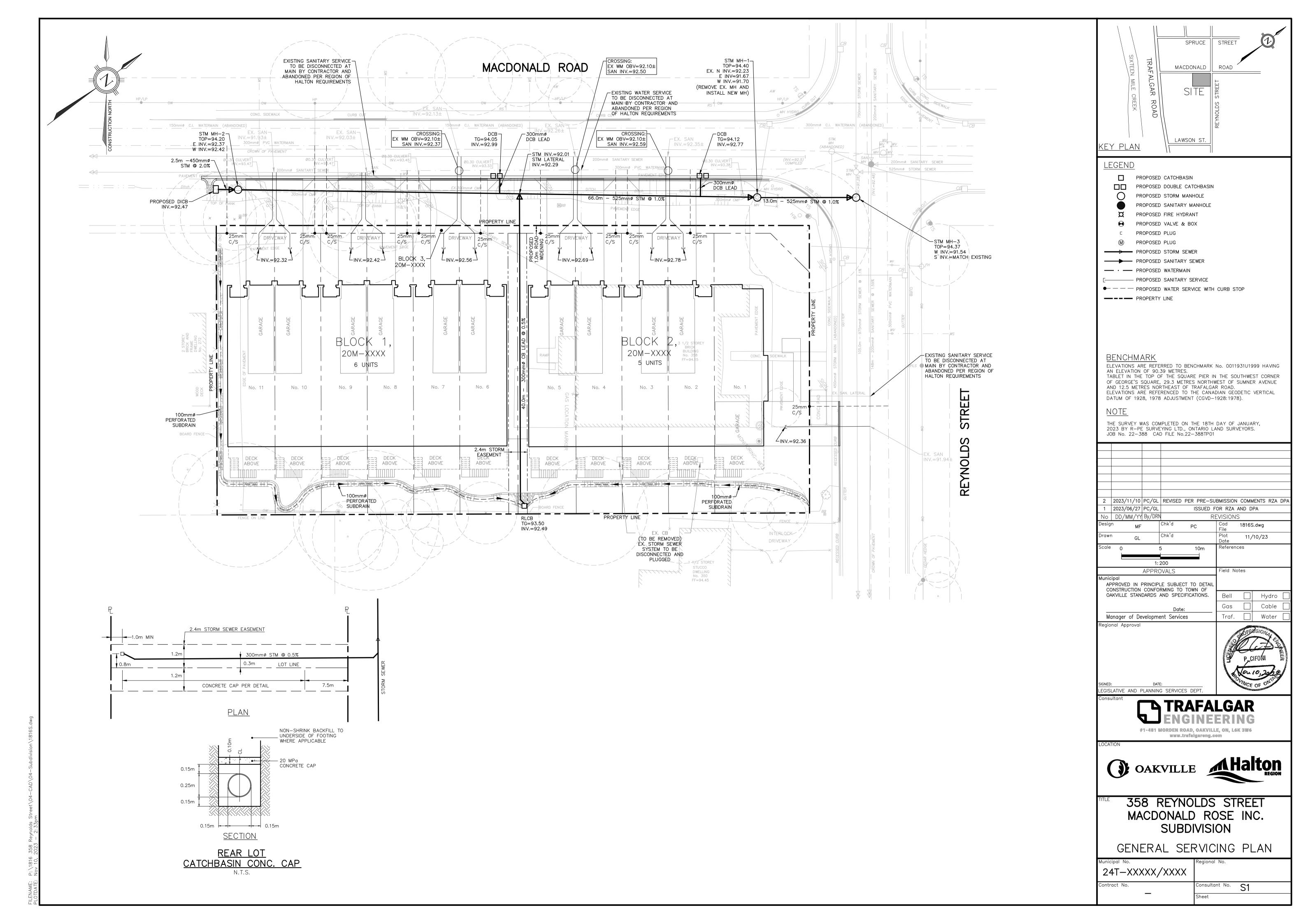


358 REYNOLDS STREET MACDONALD ROSE INC. **SUBDIVISION** 

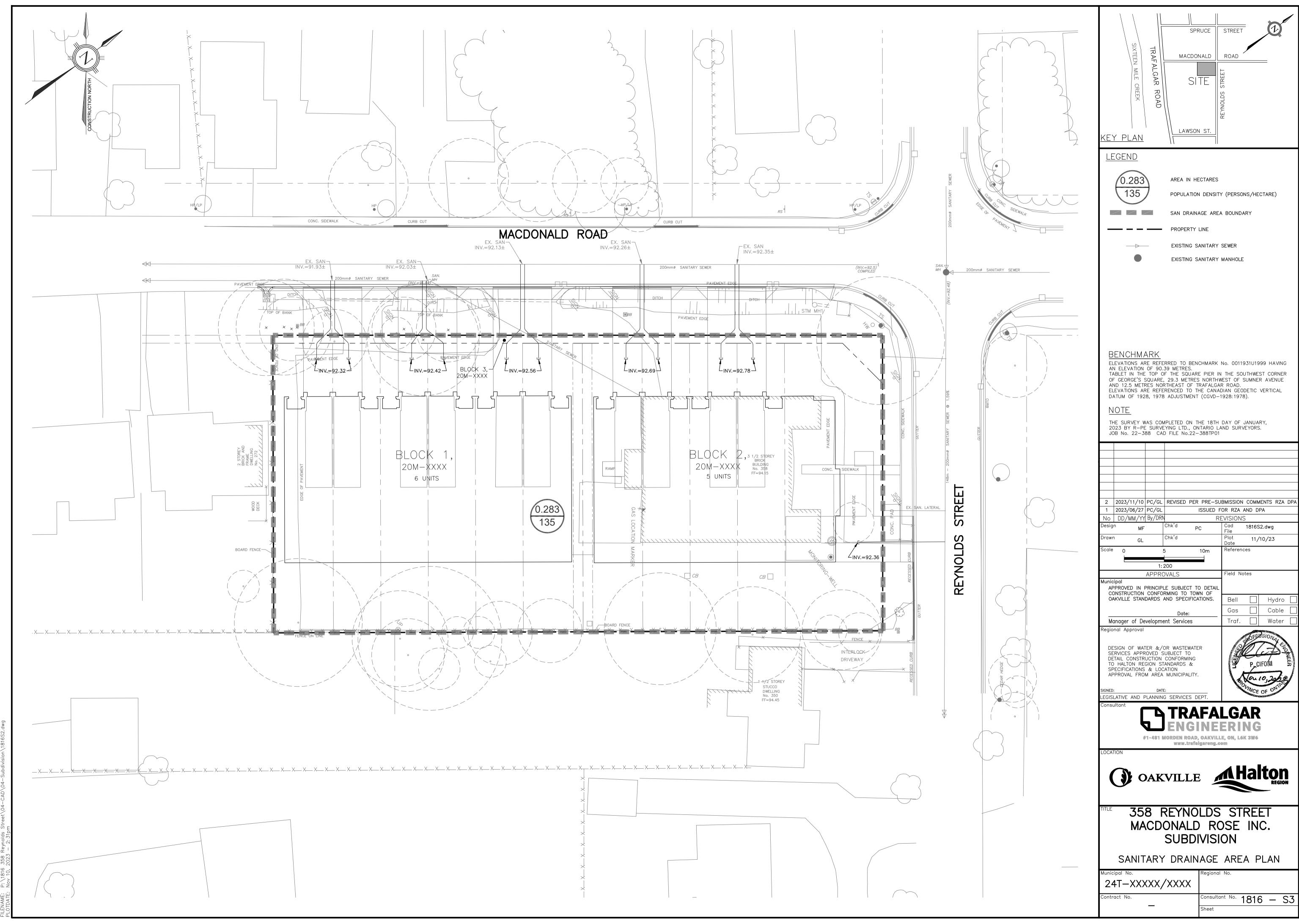
EROSION AND SEDIMENT CONTROL PLAN

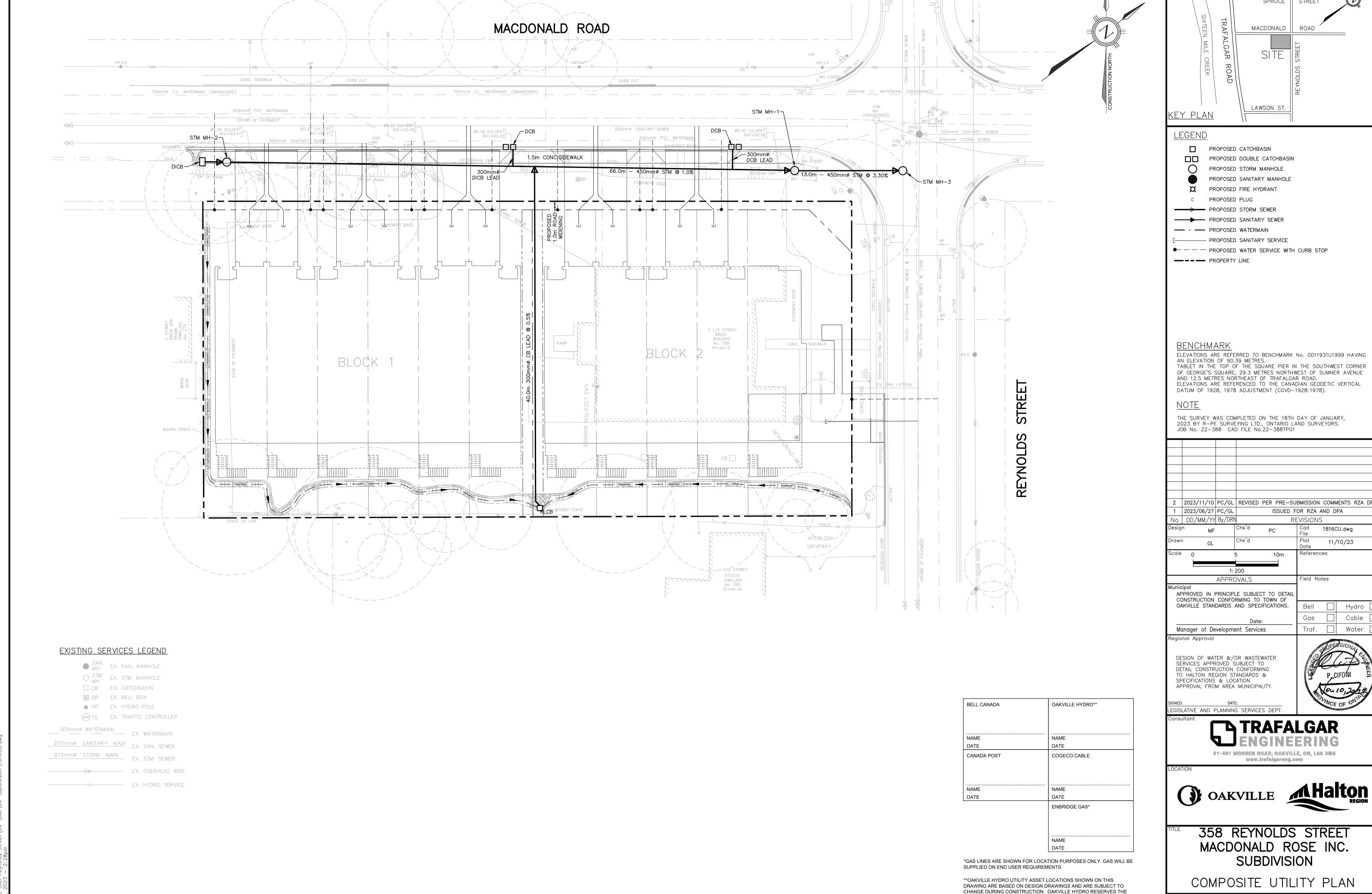
24T-XXXXX/XXXX

E1









SPRUCE | STREET ROAD

● - - - PROPOSED WATER SERVICE WITH CURB STOP

OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL

2 | 2023/11/10 | PC/GL | REVISED PER PRE-SUBMISSION COMMENTS RZA DPA ISSUED FOR RZA AND DPA REVISIONS

1816CU.dwg 11/10/23 References

Cable Traf. Water

Hydro





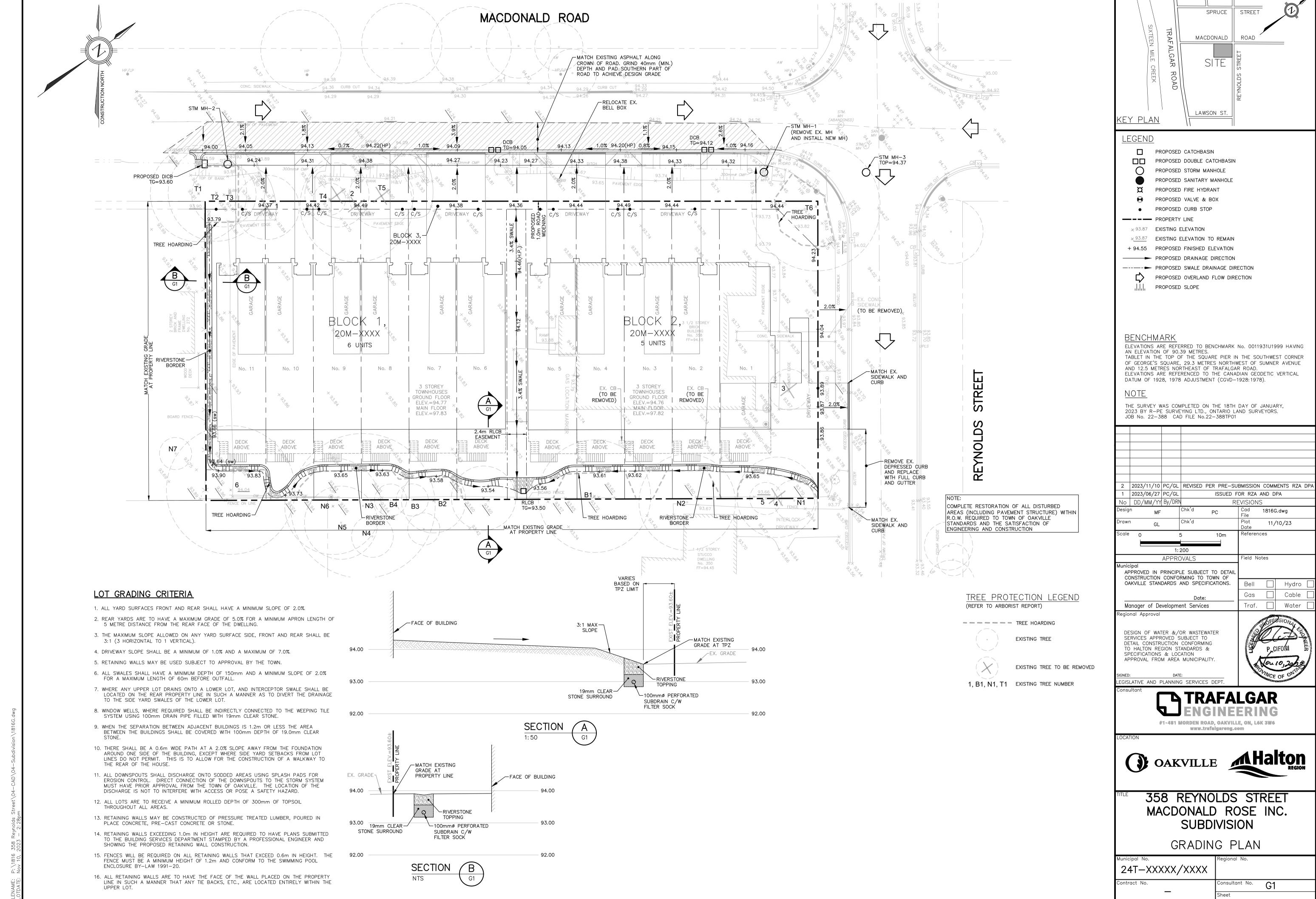
358 REYNOLDS STREET MACDONALD ROSE INC.

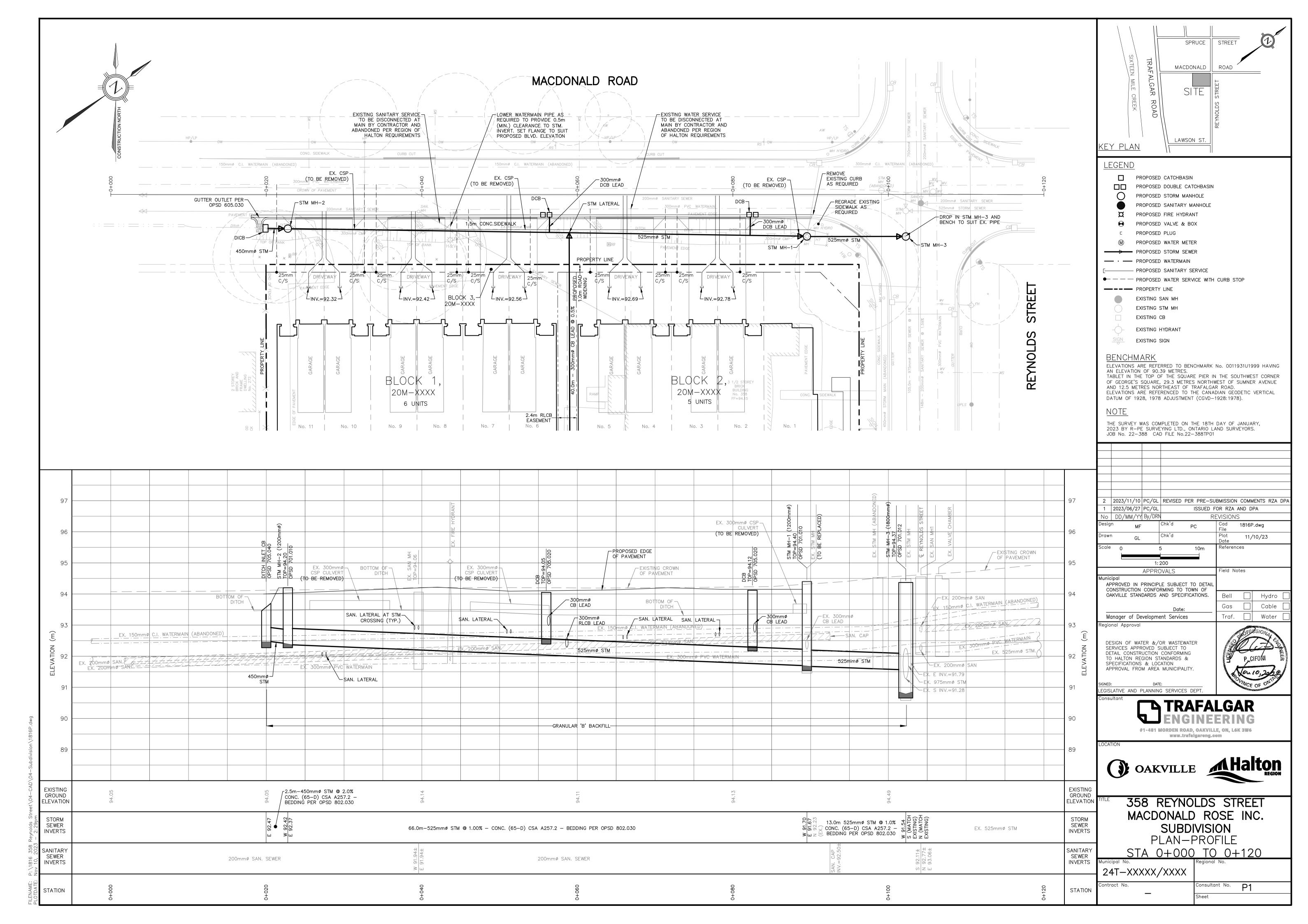
COMPOSITE UTILITY PLAN

RIGHT TO APPROVE OR DENY TREES IN THE VICINITY OF TRANSFORMERS OR ANY OTHER ASSETS. NO UTILITY PEDESTAL,

MAILBOX, TREE AND/OR OTHER ASSETS ALLOWED TO BE INSTALLED ON

24T-XXXXX/XXXX Consultant No. CU1





### GENERAL NOTES

- 1. ALL ROADS, STORM SEWERS AND OTHER MISCELLANEOUS ITEMS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE TOWN OF OAKVILLE REQUIREMENTS. SANITARY SEWERS AND WATERMAINS SHALL BE IN ACCORDANCE WITH THE REGION OF HALTON REQUIREMENTS. IN ABSENCE OF LOCAL STANDARDS, ONTARIO PROVINCIAL STANDARDS AND SPECIFICATIONS SHALL BE USED. AS MODIFIED BY THE LOCAL MUNICIPALITY. ALL MATERIALS SHALL MEET OR EXCEED ONTARIO PROVINCIAL STANDARDS AND TOWN STANDARD SPECIFICATIONS.
- 2. ONTARIO PROVINCIAL STANDARD DRAWINGS (O.P.S.D.) ARE TO BE USED WHEN INDICATED (EXAMPLE: O.P.S.D. 600.04) TOWN OF OAKVILLE STANDARDS ARE USED FOR ROADS. STORM SEWERS AND MISCELLANEOUS WHEN INDICATED (EXAMPLE: 6-1). THE REGION OF HALTON STANDARDS ARE USED ON WATERMAINS AND SANITARY SEWERS AS INDICATED (EXAMPLE: RH 400.01).
- 3. ALL INFORMATION SHOWN ON THE ENGINEERING DRAWINGS REGARDING THE SIZE AND LOCATION OF EXISTING UTILITIES AND/OR SERVICES HAS NOT BEEN VERIFIED IN THE FIELD. BEFORE STARTING WORK, THE CONTRACTOR IS RESPONSIBLE FOR VERIFICATION AND LOCATION OF SAID UTILITIES, PROTECTING AND MAINTAINING UTILITIES DURING CONSTRUCTION, AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO
- 4. THE CONTRACTOR SHALL REPORT ALL DISCREPANCIES TO THE ENGINEER.
- 5. HOARDING OR SNOW FENCE SHALL BE ERECTED PRIOR TO ANY GRADING OR CONSTRUCTION AND SHALL REMAIN IN PLACE AND IN GOOD REPAIR THROUGHOUT THE CONSTRUCTION AND GRADING PHASE AND REMOVED ONLY AS DIRECTED BY THE ENGINEER.
- 6. PRIOR TO THE PLACEMENT OF ANY FILL MATERIAL ALL TOPSOIL IS TO BE REMOVED AND SUBGRADE IS TO BE CERTIFIED BY THE SOILS
- 7. THE CONTRACTOR SHALL NOT DAMAGE TREES OUTSIDE AREAS INDICATED TO BE CLEARED AND GRUBBED.
- 8. TRAFFIC DETOURS AND SIGNAGE TO BE APPROVED BY OAKVILLE TRAFFIC DEPARTMENT. MAINTAIN ONE LANE OPEN TO TRAFFIC AT
- 9. TOWN OF OAKVILLE AND REGION OF HALTON STANDARD DRAWINGS. O.P.S.S. AND O.P.S.D. WITH REGIONAL AMENDMENTS FOR SANITARY SEWERS AND WATERMAINS SHALL CONSTITUTE PART OF THE ENGINEERING DESIGN AND CONSTRUCTION CONTRACT.
- 10. ALL WATERMAIN AND WASTEWATER MAIN APPURTENANCES, MATERIALS AND COMPONENTS SHALL COMPLY WITH THE REGION'S APPROVED MANUFACTURER'S PRODUCT LIST FOR WATER SYSTEMS AND WASTEWATER SYSTEMS. ALTERNATIVE MATERIALS MAY BE ACCEPTABLE, PROVIDED APPROVAL HAS FIRST BEEN OBTAINED FROM THE CITY/TOWN ENGINEER AND/OR THE REGIONAL COMMISSIONER OF PUBLIC WORKS.
- 11. NO BLASTING IS PERMITTED.
- 12. MANHOLE AND VALVE CHAMBER COVERS ARE TO BE SET FLUSH WITH BASE COURSE ASPHALT AND ADJUSTED TO FINAL GRADE PRIOR TO INSTALLING TOP LIFT OF ASPHALT.
- 13. ALL TRENCHES WITHIN EXISTING RIGHT-OF-WAY ARE TO BE BACKFILLED IN ACCORDANCE WITH TOWN OF OAKVILLE REQUIREMENTS.
- 14. ALL SEDIMENT AND EROSION CONTROL MEASURES SHALL BE IN PLACE PRIOR TO COMMENCING ANY EARTHMOVING OPERATIONS.
- 15. ALL OVERLY MOIST, SOFT OR OTHERWISE UNSUITABLE SOIL MUST BE REMOVED DOWN TO FIRM NATIVE SUBSOIL. THE BASE SHOULD BE PROOF-ROLLED AND COMPACTED TO A FIRM STABLE STATE WHICH IS TO BE APPROVED BY THE GEOTECHNICAL ENGINEER BEFORE THE START OF FILL PLACEMENT.
- 16. FILL PLACEMENT MUST BE CARRIED OUT IN A CONTROLLED SYSTEMATIC PROGRESSION WHICH ALLOWS FOR HARMONIOUS AND UNIFORM COVERAGE BY THE COMPACTION EQUIPMENT.
- 17. THE MAXIMUM ALLOWABLE LIFT THICKNESS IS 150mm. THE REQUIRED COMPACTION IS MINIMUM 98% STANDARD PROCTOR MAX. DRY DENSITY.

### <u>WATERMAINS</u>

- WATERMAINS 150MM TO 300MM DIAMETER TO BE P.V.C. CL235 (DR-18) AS PER AWWA C900 (CSA B137.3) WITH GASKETED JOINTS.
- WATER SERVICE CONNECTIONS TO BE AS PER O.P.S.D. 1104.01. AS AMENDED BY REGION OF HALTON PIPE FOR ALL SERVICE CONNECTIONS UP 7. FOR COMMON TRENCH DETAILS REFER TO REGION STD. RH 302.01. TO 50MM DIA. SHALL BE TYPE "K" SOFT COPPER TUBING MEETING AWWA C800 (LATEST EDITION).
- 3. A MIN. HORIZONTAL SEPARATION OF 2.5M MUST BE MAINTAINED BETWEEN 9. BENCHING IN MANHOLES IS TO EXTEND UP TO THE SPRINGLINE OF WATERMAINS AND SANITARY OR STORM SEWERS, INCLUDING SERVICE
- 4. A MIN. VERTICAL SEPARATION OF 0.15M BETWEEN WATERMAINS AND SEWERS MUST BE MAINTAINED IF WATERMAIN CROSSES ABOVE SEWER OR 0.50M IF WATERMAIN CROSSES BELOW SEWER.
- 5. WATERMAIN BEDDING AND COVER TO BE SUITABLE GRANULAR 'A' BEDDING MATERIAL AS PER O.P.S.D. 802.010 AND O.P.S.S. 401.
- 6. ALL HYDRANTS AS PER O.P.S.D. 1105.01 TO HAVE STEAMER CONNECTIONS.
- HYDRANTS TO BE SUPPLIED WITH: a) TWO (2) 63.5MM (21/2") WITH CSA STANDARD THREAD, 63.5MM I.D., 79.4
- O.D., 5 THREADS PER 25MM, 31.75MM SQUARE OPERATING NUT; AND b) ONE (1) 100MM (4") STORZ PUMPER CONNECTION AS PER CAN/ULC #S-520, 31.75MM SQUARE OPERATING NUT, AND STORZ CAP PAINTED
- c) SECONDARY VALVE AND ANCHOR TEE.
- 7. HYDRANTS SHALL BE INSTALLED SUCH THAT THE ROD STEM LENGTH SHALL NOT EXCEED 1.7M MEASURED FROM THE BREAK-OFF FLANGE. IF HYDRANT BARREL LENGTH EXCEEDS 1.7M THEN A HYDRANT THAT CAN BE RAISED FROM THE BOTTOM WITHOUT INCREASING ROD LENGTH IS TO BE USED.
- 8. ALL METALLIC WATERMAINS, FITTINGS, AND APPURTENANCES SHALL BE INSTALLED WITH A MINIMUM OF ONE ANODE PER LENGTH PER PIPE AND ONE ANODE PER ELECTRONICALLY ISOLATED APPURTENANCE AND INSTALLED IN ACCORDANCE WITH OPSS 442 AND OPSD 1109.010 AND 1109.011. ANODE INSTALLATION IS NOT REQUIRED WITHIN VALVE CHAMBERS, DRAIN CHAMBERS, AIR RELEASE CHAMBERS OR SWAB PORTS.
- 9. ALL SACRIFICIAL ANODES SHALL CONFORM TO A.S.T.M. B-418 TYPE II AND SHALL BE MADE OF HIGH GRADE ELECTROLYTIC ZINC, 99.99% PURE, AS PER HALTON LINEAR DESIGN MANUAL, WATER SERVICE CONNECTIONS - 2.10.5.C.ii
- 10. ALL WELD CONNECTIONS TO BE COATED WITH "TC MASTIC" OR APPROVED EQUIVALENT.
- 11. FOR ALL ANODES CONNECTED TO NEW PIPE, FITTINGS OR TO EXISTING METALLIC WATERMAINS, A CADWELDER AND CA-15 OR EQUIVALENT CARTRIDGE SHALL BE USED. ANODE INSTALLATION SHALL BE PERFORMED IN ACCORDANCE WITH THE MANUFACTURER'S INSTRUCTIONS.
- 12. WHERE NEW PIPE IS METALLIC OR OTHERWISE TO BE CONNECTED TO EXISTING DUCTILE IRON OR CAST IRON PIPE A 14.5KG MAGNESIUM ANODE IS TO BE CONNECTED TO THE FIRST LENGTH OF EXISTING PIPE, AS PER OPSS 442 AND OPSD 1109.010 AND 1109.011
- 13. ALL VALVES TO OPEN LEFT (COUNTER-CLOCKWISE), BE OF THE APPROVED TYPE WITH NON-RISING STEM AND SHALL HAVE 50MM SQUARE STANDARD AWWA OPERATING NUT.
- 14. ALL PLUGS, CAPS, TEES, BENDS, AND OTHER APPURTENANCES SHALL BE MECHANICALLY RESTRAINED AS PER MANUFACTURER'S SPECIFICATIONS. MECHANICAL THRUST RESTRAINT DEVICES SHALL HAVE THIRD PARTY TESTING, APPROVALS FROM THE UNDERWRITERS LABORATORY (UL) AND FACTORY MUTUAL (FM), AND BE INCLUDED IN HALTON REGION'S APPROVED MANUFACTURER'S PRODUCT LIST FOR WATER SYSTEMS.

### WATERMAINS Cont'd

- 15. WHERE WATERMAIN IS PLACED IN FILL OR IN PREVIOUSLY DISTURBED GROUND, ALL JOINTS TO BE MECHANICALLY RESTRAINED.
- 16. MINIMUM DEPTH OF COVER OVER WATERMAIN SHALL BE 1.70M MEASURED FROM THE TOP OF THE PIPE TO THE FINISHED GRADE.
- 17. THE DEPTH OF WATER SERVICES AT PROPERTY LINE SHOULD BE A MINIMUM OF 1.7M AND A MAXIMUM OF 2.0M. THE DISTANCE BETWEEN THE GROUND ELEVATION AND THE TOP OF THE ROD SHOULD BE BETWEEN 0.5M AND 1.0M.
- 18. WATER SERVICES CROSSING THE STORM SEWER TO HAVE MIN. 1.70M OF COVER. WHERE THIS CANNOT BE ACHIEVED, WATER SERVICE IS TO CROSS UNDER SEWER.
- 19. GATE VALVES CONFORMING TO A.W.W.A. C509 OR C515 ARE REQUIRED ON WATERMAINS 300MM AND UNDER. LINE GATE VALVES SHALL HAVE SCREW TYPE VALVE BOXES
- 20. ALL WATERMAIN FITTINGS SHALL HAVE MECHANICAL JOINTS. VALVES IN CHAMBERS TO BE FLANGED.
- 21. PIPE BARREL BENDING/DEFLECTION SHALL NOT BE ALLOWED. PIPE JOINT DEFLECTIONS ARE DISCOURAGED (UTILIZE STANDARD BENDS TO ACHIEVE DESIRED VERTICAL AND HORIZONTAL PIPE ALIGNMENT). HOWEVER, IF ABSOLUTELY NECESSARY THE MAXIMUM ALLOWABLE PIPE JOINT DEFLECTION SHALL BE 50% OF THE MANUFACTURER'S SPECIFICATIONS.
- 22. TRACER WIRE IS TO BE INSTALLED ON ALL NEW INSTALLATIONS OF PVC WATERMAIN PIPE FOR LOCATING PURPOSES. A SOLID 10 GAUGE T.W.U. COPPER WIRE IS TO BE INSTALLED ALONG THE TOP OF THE PIPE, STRAPPED TO THE PIPE AT 6M INTERVALS.
- 23. THE INSPECTOR MAY TEST THE TRACING WIRE FOR CONDUCTIVITY. THE TRACER WIRE SHALL BE INSTALLED BETWEEN EACH VALVE AND/OR THE END OF THE NEW WATERMAIN TO ENSURE A CONTINUOUS SIGNAL FOR LOCATING THE MAIN. JOINTS IN THE TRACER WIRE BETWEEN VALVES IS DISCOURAGED, BUT WHEN NECESSARY, MUST BE WATER- PROOFED (REFER TO O.P.S.D. 1109.025) AND DONE IN SUCH A WAY TO ENSURE ELECTRICAL CONDUCTIVITY. AT EACH VALVE. A LOOP OF WIRE IS TO BE BROUGHT UP OUTSIDE THE VALVE BOX AS PER HALTON STANDARD DRAWING RH 406.010. TRACER WIRE FOR HORIZONTAL DIRECTIONAL DRILLING AND PIPE BURSTING INSTALLATION SHALL BE IN ACCORDANCE WITH HALTON REGION'S AMENDMENTS TO O.P.S.S. IF THE TRACING WIRE IS NOT CONTINUOUS FROM VALVE TO VALVE, THE CONTRACTOR SHALL, AT HIS OWN EXPENSE, REPLACE OR REPAIR THE WIRE.
- 24. ALL WATER CUSTOMERS SUPPLIED BY A WATERMAIN TO BE SHUT DOWN SHALL BE NOTIFIED BY THE CONTRACTOR AT LEAST 48 HOURS IN ADVANCE OF THE SHUT DOWN AS PER REGION OF HALTON SPECIFICATIONS. NOTIFICATION SHALL TAKE PLACE UNDER THE ENGINEER'S DIRECTION.
- 25. OPERATING OF EXISTING WATERMAINS SHALL BE BY REGION OF HALTON STAFF ONLY.

### STORM SEWERS

- 1. ALL STORM SEWERS 450mm DIA. OR SMALLER SHALL BE RIBBED PVC PIPE IN ACCORDANCE WITH CSA B182.4. SDR35 WITH LOCK IN RUBBER SEAL RING BEDDING SHALL BE O.P.S.D. 802.010. BEDDING MATERIAL SHALL BE CRUSHED STONE BASE (HL-6) GRAVEL AGGREGATE) AND A GRANULAR "C" COVER MATERIAL.
- 2. ALL STORM SEWERS LARGER THAN 450mm DIAMETER SHALL BE REINFORCED CONCRETE PIPE (CLASS AS SHOWN) IN ACCORDANCE WITH CSA A257.2. BEDDING SHALL BE O.P.S.D. 802.030. BEDDING MATERIAL SHALL BE CRUSHED STONE BASE (HL-6 GRAVEL AGGREGATE) AND A GRANULAR "C" COVER MATERIAL.
- 3. CONTRACTOR IS RESPONSIBLE FOR SUPPLYING ADDITIONAL BEDDING AND/OR STRONGER PIPE IF ACTUAL TRENCH WIDTHS EXCEED DESIGN
- 4. MANHOLE SIZES AS SHOWN.
- 5. SURROUND ALL MANHOLES WITH A MINIMUM OF 1.0m COMPACTED GRANULAR "C"BACKFILL. ALL CATCHBASINS TO HAVE COMPLETE, COMPACTED GRANULAR "C" BACKFILL SURROUND.
- 6. CATCHBASIN (CB) PER O.P.S.D. 705.010 C/W 250mm DIA. LEAD. DOUBLE CATCHBASINS (DCB) PER O.P.S.D. 705.020 C/W 300mm DIA. LEAD. CATCHBASINS TO BE FITTED WITH INLET CONTROL DEVICE AS SHOWN. REAR LOT CATCHBASINS TO BE SUMPLESS PER TOWN STD 3-1 C/W BEEHIVE GRATE PER TOWN STD 5-2.
- 8. DROP STRUCTURES TO BE TOWN OF OAKVILLE STD. 2-2.
- 10. DITCH INLETS TO BE AS PER O.P.S.D. 705.030 3:1 GRATE.
- 11. CATCHBASIN FRAME AND GRATES FOR ROADS TO BE AS PER O.P.S.D.
- 12. SERVICE CONNECTION AT THE STREET LINE IS TO BE HIGHER THAN THE SANITARY CONNECTION AT THAT POINT.
- LUMBER MARKERS PLACED FROM THE INVERT OF THE SERVICE TO 1.0m ABOVE GROUND LEVEL AND PAINTED WHITE.
- DEPTH OF THE MANHOLE EXCEEDS 5.0m.
- 13. ALL ENDS OF SERVICE CONNECTIONS SHALL BE MARKED WITH 100x50
- 14. SAFETY GRATINGS SHALL BE PROVIDED IN ALL MANHOLES WHEN THE
- 15. STORM SERVICE LATERALS TO BE 150mmø DIA FOR SINGLE FAMILY DWELLINGS. LATERALS TO BE MINIMUM 2.00% GRADE. PVC PIPES TO BE WHITE IN COLOUR AND DR28. SHALL BE USED.

### SANITARY SEWERS

- 1. SANITARY MANHOLES AS PER O.P.S.D. 701.010 WITH FRAMES AND COVERS AS PER O.P.S.D. 401.010 TYPE "A" (AS AMENDED RESPECTIVELY BY THE REGION OF HALTON) UNLESS OTHERWISE NOTED ON THE DRAWINGS.
- 2. BENCHING IN MANHOLES TO BE AS PER O.P.S.D. 701.021 AS AMENDED BY THE REGION OF HALTON. BENCHING IN SANITARY MANHOLES TO BE TO THE OBVERT OF THE PIPE.
- 3. SANITARY SEWER PIPE SHALL BE PVC SDR35 (GREEN IN COLOUR) CONFORMING TO CSA B182.2 UNLESS OTHERWISE NOTED.
- 4. SANITARY SERVICE CONNECTIONS TO BE 125mm DIA. FOR SINGLE FAMILY DWELLINGS AND ROWED TOWNHOUSES. COMMERCIAL, INDUSTRIAL, AND INSTITUTIONAL LATERALS SHALL BE A MINIMUM OF 150mm DIAMETER. SANITARY SERVICE CONNECTIONS TO BE MINIMUM 2% GRADE AND SHALL BE NON-WHITE IN COLOUR. FOR PVC LATERAL CONNECTIONS, PIPE SHALL BE GREEN IN COLOUR AND DR28 SHALL
- 5. SERVICES TO BE MIN. 2.15M AND MAX. 2.75M DEEP AT PROPERTY LINE. RISERS SHALL BE USED WHERE NOTED AS PER O.P.S.D.
- 6. GRANULAR "A" BEDDING AND COVER ON ALL SEWERS AND CONNECTIONS TO BE AS PER O.P.S.D. 802.010 UNLESS NOTED OTHERWISE, WITH GRANULAR "B" BACKFILL.
- 7. GRANULAR BACKFILL AROUND MANHOLES SHALL BE COMPACTED BY MECHANICAL MEANS TO A MINIMUM OF 95% S.P.D.

### **ROADS**

- 1. ALL ROAD BASE AND SUB-BASE MATERIALS SHALL BE CRUSHER RUN LIMESTONE MEETING OPSS TYPE II SPECIFICATIONS.
- 2. ANY AREAS WITHIN R.O.W. WHICH REQUIRE FILL IN EXCESS OF 0.30m ARE SUBJECT TO COMPACTION TESTS AND SUCH TESTS MUST SHOW A MIN. COMPACTION OF 98% S.P.M.D.D. AT ALL DEPTHS. ALL EARTHWORKS MUST COMPLY WITH GEOTECHNICAL INVESTIGATION PREPARED BY SOIL-MAT ENGINEERS AND CONSULTANTS LTD. DATED JULY 13, 2012 (PROJ.: SM 124590-G).
- 3. GRANULAR BASE SHALL BE COMPACTED TO A MIN. OF 100% SPMDD IN LIFTS OF 150mm OR LESS.
- 4. ASPHALT MATERIALS SHALL BE ROLLED AND COMPACTED TO A MIN. OF 97% MARSHALL BULK DENSITY.
- 5. PRIOR TO PLACEMENT OF GRANULAR COURSES, THE SUBGRADE SHALL BE PROOF-ROLLED AND ALL LOOSE, SOFT OR UNSTABLE AREAS REMOVED AS DIRECTED BY THE ENGINEER.
- 6. ALL CURB AND GUTTERS SHALL BE PER OPSD 600.040 UNLESS OTHERWISE NOTED.
- 7. PERFORATED SUBDRAINS C/W FILTER SOCK PER TOWN STD. 7-60, SHALL BE INSTALLED UNDER ALL CURBS.
- 8. SIDEWALK TO BE OPSD 310.010.
- 9. AN EXTRA 150mm THICKNESS GRANULAR 'B' SHALL BE ADDED AT ARTERIAL AND INDUSTRIAL ROAD INTERSECTIONS. THIS EXTRA DEPTH SHALL BE EXTENDED FOR A MINIMUM OF 15.0m FROM THE PROPERTY LINE OF THE INTERSECTING STREET.
- 10. TOP COURSE ASPHALTIC CONCRETE SHALL BE PLACED ONLY AFTER ADJACENT BUILDINGS (HOMES, INDUSTRIAL, COMMERCIAL, ETC.) HAVE BEEN CONSTRUCTED AND ONLY WITH THE CONSENT OF THE DIRECTOR OF ENGINEERING AND CONSTRUCTION.
- 11. SIDEWALK RAMPS AT INTERSECTIONS AND MID-BLOCK CROSSINGS SHALL CONFORM TO OPSD 310.030 WITH THE REQUIREMENT THAT THE
- 12. PAVEMENT STRUCTURE (TO BE CONFIRMED BY GEOTECHNICAL

RAMP GRADIENT SHALL NOT EXCEED 5%.

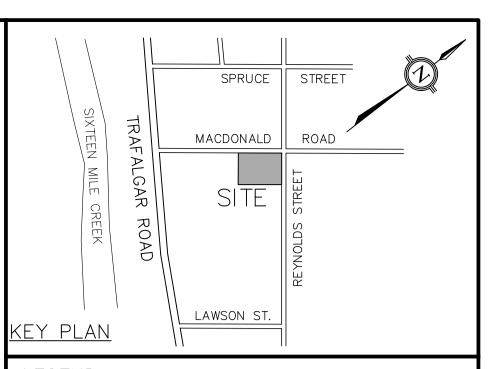
50mm HL8 150mm GRANULAR 'A'

350mm GRANULAR 'B'

### CONSTRUCTION

CONSULTANT):

- 1. CONTRACTOR IS RESPONSIBLE FOR ALL TEMPORARY TRAFFIC CONTROLS, PER MTO BOOK 7.
- 2. CONTRACTOR IS RESPONSIBLE FOR ALL CONSTRUCTION LAYOUT, WITH CONTROL BARS PROVIDED BY THE OWNER. PROTECTION OF CONTROL BARS IS THE RESPONSIBILITY OF THE CONTRACTOR.
- 3. CONTRACTOR IS RESPONSIBLE TO VERIFY THE SIZE AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO CONSTRUCTION, INCLUDING VAC TRUCK AND RESTORATION AS REQUIRED.
- 4. CONTRACTOR SHALL PROVIDE THIRD-PARTY DIGITAL AS-BUILTS IN CAD TO INCLUDE ALL NEW SITE SERVICING INCLUDING TOPS AND INVERTS, AND FINISHED GRADES, INCLUDING PAVED AREAS, SWALES, CURBS, SIDEWALKS AND AND RETAINING WALLS, TO THE SATISFACTION
- 5. CONTRACTOR SHALL FLUSH AND VIDEO ALL EXISTING SEWERS PRIOR TO AND AFTER CONNECTION, AND NEW AND DISTURBED SEWERS UPON INSTALLATION AND LATER UPON COMPLETION OF TOP WORKS AND LANDSCAPING, PER OPSS 409. VIDEOS TO BE PROVIDED TO THE ENGINEER FOR REVIEW AND APPROVAL.

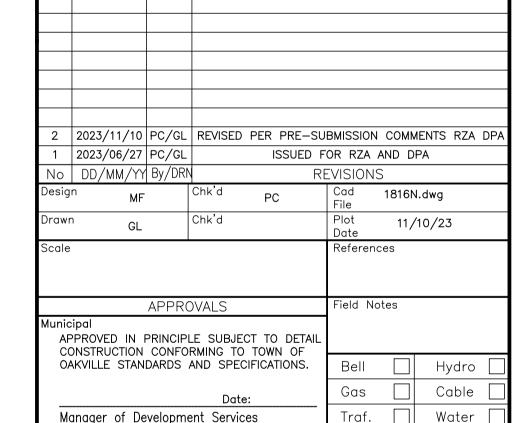


LEGEND

BENCHMARK

ELEVATIONS ARE REFERRED TO BENCHMARK No. 0011931U1999 HAVING AN ELEVATION OF 90.39 METRES. TABLET IN THE TOP OF THE SQUARE PIER IN THE SOUTHWEST CORNER OF GEORGE'S SQUARE, 29.3 METRES NORTHWEST OF SUMNER AVENUE AND 12.5 METRES NORTHEAST OF TRAFALGAR ROAD. ELEVATIONS ARE REFERENCED TO THE CANADIAN GEODETIC VERTICAL DATUM OF 1928, 1978 ADJUSTMENT (CGVD-1928:1978).

THE SURVEY WAS COMPLETED ON THE 18TH DAY OF JANUARY, 2023 BY R-PE SURVEYING LTD., ONTARIO LAND SURVEYORS. JOB No. 22-388 CAD FILE No.22-388TP01



DESIGN OF WATER &/OR WASTEWATER SERVICES APPROVED SUBJECT TO DETAIL CONSTRUCTION CONFORMING TO HALTON REGION STANDARDS & SPECIFICATIONS & LOCATION APPROVAL FROM AREA MUNICIPALITY.

Regional Approval

LEGISLATIVE AND PLANNING SERVICES DEPT.



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OCATION



358 REYNOLDS STREET MACDONALD ROSE INC. **SUBDIVISION** 

STANDARD NOTES

24T-XXXXX/XXXX onsultant No. ontract No.